Stormwater Report North Street & Blackstone Street Bellingham, MA



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G&H Project F4457



Massachusetts Department of Environmental Protection Bureau of Resource Protection - Wetlands Program Checklist for Stormwater Report

A. Introduction

Important: When filling out forms on the computer, use only the tab key to move your cursor - do not use the return key.



A Stormwater Report must be submitted with the Notice of Intent permit application to document compliance with the Stormwater Management Standards. The following checklist is NOT a substitute for the Stormwater Report (which should provide more substantive and detailed information) but is offered here as a tool to help the applicant organize their Stormwater Management documentation for their Report and for the reviewer to assess this information in a consistent format. As noted in the Checklist, the Stormwater Report must contain the engineering computations and supporting information set forth in Volume 3 of the Massachusetts Stormwater Handbook. The Stormwater Report must be prepared and certified by a Registered Professional Engineer (RPE) licensed in the Commonwealth.

The Stormwater Report must include:

- The Stormwater Checklist completed and stamped by a Registered Professional Engineer (see page 2) that certifies that the Stormwater Report contains all required submittals.¹ This Checklist is to be used as the cover for the completed Stormwater Report.
- Applicant/Project Name
- Project Address
- Name of Firm and Registered Professional Engineer that prepared the Report
- Long-Term Pollution Prevention Plan required by Standards 4-6
- Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan required by Standard 8²
- Operation and Maintenance Plan required by Standard 9

In addition to all plans and supporting information, the Stormwater Report must include a brief narrative describing stormwater management practices, including environmentally sensitive site design and LID techniques, along with a diagram depicting runoff through the proposed BMP treatment train. Plans are required to show existing and proposed conditions, identify all wetland resource areas, NRCS soil types, critical areas, Land Uses with Higher Potential Pollutant Loads (LUHPPL), and any areas on the site where infiltration rate is greater than 2.4 inches per hour. The Plans shall identify the drainage areas for both existing and proposed conditions at a scale that enables verification of supporting calculations.

As noted in the Checklist, the Stormwater Management Report shall document compliance with each of the Stormwater Management Standards as provided in the Massachusetts Stormwater Handbook. The soils evaluation and calculations shall be done using the methodologies set forth in Volume 3 of the Massachusetts Stormwater Handbook.

To ensure that the Stormwater Report is complete, applicants are required to fill in the Stormwater Report Checklist by checking the box to indicate that the specified information has been included in the Stormwater Report. If any of the information specified in the checklist has not been submitted, the applicant must provide an explanation. The completed Stormwater Report Checklist and Certification must be submitted with the Stormwater Report.

¹ The Stormwater Report may also include the Illicit Discharge Compliance Statement required by Standard 10. If not included in the Stormwater Report, the Illicit Discharge Compliance Statement must be submitted prior to the discharge of stormwater runoff to the post-construction best management practices.

² For some complex projects, it may not be possible to include the Construction Period Erosion and Sedimentation Control Plan in the Stormwater Report. In that event, the issuing authority has the discretion to issue an Order of Conditions that approves the project and includes a condition requiring the proponent to submit the Construction Period Erosion and Sedimentation Control Plan before commencing any land disturbance activity on the site.



B. Stormwater Checklist and Certification

The following checklist is intended to serve as a guide for applicants as to the elements that ordinarily need to be addressed in a complete Stormwater Report. The checklist is also intended to provide conservation commissions and other reviewing authorities with a summary of the components necessary for a comprehensive Stormwater Report that addresses the ten Stormwater Standards.

Note: Because stormwater requirements vary from project to project, it is possible that a complete Stormwater Report may not include information on some of the subjects specified in the Checklist. If it is determined that a specific item does not apply to the project under review, please note that the item is not applicable (N.A.) and provide the reasons for that determination.

A complete checklist must include the Certification set forth below signed by the Registered Professional Engineer who prepared the Stormwater Report.

Registered Professional Engineer's Certification

I have reviewed the Stormwater Report, including the soil evaluation, computations, Long-term Pollution Prevention Plan, the Construction Period Erosion and Sedimentation Control Plan (if included), the Longterm Post-Construction Operation and Maintenance Plan, the Illicit Discharge Compliance Statement (if included) and the plans showing the stormwater management system, and have determined that they have been prepared in accordance with the requirements of the Stormwater Management Standards as further elaborated by the Massachusetts Stormwater Handbook. I have also determined that the information presented in the Stormwater Checklist is accurate and that the information presented in the Stormwater Report accurately reflects conditions at the site as of the date of this permit application.

Registered Professional Engineer Block and Signature



2/13/2024 ma

Signature and Date

Checklist

Project Type: Is the application for new development, redevelopment, or a mix of new and redevelopment?

New development

Redevelopment

Mix of New Development and Redevelopment



LID Measures: Stormwater Standards require LID measures to be considered. Document what environmentally sensitive design and LID Techniques were considered during the planning and design of the project:

| No disturbance to any Wetland Resource A | reas |
|--|------|
|--|------|

- Site Design Practices (e.g. clustered development, reduced frontage setbacks)
- Reduced Impervious Area (Redevelopment Only)
- Minimizing disturbance to existing trees and shrubs
- LID Site Design Credit Requested:
 - Credit 1
 - Credit 2
 - Credit 3
- Use of "country drainage" versus curb and gutter conveyance and pipe
- Bioretention Cells (includes Rain Gardens)
- Constructed Stormwater Wetlands (includes Gravel Wetlands designs)
- Treebox Filter
- Water Quality Swale
- Grass Channel
- Green Roof
- Other (describe):

Standard 1: No New Untreated Discharges

- No new untreated discharges
- Outlets have been designed so there is no erosion or scour to wetlands and waters of the Commonwealth
- Supporting calculations specified in Volume 3 of the Massachusetts Stormwater Handbook included.



Standard 2: Peak Rate Attenuation

- Standard 2 waiver requested because the project is located in land subject to coastal storm flowage and stormwater discharge is to a wetland subject to coastal flooding.
- Evaluation provided to determine whether off-site flooding increases during the 100-year 24-hour storm.

Calculations provided to show that post-development peak discharge rates do not exceed predevelopment rates for the 2-year and 10-year 24-hour storms. If evaluation shows that off-site flooding increases during the 100-year 24-hour storm, calculations are also provided to show that post-development peak discharge rates do not exceed pre-development rates for the 100-year 24hour storm.

Standard 3: Recharge

Soil Analysis provided.

- Required Recharge Volume calculation provided.
- Required Recharge volume reduced through use of the LID site Design Credits.
- Sizing the infiltration, BMPs is based on the following method: Check the method used.

| \bowtie | Static |
|-----------|--------|
|-----------|--------|

Dynamic Field¹

 \boxtimes Runoff from all impervious areas at the site discharging to the infiltration BMP.

Simple Dynamic

- Runoff from all impervious areas at the site is *not* discharging to the infiltration BMP and calculations are provided showing that the drainage area contributing runoff to the infiltration BMPs is sufficient to generate the required recharge volume.
- Recharge BMPs have been sized to infiltrate the Required Recharge Volume.
- Recharge BMPs have been sized to infiltrate the Required Recharge Volume *only* to the maximum extent practicable for the following reason:
 - Site is comprised solely of C and D soils and/or bedrock at the land surface
 - M.G.L. c. 21E sites pursuant to 310 CMR 40.0000
 - Solid Waste Landfill pursuant to 310 CMR 19.000
 - Project is otherwise subject to Stormwater Management Standards only to the maximum extent practicable.
- \boxtimes Calculations showing that the infiltration BMPs will drain in 72 hours are provided.
- Property includes a M.G.L. c. 21E site or a solid waste landfill and a mounding analysis is included.

¹ 80% TSS removal is required prior to discharge to infiltration BMP if Dynamic Field method is used.



Standard 3: Recharge (continued)

- The infiltration BMP is used to attenuate peak flows during storms greater than or equal to the 10year 24-hour storm and separation to seasonal high groundwater is less than 4 feet and a mounding analysis is provided.
- Documentation is provided showing that infiltration BMPs do not adversely impact nearby wetland resource areas.

Standard 4: Water Quality

The Long-Term Pollution Prevention Plan typically includes the following:

- Good housekeeping practices;
- Provisions for storing materials and waste products inside or under cover;
- Vehicle washing controls;
- Requirements for routine inspections and maintenance of stormwater BMPs;
- Spill prevention and response plans;
- Provisions for maintenance of lawns, gardens, and other landscaped areas;
- Requirements for storage and use of fertilizers, herbicides, and pesticides;
- Pet waste management provisions;
- Provisions for operation and management of septic systems;
- Provisions for solid waste management;
- Snow disposal and plowing plans relative to Wetland Resource Areas;
- Winter Road Salt and/or Sand Use and Storage restrictions;
- Street sweeping schedules;
- Provisions for prevention of illicit discharges to the stormwater management system;
- Documentation that Stormwater BMPs are designed to provide for shutdown and containment in the event of a spill or discharges to or near critical areas or from LUHPPL;
- Training for staff or personnel involved with implementing Long-Term Pollution Prevention Plan;
- List of Emergency contacts for implementing Long-Term Pollution Prevention Plan.
- A Long-Term Pollution Prevention Plan is attached to Stormwater Report and is included as an attachment to the Wetlands Notice of Intent.
- Treatment BMPs subject to the 44% TSS removal pretreatment requirement and the one inch rule for calculating the water quality volume are included, and discharge:
 - is within the Zone II or Interim Wellhead Protection Area
 - is near or to other critical areas
 - is within soils with a rapid infiltration rate (greater than 2.4 inches per hour)
 - involves runoff from land uses with higher potential pollutant loads.
- The Required Water Quality Volume is reduced through use of the LID site Design Credits.
- Calculations documenting that the treatment train meets the 80% TSS removal requirement and, if applicable, the 44% TSS removal pretreatment requirement, are provided.



| Checklist (continued) |
|--|
| Standard 4: Water Quality (continued) |
| \boxtimes The BMP is sized (and calculations provided) based on: |
| ☐ The ½" or 1" Water Quality Volume or |
| The equivalent flow rate associated with the Water Quality Volume and documentation is provided showing that the BMP treats the required water quality volume. |
| ☐ The applicant proposes to use proprietary BMPs, and documentation supporting use of proprietary BMP and proposed TSS removal rate is provided. This documentation may be in the form of the propriety BMP checklist found in Volume 2, Chapter 4 of the Massachusetts Stormwater Handbook and submitting copies of the TARP Report, STEP Report, and/or other third party studies verifying performance of the proprietary BMPs. |
| A TMDL exists that indicates a need to reduce pollutants other than TSS and documentation showing that the BMPs selected are consistent with the TMDL is provided. |
| Standard 5: Land Uses With Higher Potential Pollutant Loads (LUHPPLs) |
| The NPDES Multi-Sector General Permit covers the land use and the Stormwater Pollution Prevention Plan (SWPPP) has been included with the Stormwater Report. The NPDES Multi-Sector General Permit covers the land use and the SWPPP will be submitted <i>prior to</i> the discharge of stormwater to the post-construction stormwater BMPs. |
| ☐ The NPDES Multi-Sector General Permit does <i>not</i> cover the land use. |
| LUHPPLs are located at the site and industry specific source control and pollution prevention measures have been proposed to reduce or eliminate the exposure of LUHPPLs to rain, snow, snow melt and runoff, and been included in the long term Pollution Prevention Plan. |
| All exposure has been eliminated. |
| All exposure has <i>not</i> been eliminated and all BMPs selected are on MassDEP LUHPPL list. |
| The LUHPPL has the potential to generate runoff with moderate to higher concentrations of oil and grease (e.g. all parking lots with >1000 vehicle trips per day) and the treatment train includes an oil |

Standard 6: Critical Areas

- The discharge is near or to a critical area and the treatment train includes only BMPs that MassDEP has approved for stormwater discharges to or near that particular class of critical area.
- Critical areas and BMPs are identified in the Stormwater Report.

grit separator, a filtering bioretention area, a sand filter or equivalent.



Standard 7: Redevelopments and Other Projects Subject to the Standards only to the maximum extent practicable

The project is subject to the Stormwater Management Standards only to the maximum Extent Practicable as a:

| Limited Project | ct |
|-----------------|----|
|-----------------|----|

- Small Residential Projects: 5-9 single family houses or 5-9 units in a multi-family development provided there is no discharge that may potentially affect a critical area.
- Small Residential Projects: 2-4 single family houses or 2-4 units in a multi-family development with a discharge to a critical area
- Marina and/or boatyard provided the hull painting, service and maintenance areas are protected from exposure to rain, snow, snow melt and runoff
- Bike Path and/or Foot Path
- Redevelopment Project
- Redevelopment portion of mix of new and redevelopment.
- Certain standards are not fully met (Standard No. 1, 8, 9, and 10 must always be fully met) and an explanation of why these standards are not met is contained in the Stormwater Report.

☐ The project involves redevelopment and a description of all measures that have been taken to improve existing conditions is provided in the Stormwater Report. The redevelopment checklist found in Volume 2 Chapter 3 of the Massachusetts Stormwater Handbook may be used to document that the proposed stormwater management system (a) complies with Standards 2, 3 and the pretreatment and structural BMP requirements of Standards 4-6 to the maximum extent practicable and (b) improves existing conditions.

Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control

A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan must include the following information:

- Narrative;
- Construction Period Operation and Maintenance Plan;
- Names of Persons or Entity Responsible for Plan Compliance;
- Construction Period Pollution Prevention Measures;
- Erosion and Sedimentation Control Plan Drawings;
- Detail drawings and specifications for erosion control BMPs, including sizing calculations;
- Vegetation Planning;
- Site Development Plan;
- Construction Sequencing Plan;
- Sequencing of Erosion and Sedimentation Controls;
- Operation and Maintenance of Erosion and Sedimentation Controls;
- Inspection Schedule;
- Maintenance Schedule;
- Inspection and Maintenance Log Form.

A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan containing the information set forth above has been included in the Stormwater Report.



Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control (continued)

- ☐ The project is highly complex and information is included in the Stormwater Report that explains why it is not possible to submit the Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan with the application. A Construction Period Pollution Prevention and Erosion and Sedimentation Control has *not* been included in the Stormwater Report but will be submitted *before* land disturbance begins.
- The project is *not* covered by a NPDES Construction General Permit.
- The project is covered by a NPDES Construction General Permit and a copy of the SWPPP is in the Stormwater Report.
- The project is covered by a NPDES Construction General Permit but no SWPPP been submitted. The SWPPP will be submitted BEFORE land disturbance begins.

Standard 9: Operation and Maintenance Plan

- The Post Construction Operation and Maintenance Plan is included in the Stormwater Report and includes the following information:
 - Name of the stormwater management system owners;
 - Party responsible for operation and maintenance;
 - Schedule for implementation of routine and non-routine maintenance tasks;
 - Plan showing the location of all stormwater BMPs maintenance access areas;
 - Description and delineation of public safety features;
 - Estimated operation and maintenance budget; and
 - Operation and Maintenance Log Form.
- The responsible party is *not* the owner of the parcel where the BMP is located and the Stormwater Report includes the following submissions:
 - A copy of the legal instrument (deed, homeowner's association, utility trust or other legal entity) that establishes the terms of and legal responsibility for the operation and maintenance of the project site stormwater BMPs;
 - A plan and easement deed that allows site access for the legal entity to operate and maintain BMP functions.

Standard 10: Prohibition of Illicit Discharges

- The Long-Term Pollution Prevention Plan includes measures to prevent illicit discharges;
- An Illicit Discharge Compliance Statement is attached;
- NO Illicit Discharge Compliance Statement is attached but will be submitted *prior to* the discharge of any stormwater to post-construction BMPs.

Project Description

The project locus is a $20.8\pm$ acre site located adjacent to North Street, and Blackstone Street. It is in the Agricultural District Zone. The project area contains approximately $5.4\pm$ acres of land which will be fully developed, and the remaining lot area consists of approximately $15.5\pm$ acres which will be designated as conservation land which will remain undeveloped. Run-off from this property generally flows from west to east ultimately captured within Bordering Vegetative Wetland (BVW) located in the easterly portion of the property. See Appendix 1/Locus Map.

Soils on site are in three categories – a Canton fine sandy loam 422B, 0 to 8% slopes, extremely stony, Hydrologic Group B, Canton fine sandy loam 420B, 3 to 8% slopes, Hydrologic Group B, and Merrimac fine sandy loam 254B, 3 to 8% slopes, Hydrologic Group A based on the web soil survey and site observations - See Appendix 2 / NRCS Soil Report.

The project proponent intends to construct a $366\pm$ foot long roadway with bituminous concrete curbing and asphalt sidewalk. The proposed road will be 22' wide paved surface with access to Blackstone Street and will serve five 3-unit Townhouses. Each unit will have public water service and all units will be connected to a shared septic system for sewer. Storm water run-off will be collected by catch basin to manhole drainage system. A majority of run-off captured within the development will be sent to an infiltration basin, while the remaining runoff, will be conveyed through a series of drainage pipes and swales. Ultimately all the runoff generated from this development will be discharged to the existing wetlands located on the property to the east.

Pre-development drainage runoff from the site was analyzed as two watersheds - See Appendix 10 / Drainage Area Plans.

- EX-1 This watershed drainage area includes approximately 19.4± acres of both onsite and offsite areas. Runoff from this watershed flows easterly to an existing depression, which discharges overland when full to the bordering vegetative wetlands located on the east side of the property and is identified at the point of analysis (AP-1).
- EX-2 This watershed drainage area includes approximately 2.0± acres of contributing area. Runoff from this watershed flows overland southeasterly to Blackstone Street, which is identified at the point of analysis (AP-2).

The Post-Development Drainage Analysis regards the area as four watersheds – See Appendix 10 / Drainage Area Plans.

• PR-1 watershed consists of a proposed paved roadway, sidewalks, driveways, roofs, infiltration basin, and lawn areas of the proposed development which will be collected by the proposed drainage system. The entirety of the proposed drainage system is collected by street catch basins and conveyed by drainage pipes and

manholes to the proposed infiltration basin located in the eastern side of the project area, ultimately discharging to the wetlands located to the east within the proposed conservation area and is identified as point of analysis (AP-1).

- PR-2 watershed includes primarily the undeveloped portion of the property located along the north and west property lines, as well as a portion of the westerly lawn area. Topography and runoff patterns remain generally unchanged from the predevelopment conditions. Runoff generated in this sub catchment flows via surface flow to inlet basin #2 and is captured and conveyed via pipe to the proposed infiltration basin for infiltration and detention prior to discharging to the wetlands located to the east within the conservation easement and is identified as point of analysis (AP-1).
- PR-3 watershed includes primarily the undeveloped portion of the property which currently flows to Blackstone Street, as well as a portion of the southwesterly lawn area. Topography and runoff patterns remain generally unchanged from the predevelopment conditions. Runoff generated in this sub catchment flows via surface flow southeasterly to Blackstone Street, identified as point of analysis (AP-2).
- PR-4 watershed consists of that portion of the proposed lawn area not captured by the proposed drainage system, which flows easterly overland via swale, discharging to the wetlands identified as point of analysis (AP-1)

Post development stormwater runoff will be treated and attenuated by a standard catch basin to manhole collection system. The site has soils that are considered to have low stormwater runoff potential as identified in the NRCS Web Soil Survey information provided in Appendix 2. The site is designed to be in conformance with the Massachusetts Stormwater Management Guidelines, Massachusetts Wetlands Protection Act and the Town of Bellingham local bylaws and regulations for stormwater management and compliance.

Stormwater Design Parameter:

The stormwater management system was designed to control the post-development rate of peak rainfall runoff from the site by keeping it below the post-development peak rate of rainfall runoff as stated as the objective in the Massachusetts Stormwater Handbook. The calculations were performed using the HydroCAD hydraulic program, developed by applied Microcomputer System. The HydroCAD software is based upon the Soil Conservation Service, "Technical Release 55 – Urban Hydrology for Small Watersheds" and is generally accepted industry methodology.

The analysis was performed for the 2-year, 10-year, and 100-year 24-hour storm events.

The following data was required for input:

• Watershed Area: Areas of each watershed were calculated and expressed in square feet for these calculations.

- SCS Curve Number (Cn): Based on the cover type and hydrologic soil group, a weighted curve number (CN) was determined for each of the existing watersheds utilizing Table 2-2a- *Runoff Curve Numbers For Urban Areas* and *Worksheet 2, Runoff Curve Number and Runoff* from the Soil Conservation Service Technical Release 55 Urban Hydrology for Small Watersheds.
- Time of Concentration, Tc (Minutes): The time of concentration for each watershed was determined by finding the time necessary for runoff to travel from the hydraulically most distant point in the watershed to the point of analysis. This was calculated by using a minimum time of 6 minutes for runoff to reach the most distant catch basin.
- SCS 24-Hour Storm Type: For the greater New England region, a Type III storm rainfall distribution is recommended for drainage calculations and was used for this project.
- Rainfall Precipitation: Rainfall precipitations used the Cornell Extreme Precipitations rainfall estimates for Norfolk County for the 2, 10, 25, and 100 year storm events and are as follows:

2-year storm event: 3.26 inches10-year storm event: 4.88 inches25 year storm event: 6.15 inches100-year storm event: 8.74 inches

An on-site conventional storm drainage collection system is designed based on the "Rational Method" using Manning's equation to carry a minimum 25-year storm event and underground culverts to carry a minimum 50-year storm event through the site (See Pipe Sizing Attachments). The proposed drainage pipes will be Reinforced Concrete Pipe (RCP), unless otherwise noted on the plans.

Compliance with the 10 Stormwater Standards

Standard 1: No new untreated Discharges

All Paved area runoff from the proposed development will flow across the pavement areas, accumulate into hooded catch basins, connect with drain pipe to a sediment forebay, which discharges to the infiltration basin. No new untreated stormwater discharges are proposed.

Standard 2: Peak Rate Attenuation

To meet Standard 2, the post-development peak discharge rate must be equal to or less than pre-development rates to prevent storm damage and downstream and offsite flooding from the 2-year and the 10-year 24-hour storm events. In addition, the Bellingham Wetlands Bylaws require that runoff volumes not exceed pre-development conditions for up to the 25year storm. Additionally, surface basins are to be sized assuming frozen conditions within the basin, with no infiltration during a 25-year storm event. Peak discharge rates were calculated and evaluated at Blackstone Street and the existing wetlands. The point of evaluation is shown on the accompanying watershed plans.

In summary of the attached drainage analysis (HydroCAD), the peak discharge rates (cfs) and Volumes (af) at the point of evaluation are as follows;

| | 2-yr Storm | 10-yr Storm | 25-yr Storm | 25-yr Storm | 100-yr Storm |
|-------------------------------|------------|-------------|-------------|--------------|--------------|
| | | | | Frozen Cond. | |
| Flow to Analysis Point (AP-1) | | | | | |
| Pre-Development | 0.0 cfs | 0.0 cfs | 1.65 cfs | 4.38 cfs | 19.70 cfs |
| Post-Development | 0.0 cfs | 0.0 cfs | 1.30 cfs | 4.34 cfs | 15.87 cfs |
| Flow to Analysis Point (AP-2) | | | | | |
| Pre-Development | 0.21 cfs | 1.43 cfs | 2.74 cfs | N/A | 5.94 cfs |
| Post-Development | 0.21 cfs | 1.42 cfs | 2.73 cfs | N/A | 5.90 cfs |

Table 1A: Peak Rate Attenuation Summary

Table 1B: Runoff Volume

| | 2-yr Storm | 10-yr Storm | 25-yr Storm | 25-yr Storm | 100-yr Storm |
|-------------------------------|------------|-------------|-------------|--------------|--------------|
| Flow to Analysis Point (AP-1) | | | | Frozen Cond. | |
| Pre-Development | 0.000 af | 0.00 af | 0.15 af | 1.39 af | 1.93 af |
| Post-Development | 0.000 af | 0.00 af | 0.12 af | 2.11 af | 1.34 af |
| Flow to Analysis Point (AP-2) | | | | | |
| Pre-Development | 0.05 af | 0.16 af | 0.28 af | N/A | 0.56 af |
| Post-Development | 0.05 af | 0.16 af | 0.28 af | N/A | 0.56 af |

In addition to peak rate attenuation and volume reduction, an on-site storm drain collection system was designed based on the "Rational Method" using Manning's equation to carry a minimum 25-year storm event through the site. The proposed drainage pipes will be Class V reinforced concrete pipe (RCP). On-site storm drainage calculations are included in Appendix 11 / Supplemental Attachments.

Standard 3: Recharge

Soil Evaluation

Soil evaluation is broken down into two stages. Stage 1 identifies the underlying soils just beneath the surface that contribute to how much runoff is generated as stormwater falls and moves across the surface. Stage 2 evaluates the soils in direct contact with the proposed infiltration BMPs. Appendix 2 includes the NRCS Soil Survey used for Stage 1 while Appendix 3 includes the on-site soil textural analysis in the specific locations that infiltration

is proposed. The information from the NRCS Soil Survey is on the Pre and Post Development drainage plans in Appendix 10.

Recharge Volume

The required recharge volume is determined by calculating the proposed impervious area over the corresponding soil identified in the NRCS Soil Survey. As previously stated, the NRCS Soil Survey lists the site as Canton Fine Sandy Loam, 0 to 8 percent slopes, HSG B, Canton Fine Sandy Loam, 3 to 8 percent slopes, HSG B, and Merrimac Fine Sandy Loam, 3 to 8 percent slopes, HSG B, and Merrimac Fine Sandy Loam, 3 to 8 percent slopes, the site consists of an existing undeveloped residential lot, the project is considered a new development project, as noted in Standard 7, therefore the recharge volume was calculated for the total impervious area.

| | Recharge | Impervious | Volume |
|--------------------------------|-----------|------------|----------|
| Hydrologic Group | (in/sqft) | (sqft) | (cf) |
| A - sand | 0.60 | 57,369 | 2,868 cf |
| B - loam | 0.35 | 0 | 0 |
| C - silty loam | 0.25 | None | 0 |
| D - clay | 0.10 | None | 0 |
| Required Recharge Volume Total | | | 2,868 cf |

Table 2: Required Recharge Volume Calculation

Stormwater Basin Sizing

There are three ways of determining the recharge volume provided by a storm water basin (Static, Simple Dynamic and Dynamic Field). The Static Method, used here, includes the volume of water that can be stored beneath the lowest outlet of the basin. This, the most conservative method of determining the recharge volume, does not account for any infiltration that takes place while the basin is filling with water and is less dependent on maintenance of the basin since the only way for the water below the lowest invert can leave the basin is though infiltration. The following table summarizes the recharge volume provided by the infiltration basin. Detailed volume calculations for the basins are included in Appendix 5 / Stage-Area-Storage Calculations.

Table 3: Basin Recharge Volume

| | Recharge Volume |
|---------|-----------------|
| Basin 1 | 17,862 cf |
| Total | 17,862 cf |

72-hour Drawdown

When using the conservative Static Method to determine infiltration volume provided, the Rawls Rate is used to represent the infiltration rate in place of a hydraulic conductivity rate. The specific rate chosen is based on the textural analysis of the in-situ soil performed by a competent soil professional.

A Massachusetts Certified Soil Evaluator performed an evaluation of the soil at the proposed infiltration BMP. The soil textural analysis for the infiltration BMP is listed below with the associated Rawls Rate used in the calculations. Where textural analysis varied within any single BMP, the most restrictive textural evaluation and Rawls Rate were used. Soil logs of the in-situ soil evaluation are included in Appendix 3 / Field Soils Evaluation.

Table 4: Rawls Rate

| | Most Restrictive Soil Texture | Rawls Rate (in/hour) |
|---------|----------------------------------|-------------------------|
| Basin 1 | Sand | 8.27 in/hr |

Drawdown time for the infiltration basin is determined by applying the Rawls Rate across the bottom area of the infiltration basin. The volume required for drawdown includes the entire volume below in the lowest outlet in the infiltration basin. The following table summarizes the drawdown time for the basin to show it will drawdown within the 72-hour maximum.

Table 5: Basin Drawdown

| | Storage Volume | Bottom Area | Time for Drawdown |
|---------|----------------|--------------------|-------------------|
| Basin 1 | 17,862 cf | 10,452 sf | 3 hours |

In addition, the HydroCAD model demonstrates that the proposed basin will fully dewater at the 26 hour mark during/after the 100-year design storm.

Standard 4: Water Quality

Water Quality Volume

The required water quality volume is determined through a calculation of the proposed impervious pavement throughout the site and a determination of whether the site is in a critical area, or the proposed use is considered to produce a high pollutant load. As noted in Standards 5 and 6, the land use does not qualify as a use with high pollutant load and no critical area was identified for this site. However, the required water quality volume is based on 1.0" as the soil recharge rate is 8.27 in/hr, meeting the threshold rate of 2.4 in/hr or greater, therefore, the water quality volume is calculated at 1.0" over the area of new proposed impervious pavement.

The area of impervious materials within the proposed site is calculated from the information entered HydroCAD and can be found in Appendix 4. One inch across 38,071 square feet of impervious pavement requires a water quality volume of 3,172.6 cubic feet. Detailed calculations for the infiltration basin are included in Appendix 5 / Stage-Area-Storage Calculations.

Removal of Total Suspended Solids

The water quality volume, as calculated in the previous section, is treated through "Treatment Trains" to provide a minimum of 80 percent TSS removal including 44 percent TSS removal for pretreatment prior to discharging to the infiltration BMP. The TSS Removal Worksheets are included in Appendix 6 for the proposed treatment train. The infiltration basin in conjunction with deep sump hooded catch basins and sediment forebay complete the treatment trains at a minimum of 80 percent and 44 percent TSS removal.

Forebay Sizing

All the stormwater from the impervious pavement is collected and discharged to the proposed sediment forebay which is sized to treat 0.1" of runoff from the 38,071-sf impervious area contributing to the basin. Detailed calculations for the sediment forebay are included in Appendix 5 / Stage-Area-Storage Calculations.

$0.1^{"}/12^{"}$ per foot x 38,071 sf = 317.3 cf of storage required

Table 6: Sediment Forebay Sizing

| | Impervious Area being Discharged | Required Volume | Provided Volume |
|------------------------|-------------------------------------|-----------------|-----------------|
| Forebay 1 @ Inv.=307.0 | 38,071 cf | 317.3 c.f. | 1,425c.f. |

Standard 5: Land Uses with Higher Potential Pollutant Loads

The proposed project is not a use that would qualify as a LUHPPL.

Standard 6: Critical Areas

The proposed project is not within, nor does it discharge stormwater to an identified Critical Area. However, the site does contain soils with rapid infiltration rates (>2.41 in/hr), and must meet the 1" WQV requirement of Standard 4.

Standard 7: Redevelopment Project

This project is not a redevelopment project.

Standard 8: Construction Period Controls

A Construction Period Pollution Control Plan is included in Appendix 8 will be followed to prevent discharge of erosion to abutting properties.

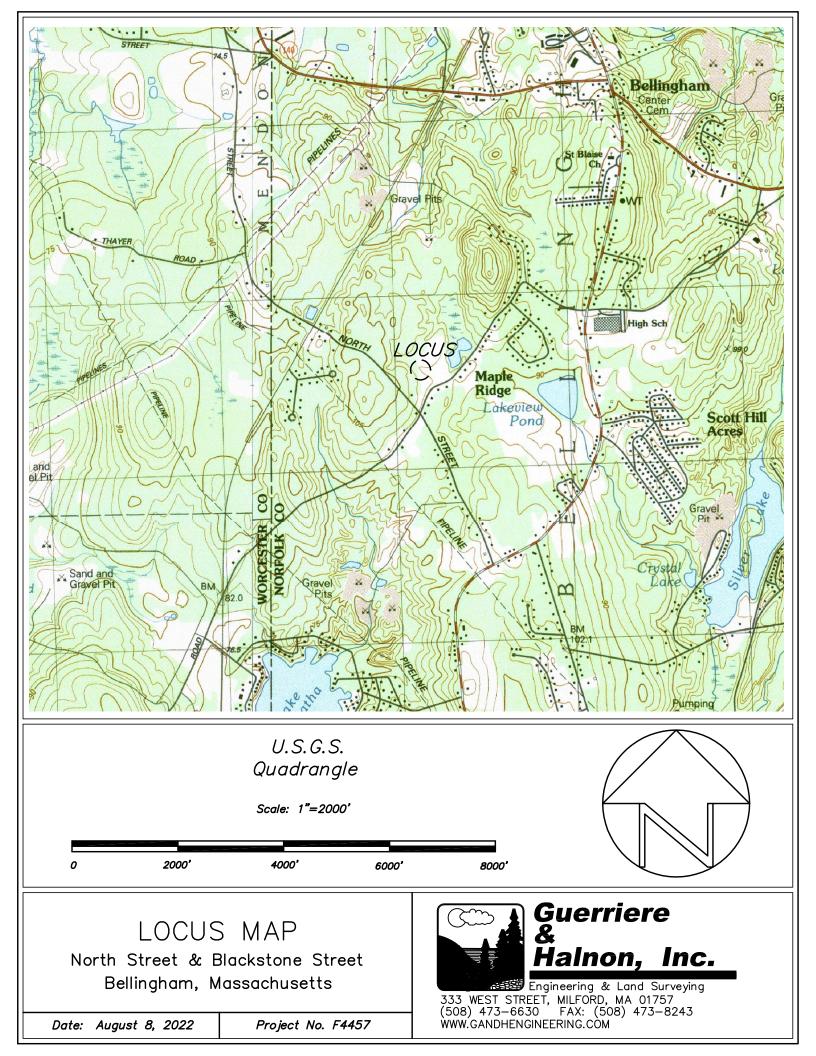
Standard 9: Operation and Maintenance Plan

The Operation and Maintenance Plan included in Appendix 7 address the responsibilities of maintaining the stormwater BMPs.

Standard 10: Illicit Discharges to Drainage System

It is the intent of the developer to follow the Construction Period Pollution Prevention Control Plan and the Order of Conditions to mitigate the affects of the proposed project on the adjacent environment. Following completion of construction, the Operation and Maintenance Plan will be provided to the property manager who will continue, the maintenance of the project. The Illicit Discharge Statement is included in Appendix 9.

<u>Locus Map</u> Appendix 1



NRCS Soils Report Appendix 2



United States Department of Agriculture

NRCS

Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for Norfolk and Suffolk Counties, Massachusetts

North Street & Blackstone Street



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/? cid=nrcs142p2_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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Contents

| Preface | 2 |
|---|-------------|
| How Soil Surveys Are Made | 5 |
| Soil Map | |
| Soil Map | 9 |
| Legend | 10 |
| Map Unit Legend | 11 |
| Map Unit Descriptions | 11 |
| Norfolk and Suffolk Counties, Massachusetts | |
| 53—Freetown muck, ponded, 0 to 1 percent slopes | 13 |
| 254B—Merrimac fine sandy loam, 3 to 8 percent slopes | 14 |
| 420B—Canton fine sandy loam, 3 to 8 percent slopes | 16 |
| 422B—Canton fine sandy loam, 0 to 8 percent slopes, extremely stony | <i>.</i> 18 |
| References | 20 |

How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



| | MAP L | EGEND | 1 | MAP INFORMATION | |
|-------------|--|---------------------|---|---|--|
| Area of Int | erest (AOI) Area of Interest (AOI) | 8 | Spoil Area Stony Spot | The soil surveys that comprise your AOI were mapped at 1:25,000. | |
| Soils | Soil Map Unit Polygons Soil Map Unit Lines | 00 V | Very Stony Spot Wet Spot | Warning: Soil Map may not be valid at this scale. Enlargement of maps beyond the scale of mapping can cause | |
| Special F | Soil Map Unit Points Point Features | ∆ ≁= Water Fe | Other Special Line Features | misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed | |
| 9 2 | Blowout Borrow Pit | Transport | Streams and Canals | scale. Please rely on the bar scale on each map sheet for map | |
| ☆ ※ | Clay Spot Closed Depression Gravel Pit | ∷ | Rails Interstate Highways | measurements. Source of Map: Natural Resources Conservation Service | |
| ™ ∴ © | Gravelly Spot Landfill | ~ ~ | US Routes Major Roads Local Roads | Web Soil Survey URL: Coordinate System: Web Mercator (EPSG:3857) Maps from the Web Soil Survey are based on the Web Mercator | |
| ٨. | Lava Flow Marsh or swamp | Backgrou | | projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. | |
| * 0 0 | Mine or Quarry Miscellaneous Water Perennial Water | | | This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. | |
| ~ + | Rock Outcrop Saline Spot | | | Soil Survey Area: Norfolk and Suffolk Counties, Massachusetts Survey Area Data: Version 17, Sep 3, 2021 | |
| :: = | Sandy Spot Severely Eroded Spot Sinkhole | | | Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. | |
| ବ ୬ ୭ | Slide or Slip Sodic Spot | | | Date(s) aerial images were photographed: May 24, 2020—Jul 18, 2020 | |
| <i>120</i> | | | | The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. | |

| Map Unit Symbol | Map Unit Name | Acres in AOI | Percent of AOI | | |
|-----------------------------|--|--------------|----------------|--|--|
| 53 | Freetown muck, ponded, 0 to 1 percent slopes | 2.0 | 9.5% | | |
| 254B | Merrimac fine sandy loam, 3 to 8 percent slopes | 12.8 | 61.3% | | |
| 420B | Canton fine sandy loam, 3 to 8 percent slopes | 1.3 | 6.1% | | |
| 422B | Canton fine sandy loam, 0 to 8 percent slopes, extremely stony | 4.8 | 23.1% | | |
| Totals for Area of Interest | | 20.8 | 100.0% | | |

Map Unit Legend

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Norfolk and Suffolk Counties, Massachusetts

53—Freetown muck, ponded, 0 to 1 percent slopes

Map Unit Setting

National map unit symbol: 2t2qc Elevation: 0 to 1,140 feet Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 140 to 240 days Farmland classification: Not prime farmland

Map Unit Composition

Freetown, ponded, and similar soils: 85 percent *Minor components:* 15 percent *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of Freetown, Ponded

Setting

Landform: Kettles, marshes, depressions, depressions, bogs, swamps Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Tread, dip Down-slope shape: Concave Across-slope shape: Concave Parent material: Highly decomposed organic material

Typical profile

Oe - 0 to 2 inches: mucky peat *Oa - 2 to 79 inches:* muck

Properties and qualities

Slope: 0 to 1 percent
Surface area covered with cobbles, stones or boulders: 0.0 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Very poorly drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high (0.14 to 14.17 in/hr)
Depth to water table: About 0 to 6 inches
Frequency of flooding: Rare
Frequency of ponding: Frequent
Available water supply, 0 to 60 inches: Very high (about 19.2 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 5w Hydrologic Soil Group: B/D Ecological site: F144AY043MA - Acidic Organic Wetlands Hydric soil rating: Yes

Minor Components

Whitman, ponded

Percent of map unit: 5 percent Landform: Depressions on ground moraines Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Base slope Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

Scarboro

Percent of map unit: 5 percent Landform: Drainageways, depressions Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Base slope, tread, dip Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

Swansea, ponded

Percent of map unit: 5 percent Landform: Bogs, swamps, marshes, depressions, depressions, kettles Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Tread, dip Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

254B—Merrimac fine sandy loam, 3 to 8 percent slopes

Map Unit Setting

National map unit symbol: 2tyqs Elevation: 0 to 1,290 feet Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 140 to 240 days Farmland classification: All areas are prime farmland

Map Unit Composition

Merrimac and similar soils: 85 percent *Minor components:* 15 percent *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of Merrimac

Setting

Landform: Outwash plains, outwash terraces, moraines, eskers, kames Landform position (two-dimensional): Summit, shoulder, backslope, footslope Landform position (three-dimensional): Crest, side slope, riser, tread Down-slope shape: Convex Across-slope shape: Convex

Parent material: Loamy glaciofluvial deposits derived from granite, schist, and gneiss over sandy and gravelly glaciofluvial deposits derived from granite, schist, and gneiss

Typical profile

Ap - 0 to 10 inches: fine sandy loam *Bw1 - 10 to 22 inches:* fine sandy loam *Bw2 - 22 to 26 inches:* stratified gravel to gravelly loamy sand *2C - 26 to 65 inches:* stratified gravel to very gravelly sand

Properties and qualities

Slope: 3 to 8 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Somewhat excessively drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very high (1.42 to 99.90 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 2 percent
Maximum salinity: Nonsaline (0.0 to 1.4 mmhos/cm)
Sodium adsorption ratio, maximum: 1.0
Available water supply, 0 to 60 inches: Low (about 4.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2s Hydrologic Soil Group: A Ecological site: F145XY008MA - Dry Outwash Hydric soil rating: No

Minor Components

Hinckley

Percent of map unit: 5 percent Landform: Deltas, kames, eskers, outwash plains Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Head slope, nose slope, crest, side slope, rise Down-slope shape: Convex Across-slope shape: Convex, linear Hydric soil rating: No

Sudbury

Percent of map unit: 5 percent Landform: Deltas, terraces, outwash plains Landform position (two-dimensional): Footslope Landform position (three-dimensional): Tread, dip Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

Windsor

Percent of map unit: 3 percent Landform: Outwash terraces, dunes, deltas, outwash plains Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Tread, riser Down-slope shape: Linear, convex Across-slope shape: Linear, convex Hydric soil rating: No

Agawam

Percent of map unit: 2 percent Landform: Outwash plains, outwash terraces, moraines, stream terraces, eskers, kames Landform position (three-dimensional): Rise Down-slope shape: Convex Across-slope shape: Convex

Hydric soil rating: No

420B—Canton fine sandy loam, 3 to 8 percent slopes

Map Unit Setting

National map unit symbol: 2w81b Elevation: 0 to 1,180 feet Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 140 to 240 days Farmland classification: All areas are prime farmland

Map Unit Composition

Canton and similar soils: 80 percent *Minor components:* 20 percent *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of Canton

Setting

Landform: Hills, moraines, ridges Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Nose slope, side slope, crest Down-slope shape: Convex, linear Across-slope shape: Convex Parent material: Coarse-loamy over sandy melt-out till derived from gneiss, granite, and/or schist

Typical profile

Ap - 0 to 7 inches: fine sandy loam Bw1 - 7 to 15 inches: fine sandy loam Bw2 - 15 to 26 inches: gravelly fine sandy loam 2C - 26 to 65 inches: gravelly loamy sand

Properties and qualities

Slope: 3 to 8 percent
Depth to restrictive feature: 19 to 39 inches to strongly contrasting textural stratification
Drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high (0.14 to 14.17 in/hr)

Depth to water table: More than 80 inches Frequency of flooding: None Frequency of ponding: None Available water supply, 0 to 60 inches: Very low (about 2.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2s Hydrologic Soil Group: B Ecological site: F144AY034CT - Well Drained Till Uplands Hydric soil rating: No

Minor Components

Scituate

Percent of map unit: 10 percent Landform: Hills, drumlins, ground moraines Landform position (two-dimensional): Summit, backslope, footslope Landform position (three-dimensional): Side slope, crest Down-slope shape: Convex, linear Across-slope shape: Convex Hydric soil rating: No

Montauk

Percent of map unit: 5 percent Landform: Moraines, ground moraines, hills, drumlins Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Side slope, crest Down-slope shape: Convex, linear Across-slope shape: Convex Hydric soil rating: No

Charlton

Percent of map unit: 4 percent Landform: Ridges, ground moraines, hills Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Side slope, crest Down-slope shape: Convex, linear Across-slope shape: Convex Hydric soil rating: No

Swansea

Percent of map unit: 1 percent Landform: Marshes, depressions, bogs, swamps, kettles Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

422B—Canton fine sandy loam, 0 to 8 percent slopes, extremely stony

Map Unit Setting

National map unit symbol: 2w818 Elevation: 0 to 1,180 feet Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 145 to 240 days Farmland classification: Not prime farmland

Map Unit Composition

Canton, extremely stony, and similar soils: 80 percent *Minor components:* 20 percent *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of Canton, Extremely Stony

Setting

Landform: Moraines, hills, ridges Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Nose slope, side slope, crest Down-slope shape: Convex, linear Across-slope shape: Convex Parent material: Coarse-loamy over sandy melt-out till derived from gneiss, granite, and/or schist

Typical profile

Oi - 0 to 2 inches: slightly decomposed plant material *A - 2 to 5 inches:* fine sandy loam *Bw1 - 5 to 16 inches:* fine sandy loam *Bw2 - 16 to 22 inches:* gravelly fine sandy loam *2C - 22 to 67 inches:* gravelly loamy sand

Properties and qualities

Slope: 0 to 8 percent
Surface area covered with cobbles, stones or boulders: 9.0 percent
Depth to restrictive feature: 19 to 39 inches to strongly contrasting textural stratification
Drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high (0.14 to 14.17 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)
Available water supply, 0 to 60 inches: Low (about 3.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s Hydrologic Soil Group: B Ecological site: F144AY034CT - Well Drained Till Uplands Hydric soil rating: No

Minor Components

Charlton, extremely stony

Percent of map unit: 6 percent Landform: Ridges, ground moraines, hills Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Side slope, crest Down-slope shape: Convex, linear Across-slope shape: Convex Hydric soil rating: No

Scituate, extremely stony

Percent of map unit: 6 percent Landform: Hills, ground moraines, drumlins Landform position (two-dimensional): Summit, backslope, footslope Landform position (three-dimensional): Side slope, crest Down-slope shape: Convex, linear Across-slope shape: Convex Hydric soil rating: No

Swansea

Percent of map unit: 4 percent Landform: Marshes, depressions, bogs, swamps, kettles Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

Montauk, extremely stony

Percent of map unit: 4 percent Landform: Recessionial moraines, ground moraines, hills, drumlins Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Side slope, crest Down-slope shape: Convex, linear Across-slope shape: Convex Hydric soil rating: No

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Field Soils Evaluation Appendix 3



Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

Deep Observation Hole Number: DTH #1

| Depth | Soil Horizon/ Layer | Soil Matrix: Color-Moist (Munsell) | Redo | oximorphic Fea (mottles) | tures | Soil Texture (USDA) | Coarse Fragments % by Volume | | Soil Structure | Soil Consistence (Moist) | Other |
|--------|---------------------------|--|-------|-----------------------------|---------|---------------------------|---------------------------------|---------------------|----------------|--------------------------------|-------|
| (In.) | | | Depth | Color | Percent | | Gravel | Cobbles & Stones | | | |
| 0-10 | А | 10YR 3/3 | - | - | - | S.L. | 0 | 0 | - | - | - |
| 10-30 | В | 10YR 5/6 | - | - | - | S.L. | 0 | 0 | - | - | - |
| 30-108 | С | 2.5Y 5/4 | - | - | - | SAND | 20 | 20 | - | - | - |
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Additional Notes WEEPING @ 96"



Deep Observation Hole Number: DTH #2

| Depth | Soil Horizon/ Layer | Soil Matrix: Color-Moist (Munsell) | Redo | ximorphic Fea (mottles) | tures | Soil Texture (USDA) | ure % by Volume DA) | | Soil Structure | Soil Consistence (Moist) | Other |
|--------|---------------------------|--|-------|----------------------------|---------|---------------------------|------------------------|---------------------|----------------|--------------------------------|-------|
| (In.) | | | Depth | Color | Percent | | Gravel | Cobbles & Stones | | | |
| 0-10 | А | 10YR 3/3 | - | - | - | S.L. | 0 | 0 | - | - | - |
| 10-20 | В | 10YR 5/6 | - | - | - | S.L. | 0 | 0 | - | - | - |
| 20-136 | С | 2.5Y 5/4 | - | - | - | SAND | 20 | 20 | - | - | - |
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Additional Notes WEEPING @ 126"



Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

Deep Observation Hole Number: DTH-3

| Depth | Soil Horizon/ Layer | Soil Matrix: Color-Moist (Munsell) | Redo | oximorphic Fea (mottles) | tures | Soil Texture (USDA) | Coarse Fragments % by Volume | | Soil Structure | Soil Consistence (Moist) | Other |
|--------|---------------------------|--|-------|-----------------------------|---------|---------------------------|---------------------------------|---------------------|----------------|--------------------------------|-------|
| (In.) | | | Depth | Color | Percent | | Gravel | Cobbles & Stones | | | |
| 0-8 | А | 10YR 3/3 | - | - | - | S.L. | 0 | 0 | - | - | - |
| 8-30 | В | 10YR 5/6 | - | - | - | S.L. | 0 | 0 | - | - | - |
| 30-130 | С | 2.5Y 5/4 | - | - | - | SAND | 20 | 20 | - | - | - |
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Additional Notes NO MOTTLES / WEEPING



Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

Deep Observation Hole Number: DTH #4

| Depth | Depth (In) Soil Soil Matrix: Horizon/ Layer (Munsell) | | Redoximorphic Features (mottles) | | | Soil Texture (USDA) | Coarse F % by \ | ragments /olume | Soil Structure | Soil Consistence (Moist) | Other |
|--------|---|----------|-------------------------------------|-------|---------|---------------------------|--------------------|---------------------|----------------|--------------------------------|-------|
| (In.) | | | Depth | Color | Percent | | Gravel | Cobbles & Stones | | | |
| 0-8 | А | 10YR 3/3 | - | - | - | S.L. | 0 | 0 | - | - | - |
| 8-26 | В | 10YR 5/6 | - | - | - | S.L. | 0 | 0 | - | - | - |
| 26-156 | С | 2.5Y 5/4 | - | - | - | SAND | 20 | 20 | - | - | - |
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Additional Notes WEEPING @ 156"



Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

Deep Observation Hole Number: DTH #5

| Depth | Soil Soil Matrix: Horizon/ Color-Moist Layer (Munsell) | | Redoximorphic Features (mottles) | | | Soil Texture (USDA) | Coarse F % by \ | ragments /olume | Soil Structure | Soil Consistence (Moist) | Other |
|--------|--|----------|-------------------------------------|-------|---------|---------------------------|--------------------|---------------------|----------------|--------------------------------|-------|
| (ln.) | | | Depth | Color | Percent | | Gravel | Cobbles & Stones | | | |
| 0-6 | А | 10YR 3/3 | - | - | - | S.L. | 0 | 0 | - | - | - |
| 6-18 | В | 10YR 5/6 | - | - | - | S.L. | 0 | 0 | - | - | - |
| 18-190 | С | 2.5Y 5/4 | - | - | - | SAND | 20 | 20 | - | - | - |
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Additional Notes WEEPING @ 190"



Deep Observation Hole Number: DTH #6

| Soil Horizon/ Layer | Soil Matrix: Color-Moist (Munsell) | ist (mottles) | | | Soil Texture (USDA) | % by Volume | | Soil Structure | Soil Consistence (Moist) | Other |
|---------------------------|--|---|--|--|---|---|---|--|---|---|
| | | Depth | Color | Percent | . , | Gravel | Cobbles & Stones | | . , | |
| A | 10YR 3/3 | - | - | - | S.L. | 0 | 0 | - | - | - |
| В | 10YR 5/6 | - | - | - | S.L. | 0 | 0 | - | - | - |
| С | 2.5Y 5/4 | - | - | - | SAND | 20 | 20 | - | - | - |
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| | Horizon/ Layer A B | Horizon/ LayerColor-Moist (Munsell)A10YR 3/3B10YR 5/6 | Horizon/ LayerColor-Moist (Munsell)DepthA10YR 3/3B10YR 5/6 | Horizon/ LayerColor-Moist (Munsell)(mottles)DepthColorA10YR 3/3-B10YR 5/6- | Horizon/ LayerColor-Moist (Munsell)(mottles)DepthColorPercentA10YR 3/3B10YR 5/6 | Horizon/ LayerColor-Moist (Munsell)(mottles)Texture (USDA) A 10YR 3/3 $ B$ 10YR 5/6 $ S.L.$ | Horizon/ LayerColor-Moist (Munsell)(mottles)Texture (USDA)% by M | Horizon/ LayerColor-Moist (Munsell)(mottles)Texture (USDA)% by Volume \overline{Depth} ColorPercent \overline{Gravel} Cobbles & StonesA10YR 3/3S.L.00B10YR 5/6S.L.00 | Horizon/ LayerColor-Moist (Munsell)(mottles)Texture (USDA)% by Volume \overline{Depth} ColorPercent \overline{Gravel} Cobbles & StonesA10YR 3/3S.L.00B10YR 5/6S.L.00- | Horizon/ LayerColor-Moist (Munsell)Image: mottles)Texture (USDA)% by VolumeCobbles & StonesConsistence (Moist)A10YR 3/3S.L.00B10YR 5/6S.L.00 |

Additional Notes NO MOTTLES OR WEEPING



Deep Observation Hole Number: DTH #7

| Soil Horizon/ Layer | Soil Matrix: Color-Moist (Munsell) | st (mottles) | | | Soil Texture (USDA) | % by Volume | | Soil Structure | Soil Consistence (Moist) | Other |
|---------------------------|--|---|--|--|---|--|---|--|---|---|
| | | Depth | Color | Percent | , , | Gravel | Cobbles & Stones | | . , | |
| А | 10YR 3/3 | - | - | - | S.L. | 0 | 0 | - | - | - |
| В | 10YR 5/6 | - | - | - | S.L. | 0 | 0 | - | - | - |
| С | 2.5Y 5/4 | - | - | - | L.S. | 20 | 20 | - | - | - |
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| | Horizon/ Layer A B | Horizon/ LayerColor-Moist (Munsell)A10YR 3/3B10YR 5/6 | Horizon/ LayerColor-Moist (Munsell)A10YR 3/3A10YR 5/6B10YR 5/6 | Horizon/ LayerColor-Moist (Munsell)(mottles)DepthColorA10YR 3/3-B10YR 5/6- | Horizon/ LayerColor-Moist (Munsell)(mottles)DepthColorPercentA10YR 3/3B10YR 5/6 | Horizon/ LayerColor-Moist (Munsell)(mottles)Texture (USDA) $Depth$ ColorPercentA10YR 3/3B10YR 5/6S.L. | Horizon/ LayerColor-Moist (Munsell)(mottles)Texture (USDA)% by Y \overline{Depth} ColorPercent \overline{Color} $Colo$ | Horizon/ LayerColor-Moist (Munsell)(mottles)Texture (USDA)% by Volume \overline{Depth} ColorPercent \overline{Gravel} Cobbles & StonesA10YR 3/3S.L.00B10YR 5/6S.L.00 | Horizon/ LayerColor-Moist (Munsell)(mottles)Texture (USDA)% by VolumeDepthColorPercentGravelCobbles & StonesA10YR 3/3S.L.00B10YR 5/6S.L.00- | Horizon/ LayerColor-Moist (Munsell)(mottles)Texture (USDA)% by VolumeConsistence (Moist)Consistence (Moist)A10YR 3/3-ColorPercentS.L.00B10YR 5/6S.L.00 |

Additional Notes NO MOTTLES OR WEEPING



Deep Observation Hole Number: DTH #8

| Depth | Soil Horizon/ Layer | Soil Matrix: Color-Moist (Munsell) | t (mottles) | | | Soil Texture (USDA) | Coarse F % by V | ragments /olume | Soil Structure | Soil Consistence (Moist) | Other |
|--------|---------------------------|--|-------------|-------|---------|---------------------------|--------------------|---------------------|----------------|--------------------------------|-------|
| (ln.) | | . , | Depth | Color | Percent | , , | Gravel | Cobbles & Stones | | . , | |
| 0-8 | А | 10YR 3/3 | - | - | - | S.L. | 0 | 0 | - | - | - |
| 8-24 | В | 10YR 5/6 | - | - | - | S.L. | 0 | 0 | - | - | - |
| 24-103 | С | 2.5Y 5/4 | - | - | - | SAND | 20 | 20 | - | - | - |
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Additional Notes WATER @ 92"



Deep Observation Hole Number: DTH #9

| Depth | Soil Horizon/ Layer | Soil Matrix: Color-Moist (Munsell) | Redoximorphic Features (mottles) | | | Soil Texture (USDA) | Coarse F % by V | Fragments Volume | Soil Structure | Soil Consistence (Moist) | Other |
|--------|---------------------------|--|-------------------------------------|-------|---------|---------------------------|--------------------|---------------------|----------------|--------------------------------|-------|
| (ln.) | | | Depth | Color | Percent | . , | Gravel | Cobbles & Stones | | . , | |
| 0-48 | F | - | - | - | - | - | - | - | - | - | - |
| 48-108 | С | 2.5Y 5/4 | - | - | - | SAND | 20 | 20 | - | - | - |
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Additional Notes WEEPING @ 80"



Deep Observation Hole Number: DTH #10

| Depth | Soil Horizon/ Layer | Soil Matrix: Color-Moist (Munsell) | Redoximorphic Features (mottles) | | | Soil Texture (USDA) | Coarse F % by \ | ragments /olume | Soil Structure | Soil Consistence (Moist) | Other |
|--------|---------------------------|--|-------------------------------------|-------|---------|---------------------------|--------------------|---------------------|----------------|--------------------------------|-------|
| (ln.) | | . , | Depth | Color | Percent | . , | Gravel | Cobbles & Stones | | | |
| 0-14 | А | 10YR 3/3 | - | - | - | S.L. | 0 | 0 | - | - | - |
| 14-28 | В | 10YR 5/6 | - | - | - | S.L. | 0 | 0 | - | - | - |
| 28-42 | C1 | 2.5Y 6/2 | - | - | - | S.L. | 0 | 0 | - | - | - |
| 42-100 | C2 | 2.5Y 5/4 | 48" | - | - | SAND | 20 | 20 | - | - | - |
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Additional Notes WEEPING @ 86"



Deep Observation Hole Number: DTH #11

| Soil Horizon/ Layer | Soil Matrix: Color-Moist (Munsell) | bist (mottles) | | | Soil Texture (USDA) | Coarse Fragments % by Volume | | Soil Structure | Soil Consistence (Moist) | Other |
|---------------------------|--|---|--|--|---|---|--|--|---|---|
| | | Depth | Color | Percent | , , | Gravel | Cobbles & Stones | | . , | |
| А | 10YR 3/3 | - | - | - | S.L. | 0 | 0 | - | - | - |
| В | 10YR 5/6 | - | - | - | S.L. | 0 | 0 | - | - | - |
| С | 2.5Y 5/4 | - | - | - | SAND | 20 | 20 | - | - | - |
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| | Horizon/ Layer A B | Horizon/ LayerColor-Moist (Munsell)A10YR 3/3B10YR 5/6 | Horizon/ LayerColor-Moist (Munsell)DepthA10YR 3/3B10YR 5/6 | Horizon/ LayerColor-Moist (Munsell)(mottles)DepthColorA10YR 3/3-B10YR 5/6- | Horizon/ LayerColor-Moist (Munsell)(mottles)DepthColorPercentA10YR 3/3B10YR 5/6 | Horizon/ LayerColor-Moist (Munsell)(mottles)Texture (USDA)DepthColorPercentA10YR 3/3B10YR 5/6S.L.UUUUU | Horizon/ LayerColor-Moist (Munsell)(mottles)Texture (USDA)% by Y \overline{Depth} ColorPercent \overline{COD} \overline{Cravel} \overline{A} 10YR 3/3 $S.L.$ 0 \overline{B} 10YR 5/6 $S.L.$ 0 | Horizon/ LayerColor-Moist (Munsell)(mottles)Texture (USDA)% by Volume \overline{Depth} ColorPercent \overline{Gravel} Cobbles & StonesA10YR 3/3S.L.00B10YR 5/6S.L.00 | Horizon/ LayerColor-Moist (Munsell)(mottles)Texture (USDA)% by Volume \overline{Depth} ColorPercent \overline{Gravel} Cobbles & StonesA10YR 3/3S.L.00B10YR 5/6S.L.00- | Horizon/ LayerColor-Moist (Munsell)(mottles)Texture (USDA)% by VolumeCobbles & StonesConsistence (Moist)A10YR 3/3S.L.00B10YR 5/6S.L.00 |

Additional Notes WEEPING @ 96"



Deep Observation Hole Number: DTH #12

| Depth | Soil Horizon/ Layer | Soil Matrix: Color-Moist (Munsell) | st (mottles)) | | | Soil Texture (USDA) | Coarse F % by V | ragments /olume | Soil Structure | Soil Consistence (Moist) | Other |
|--------|---------------------------|--|-------------------|-------|---------|---------------------------|--------------------|---------------------|----------------|--------------------------------|-------|
| (ln.) | | | Depth | Color | Percent | , , , | Gravel | Cobbles & Stones | | | |
| 0-12 | А | 10YR 3/3 | - | - | - | S.L. | 0 | 0 | - | - | - |
| 12-104 | С | 2.5Y 5/4 | - | - | - | SAND | 20 | 20 | - | - | - |
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Additional Notes WEEPING @ 90"



Deep Observation Hole Number: DTH #13

| Depth | Soil Horizon/ Layer | Soil Matrix: Color-Moist (Munsell) | Redo | oximorphic Fea (mottles) | itures | Soil Texture (USDA) | Coarse Fragments % by Volume | | Soil Structure | | Other |
|--------|---------------------------|--|-------|-----------------------------|---------|---------------------------|---------------------------------|---------------------|----------------|-----|-------|
| (ln.) | | | Depth | Color | Percent | | Gravel | Cobbles & Stones | | . , | |
| 0-12 | А | 10YR 3/3 | - | - | - | S.L. | 0 | 0 | - | - | - |
| 12-24 | В | 10YR 5/6 | - | - | - | S.L. | 0 | 0 | - | - | - |
| 24-103 | С | 2.5Y 5/4 | - | - | - | SAND | 20 | 20 | - | - | - |
| | | | | | | | | | | | |
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Additional Notes STANDING WATER @ 100"

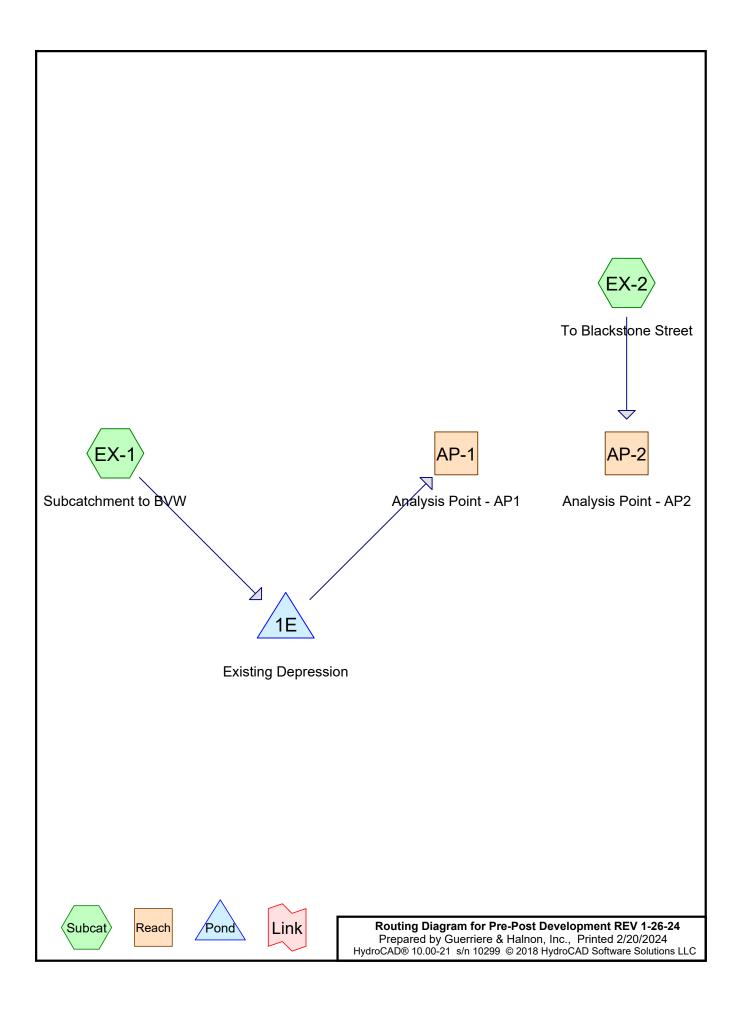


Deep Observation Hole Number: DTH #14

| Depth | Soil Horizon/ Layer | Soil Matrix: Color-Moist (Munsell) | Redo | ximorphic Fea (mottles) | atures | Soil Texture (USDA) | Coarse Fragments % by Volume | | Soil Structure Soil Consister (Moist) | | e Other |
|--------|---------------------------|--|-------|----------------------------|---------|---------------------------|---------------------------------|---------------------|---|---|---------|
| (In.) | | | Depth | Color | Percent | . , | Gravel | Cobbles & Stones | | | |
| 0-6 | А | 10YR 3/3 | - | - | - | S.L. | 0 | 0 | - | - | - |
| 6-30 | В | 10YR 5/6 | - | - | - | S.L. | 0 | 0 | - | - | - |
| 30-114 | С | 2.5Y 5/4 | - | - | - | SAND | 20 | 20 | - | - | - |
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Additional Notes WEEPING @ 100"

HydroCAD Calculations Appendix 4



Pre-Post Development REV 1-26-24 Prepared by Guerriere & Halnon, Inc. HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD Software Solutions LLC

Area Listing (selected nodes)

| Area | CN | Description | |
|---------|----|--|--|
| (acres) | | (subcatchment-numbers) | |
| 3.753 | 39 | >75% Grass cover, Good, HSG A (EX-1, EX-2) | |
| 0.860 | 61 | >75% Grass cover, Good, HSG B (EX-1, EX-2) | |
| 0.646 | 98 | Water Surface, HSG A (EX-1) | |
| 2.399 | 30 | Woods, Good, HSG A (EX-1, EX-2) | |
| 13.720 | 55 | Woods, Good, HSG B (EX-1, EX-2) | |
| 21.377 | 51 | TOTAL AREA | |

Pre-Post Development REV 1-26-24 Prepared by Guerriere & Halnon, Inc. HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD Software Solutions LLC

Soil Listing (selected nodes)

| Area | Soil | Subcatchment |
|---------|-------|--------------|
| (acres) | Group | Numbers |
| 6.798 | HSG A | EX-1, EX-2 |
| 14.579 | HSG B | EX-1, EX-2 |
| 0.000 | HSG C | |
| 0.000 | HSG D | |
| 0.000 | Other | |
| 21.377 | | TOTAL AREA |
| | | |

Pre-Post Development REV 1-26-24

| Prepared by Guerrier | re & Halnon, Inc. | |
|----------------------|--------------------------------|-------------------|
| HydroCAD® 10.00-21 s | /n 10299 © 2018 HydroCAD Softw | are Solutions LLC |

Printed 2/20/2024 Page 4

| HSG-A (acres) | HSG-B (acres) | HSG-C (acres) | HSG-D (acres) | Other (acres) | Total (acres) | Ground Cover | Subcatchment Numbers |
|----------------------|------------------|------------------|------------------|------------------|------------------|------------------------|-------------------------|
| 3.753 | 0.860 | 0.000 | 0.000 | 0.000 | 4.612 | >75% Grass cover, Good | EX-1, |
| | | | | | | | EX-2 |
| 0.646 | 0.000 | 0.000 | 0.000 | 0.000 | 0.646 | Water Surface | EX-1 |
| 2.399 | 13.720 | 0.000 | 0.000 | 0.000 | 16.119 | Woods, Good | EX-1, |
| | | | | | | | EX-2 |
| 6.798 | 14.579 | 0.000 | 0.000 | 0.000 | 21.377 | TOTAL AREA | |

Ground Covers (selected nodes)

| Pre-Post Development REV 1-26-24 Prepared by Guerriere & Halnon, Inc. HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD | NRCC 24-hr C 2-Year Rainfall=3.26" Printed 2/20/2024 Software Solutions LLC Page 5 |
|--|---|
| Runoff by SCS TR-20 m | hrs, dt=0.05 hrs, 1441 points hethod, UH=SCS, Weighted-CN hod - Pond routing by Dyn-Stor-Ind method |
| | off Area=844,997 sf 3.33% Impervious Runoff Depth=0.14" gth=1,712' Tc=41.8 min CN=50 Runoff=0.41 cfs 0.228 af |
| | noff Area=86,206 sf 0.00% Impervious Runoff Depth=0.30" ength=586' Tc=15.6 min CN=56 Runoff=0.21 cfs 0.049 af |
| Reach AP-1: Analysis Point - AP1 | Inflow=0.00 cfs 0.000 af Outflow=0.00 cfs 0.000 af |
| Reach AP-2: Analysis Point - AP2 | Inflow=0.21 cfs 0.049 af Outflow=0.21 cfs 0.049 af |
| | |

Pond 1E: Existing DepressionPeak Elev=307.63' Storage=903 cfInflow=0.41 cfs0.228 afDiscarded=0.31 cfs0.228 afPrimary=0.00 cfs0.000 afOutflow=0.31 cfs0.228 af

Total Runoff Area = 21.377 acRunoff Volume = 0.277 afAverage Runoff Depth = 0.16"96.98% Pervious = 20.731 ac3.02% Impervious = 0.646 ac

Pre-Post Development REV 1-26-24

Prepared by Guerriere & Halnon, Inc. HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD Software Solutions LLC

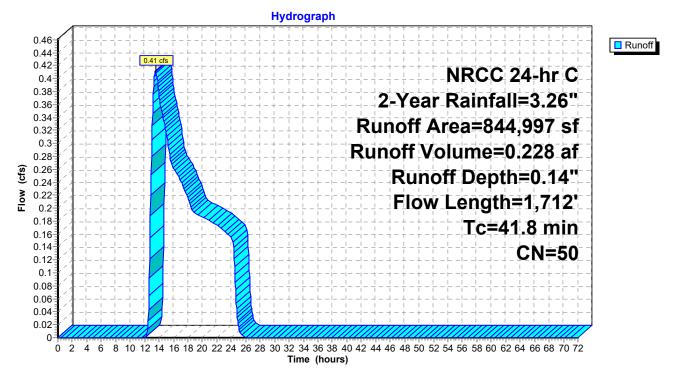
Summary for Subcatchment EX-1: Subcatchment to BVW

Runoff = 0.41 cfs @ 13.52 hrs, Volume= 0.228 af, Depth= 0.14"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 2-Year Rainfall=3.26"

| A | rea (sf) | CN E | Description | | | | |
|-------|----------|---------|--------------------|-------------|--|--|--|
| 5 | 28,369 | 55 V | Woods, Good, HSG B | | | | |
| | 20,766 | 61 > | 75% Gras | s cover, Go | bod, HSG B | | |
| 1 | 63,331 | 39 > | 75% Gras | s cover, Go | bod, HSG A | | |
| 1 | 04,370 | 30 V | Voods, Go | od, HSG A | | | |
| | 28,161 | 98 V | Vater Surfa | ace, HSG A | ι | | |
| 8 | 44,997 | 50 V | Veighted A | verage | | | |
| 8 | 16,836 | ç | 96.67% Pei | vious Area | | | |
| | 28,161 | 3 | 8.33% Impe | ervious Are | а | | |
| | | | | | | | |
| Tc | Length | Slope | Velocity | Capacity | Description | | |
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | | | |
| 7.0 | 50 | 0.0800 | 0.12 | | Sheet Flow, Segment A-B | | |
| | | | | | Woods: Light underbrush n= 0.400 P2= 3.26" | | |
| 0.9 | 78 | 0.0800 | 1.41 | | Shallow Concentrated Flow, Segment B-C | | |
| | | | | | Woodland Kv= 5.0 fps | | |
| 12.7 | 592 | 0.0240 | 0.77 | | Shallow Concentrated Flow, Segment C-D | | |
| | | | | | Woodland Kv= 5.0 fps | | |
| 14.1 | 581 | 0.0190 | 0.69 | | Shallow Concentrated Flow, Segment D-E | | |
| | | | | | Woodland Kv= 5.0 fps | | |
| 7.1 | 411 | 0.0190 | 0.96 | | Shallow Concentrated Flow, Segment E-F | | |
| | | | | | Short Grass Pasture Kv= 7.0 fps | | |
| 41.8 | 1,712 | Total | | | | | |

Subcatchment EX-1: Subcatchment to BVW



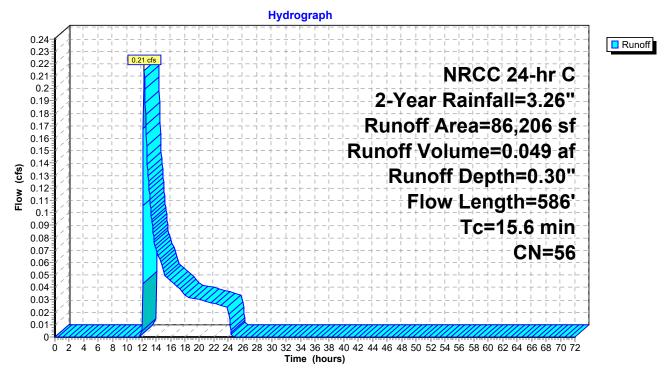
Summary for Subcatchment EX-2: To Blackstone Street

Runoff = 0.21 cfs @ 12.36 hrs, Volume= 0.049 af, Depth= 0.30"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 2-Year Rainfall=3.26"

| A | rea (sf) | CN I | Description | | |
|-------|----------|---------|-------------|-------------|--|
| | 69,268 | 55 | Noods, Go | od, HSG B | |
| | 16,676 | 61 : | >75% Gras | s cover, Go | bod, HSG B |
| | 131 | 39 : | >75% Gras | s cover, Go | bod, HSG A |
| | 131 | 30 | Noods, Go | od, HSG A | |
| | 86,206 | 56 | Neighted A | verage | |
| | 86,206 | | 100.00% Pe | ervious Are | a |
| | | | | | |
| Tc | Length | Slope | | Capacity | Description |
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | |
| 7.8 | 50 | 0.0610 | 0.11 | | Sheet Flow, Segment A-B |
| | | | | | Woods: Light underbrush n= 0.400 P2= 3.26" |
| 2.8 | 215 | 0.0640 | 1.26 | | Shallow Concentrated Flow, Segment B-C |
| | | | | | Woodland Kv= 5.0 fps |
| 2.2 | 103 | 0.0240 | 0.77 | | Shallow Concentrated Flow, Segment C-D |
| | | | | | Woodland Kv= 5.0 fps |
| 2.8 | 218 | 0.0340 | 1.29 | | Shallow Concentrated Flow, Segment D-E |
| | | | | | Short Grass Pasture Kv= 7.0 fps |
| 15.6 | 586 | Total | | | |

Subcatchment EX-2: To Blackstone Street



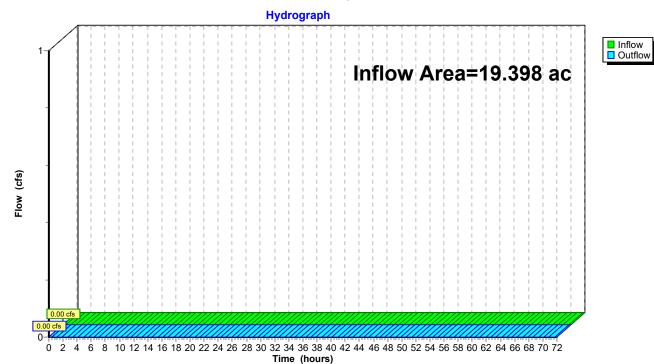
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Summary for Reach AP-1: Analysis Point - AP1

[40] Hint: Not Described (Outflow=Inflow)

| Inflow Area = | 19.398 ac, | 3.33% Impervious, I | nflow Depth = 0.00 | " for 2-Year event |
|---------------|------------|---------------------|--------------------|-------------------------|
| Inflow = | 0.00 cfs @ | 0.00 hrs, Volume= | 0.000 af | |
| Outflow = | 0.00 cfs @ | 0.00 hrs, Volume= | 0.000 af, <i>A</i> | Atten= 0%, Lag= 0.0 min |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



Reach AP-1: Analysis Point - AP1

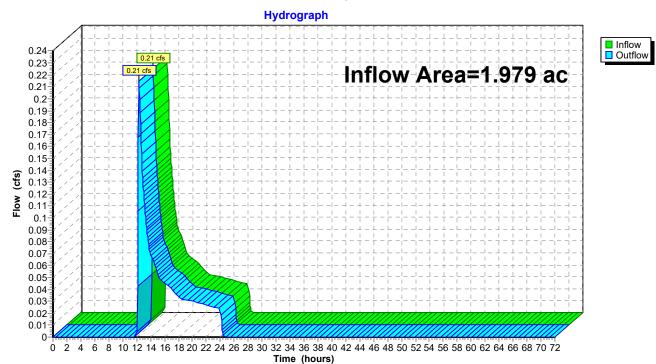
HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD Software Solutions LLC

Summary for Reach AP-2: Analysis Point - AP2

[40] Hint: Not Described (Outflow=Inflow)

| Inflow Area | a = | 1.979 ac, | 0.00% Impervious | , Inflow Depth = 0.3 | 30" for 2-Year event |
|-------------|-----|------------|------------------|----------------------|-------------------------|
| Inflow | = | 0.21 cfs @ | 12.36 hrs, Volum | e= 0.049 af | |
| Outflow | = | 0.21 cfs @ | 12.36 hrs, Volum | e= 0.049 af, | Atten= 0%, Lag= 0.0 min |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



Reach AP-2: Analysis Point - AP2

Summary for Pond 1E: Existing Depression

| Inflow Area = | 19.398 ac, | 3.33% Impervious, Inflow [| Depth = 0.14" for 2-Year event |
|---------------|------------|----------------------------|-------------------------------------|
| Inflow = | 0.41 cfs @ | 13.52 hrs, Volume= | 0.228 af |
| Outflow = | 0.31 cfs @ | 15.06 hrs, Volume= | 0.228 af, Atten= 24%, Lag= 92.2 min |
| Discarded = | 0.31 cfs @ | 15.06 hrs, Volume= | 0.228 af |
| Primary = | 0.00 cfs @ | 0.00 hrs, Volume= | 0.000 af |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 307.63' @ 15.06 hrs Surf.Area= 5,351 sf Storage= 903 cf Flood Elev= 309.20' Surf.Area= 30,032 sf Storage= 29,481 cf

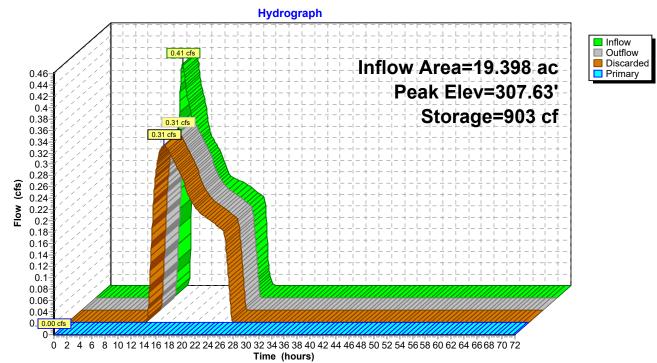
Plug-Flow detention time= 36.8 min calculated for 0.228 af (100% of inflow) Center-of-Mass det. time= 36.8 min (1,098.5 - 1,061.7)

| Volume | Invert | Avail.Sto | brage Storage Description | | | | |
|---------------------|-----------------|---|---|-----------------------------------|---------------------------------|--|--|
| #1 | 307.30' | 53,50 |)7 cf Custom | n Stage Data (P | Prismatic)Listed below (Recalc) | | |
| Flovetia | | unf Arrag | In a Ctara | Curra Chara | | | |
| Elevatio | | urf.Area | Inc.Store | Cum.Store | | | |
| (fee | et) | (sq-ft) | (cubic-feet) | (cubic-feet) | | | |
| 307.3 | 30 | 48 | 0 | 0 | | | |
| 308.0 | 00 | 11,143 | 3,917 | 3,917 | | | |
| 309.00 | | 28,160 | 19,652 | 23,568 | | | |
| 309.1 | 10 | 30,032 | 2,910 | 26,478 | | | |
| 310.0 | 00 | 30,032 | 27,029 | 53,507 | | | |
| | | | | | | | |
| Device | Routing | Invert | Outlet Device | es | | | |
| #1 | Discarded | 307.30' | 2.410 in/hr Exfiltration over Surface area | | r Surface area | | |
| | | | Conductivity to Groundwater Elevation = 304.00' Phase-In= 0.01' | | | | |
| #2 | Primary 309.05' | | 30.0' long x 5.0' breadth Broad-Crested Rectangular Weir | | | | |
| , | | Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 | | | | | |
| 2.50 3.00 3.50 4.00 | | | | | | | |
| | | | | .70 2.68 2.68 2.66 2.65 2.65 2.65 | | | |
| | | | | 66 2.68 2.70 2 | | | |
| | | | 2.05 2.07 2. | 00 2.00 2.70 2 | 2.14 2.19 2.00 | | |
| | | | | | | | |

Discarded OutFlow Max=0.31 cfs @ 15.06 hrs HW=307.63' (Free Discharge) **1=Exfiltration** (Controls 0.31 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=307.30' TW=0.00' (Dynamic Tailwater) 2=Broad-Crested Rectangular Weir(Controls 0.00 cfs) Prepared by Guerriere & Halnon, Inc. HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD Software Solutions LLC





| Pre-Post Development REV 1-26-24 Prepared by Guerriere & Halnon, Inc. <u>HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD Software Solut</u> | NRCC 24-hr C 10-Year Rainfall=4.88" Printed 2/20/2024 ions LLC Page 13 | | | | | | |
|---|--|--|--|--|--|--|--|
| Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method | | | | | | | |
| | 97 sf 3.33% Impervious Runoff Depth=0.64" =41.8 min CN=50 Runoff=4.25 cfs 1.041 af | | | | | | |
| | 06 sf 0.00% Impervious Runoff Depth=0.98" =15.6 min CN=56 Runoff=1.43 cfs 0.162 af | | | | | | |
| Reach AP-1: Analysis Point - AP1 | Inflow=0.00 cfs 0.000 af Outflow=0.00 cfs 0.000 af | | | | | | |
| Reach AP-2: Analysis Point - AP2 | Inflow=1.43 cfs 0.162 af Outflow=1.43 cfs 0.162 af | | | | | | |
| | Storage=12,684 cf Inflow=4.25 cfs 1.041 af | | | | | | |

ond 1E: Existing DepressionPeak Elev=308.55' Storage=12,684 cfInflow=4.25 cfs1.041 afDiscarded=1.33 cfs1.041 afPrimary=0.00 cfs0.000 afOutflow=1.33 cfs1.041 af

Total Runoff Area = 21.377 acRunoff Volume = 1.203 afAverage Runoff Depth = 0.68"96.98% Pervious = 20.731 ac3.02% Impervious = 0.646 ac

Pre-Post Development REV 1-26-24

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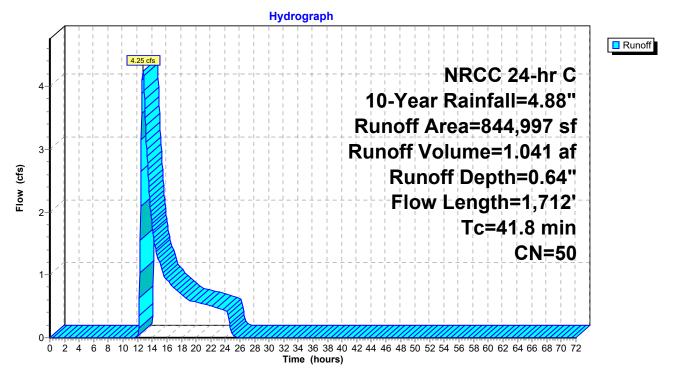
Summary for Subcatchment EX-1: Subcatchment to BVW

Runoff = 4.25 cfs @ 12.74 hrs, Volume= 1.041 af, Depth= 0.64"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 10-Year Rainfall=4.88"

| A | rea (sf) | CN [| Description | | | | |
|----------------------------|---------------------------------|----------------------------------|-----------------------|------------|--|--|--|
| 5 | 528,369 55 Woods, Good, HSG B | | | od, HSG B | | | |
| | 20,766 | 61 >75% Grass cover, Good, HSG B | | | | | |
| 1 | 163,331 39 >75% Grass cover, Go | | s cover, Go | bod, HSG A | | | |
| 104,370 30 Woods, Good, HS | | od, HSG A | | | | | |
| 28,161 98 | | 98 V | Water Surface, HSG A | | | | |
| 8 | 844,997 | | Weighted Average | | | | |
| 8 | 816,836 | | 96.67% Pervious Area | | | | |
| 28,161 | | 3 | 3.33% Impervious Area | | | | |
| | | | | | | | |
| Тс | Length | Slope | | Capacity | Description | | |
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | | | |
| 7.0 | 50 | 0.0800 | 0.12 | | Sheet Flow, Segment A-B | | |
| | | | | | Woods: Light underbrush n= 0.400 P2= 3.26" | | |
| 0.9 | 78 | 0.0800 | 1.41 | | Shallow Concentrated Flow, Segment B-C | | |
| | | | | | Woodland Kv= 5.0 fps | | |
| 12.7 | 592 | 0.0240 | 0.77 | | Shallow Concentrated Flow, Segment C-D | | |
| | | | | | Woodland Kv= 5.0 fps | | |
| 14.1 | 581 | 0.0190 | 0.69 | | Shallow Concentrated Flow, Segment D-E | | |
| | | | | | Woodland Kv= 5.0 fps | | |
| 7.1 | 411 | 0.0190 | 0.96 | | Shallow Concentrated Flow, Segment E-F | | |
| | | | | | Short Grass Pasture Kv= 7.0 fps | | |
| 41.8 | 1,712 | Total | | | | | |

Subcatchment EX-1: Subcatchment to BVW



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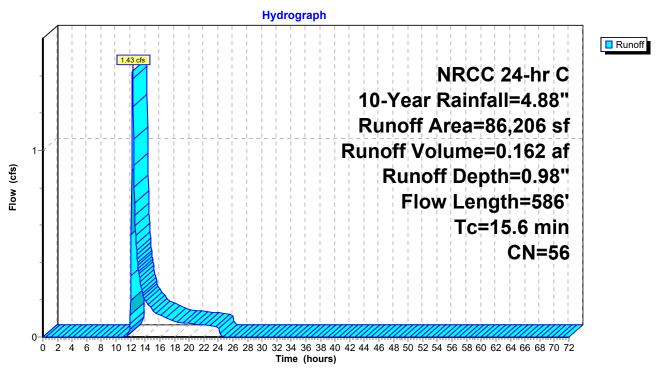
Summary for Subcatchment EX-2: To Blackstone Street

Runoff = 1.43 cfs @ 12.27 hrs, Volume= 0.162 af, Depth= 0.98"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 10-Year Rainfall=4.88"

| A | rea (sf) | CN | Description | | |
|-------|----------|---------|-------------|-------------|--|
| | 69,268 | 55 | Woods, Go | od, HSG B | |
| | 16,676 | 61 | >75% Gras | s cover, Go | bod, HSG B |
| | 131 | 39 | >75% Gras | s cover, Go | bod, HSG A |
| | 131 | 30 | Woods, Go | od, HSG A | |
| | 86,206 | 56 | Weighted A | verage | |
| | 86,206 | | 100.00% P | ervious Are | a |
| | | | | | |
| Tc | Length | Slope | | Capacity | Description |
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | |
| 7.8 | 50 | 0.0610 | 0.11 | | Sheet Flow, Segment A-B |
| | | | | | Woods: Light underbrush n= 0.400 P2= 3.26" |
| 2.8 | 215 | 0.0640 |) 1.26 | | Shallow Concentrated Flow, Segment B-C |
| | | | | | Woodland Kv= 5.0 fps |
| 2.2 | 103 | 0.0240 | 0.77 | | Shallow Concentrated Flow, Segment C-D |
| | | | | | Woodland Kv= 5.0 fps |
| 2.8 | 218 | 0.0340 |) 1.29 | | Shallow Concentrated Flow, Segment D-E |
| | | | | | Short Grass Pasture Kv= 7.0 fps |
| 15.6 | 586 | Total | | | |

Subcatchment EX-2: To Blackstone Street

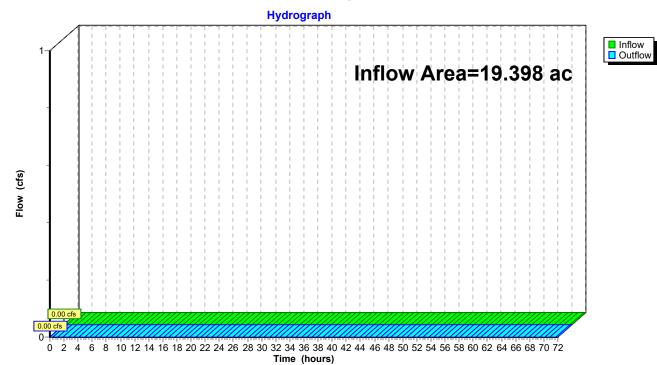


Summary for Reach AP-1: Analysis Point - AP1

[40] Hint: Not Described (Outflow=Inflow)

| Inflow Area = | 19.398 ac, | 3.33% Impervious, Inflo | ow Depth = 0.00" | for 10-Year event |
|---------------|------------|-------------------------|------------------|----------------------|
| Inflow = | 0.00 cfs @ | 0.00 hrs, Volume= | 0.000 af | |
| Outflow = | 0.00 cfs @ | 0.00 hrs, Volume= | 0.000 af, Atte | en= 0%, Lag= 0.0 min |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



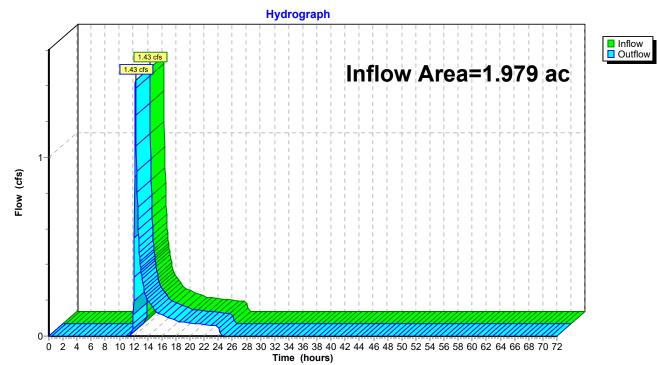
Reach AP-1: Analysis Point - AP1

Summary for Reach AP-2: Analysis Point - AP2

[40] Hint: Not Described (Outflow=Inflow)

| Inflow Area = | 1.979 ac, | 0.00% Impervious, Inflow D | epth = 0.98" | for 10-Year event |
|---------------|------------|----------------------------|----------------|----------------------|
| Inflow = | 1.43 cfs @ | 12.27 hrs, Volume= | 0.162 af | |
| Outflow = | 1.43 cfs @ | 12.27 hrs, Volume= | 0.162 af, Atte | en= 0%, Lag= 0.0 min |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



Reach AP-2: Analysis Point - AP2

Summary for Pond 1E: Existing Depression

| Inflow Area = | 19.398 ac, | 3.33% Impervious, Inflow E | Depth = 0.64" for 10-Year event |
|---------------|------------|----------------------------|--------------------------------------|
| Inflow = | 4.25 cfs @ | 12.74 hrs, Volume= | 1.041 af |
| Outflow = | 1.33 cfs @ | 14.65 hrs, Volume= | 1.041 af, Atten= 69%, Lag= 114.5 min |
| Discarded = | 1.33 cfs @ | 14.65 hrs, Volume= | 1.041 af |
| Primary = | 0.00 cfs @ | 0.00 hrs, Volume= | 0.000 af |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 308.55'@ 14.65 hrs Surf.Area= 20,556 sf Storage= 12,684 cf Flood Elev= 309.20' Surf.Area= 30,032 sf Storage= 29,481 cf

Plug-Flow detention time= 125.6 min calculated for 1.040 af (100% of inflow) Center-of-Mass det. time= 125.6 min (1,094.8 - 969.2)

| Volume | Invert | Avail.Stor | rage Storage | Description | |
|----------|-----------|--------------|--|---|--|
| #1 | 307.30' | 53,50 |)7 cf Custom | n Stage Data (P | rismatic)Listed below (Recalc) |
| | 0 | - F A | | 0 | |
| Elevatio | | rf.Area | Inc.Store | Cum.Store | |
| (fee | t) | (sq-ft) | (cubic-feet) | (cubic-feet) | |
| 307.3 | 0 | 48 | 0 | 0 | |
| 308.0 | 0 | 11,143 | 3,917 | 3,917 | |
| 309.0 | 0 | 28,160 | 19,652 | 23,568 | |
| 309.1 | 0 | 30,032 | 2,910 | 26,478 | |
| 310.0 | 0 | 30,032 | 27,029 | 53,507 | |
| | | | | | |
| Device | Routing | Invert | Outlet Device | es | |
| #1 | Discarded | 307.30' | 2.410 in/hr E | xfiltration over | Surface area |
| | | | Conductivity | to Groundwater | Elevation = 304.00' Phase-In= 0.01' |
| #2 | Primary | 309.05' | 30.0' long x | 5.0' breadth Br | oad-Crested Rectangular Weir |
| | - | | Head (feet) (| 0.20 0.40 0.60 | 0.80 1.00 1.20 1.40 1.60 1.80 2.00 |
| | | | 2.50 3.00 3. | 50 4.00 4.50 5 | .00 5.50 |
| | | | Coef. (Englis | h) 2.34 2.50 2. | 70 2.68 2.68 2.66 2.65 2.65 2.65 |
| | | | (U | 66 2.68 2.70 2 | |
| | | | | | |
| | | | Conductivity 30.0' long x Head (feet) (2.50 3.00 3. Coef. (Englis | to Groundwater 5.0' breadth Br 0.20 0.40 0.60 50 4.00 4.50 5 h) 2.34 2.50 2. | Elevation = 304.00' Phase-In= 0.01' oad-Crested Rectangular Weir 0.80 1.00 1.20 1.40 1.60 1.80 2.00 5.00 5.50 70 2.68 2.68 2.66 2.65 2.65 2.65 |

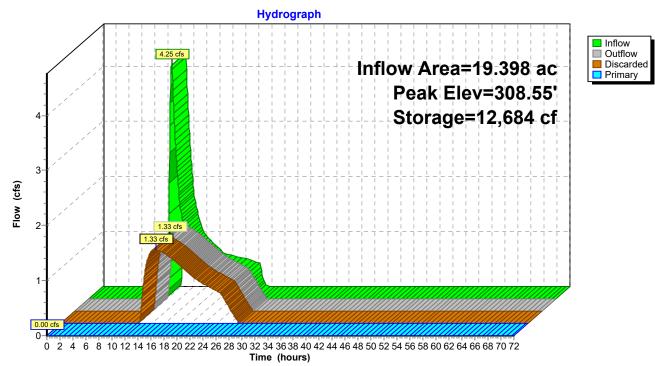
Discarded OutFlow Max=1.33 cfs @ 14.65 hrs HW=308.55' (Free Discharge) **1=Exfiltration** (Controls 1.33 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=307.30' TW=0.00' (Dynamic Tailwater) **2=Broad-Crested Rectangular Weir**(Controls 0.00 cfs)

Pre-Post Development REV 1-26-24

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Pond 1E: Existing Depression



| Pre-Post Development REV 1-26-24 Prepared by Guerriere & Halnon, Inc. HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD Software Solution | NRCC 24-hr C 25-Year Rainfall=6.15" Printed 2/20/2024 ons LLC Page 21 |
|--|--|
| Time span=0.00-72.00 hrs, dt=0.05 h Runoff by SCS TR-20 method, UH=SC Reach routing by Dyn-Stor-Ind method - Pond roo | CS, Weighted-CN |
| | 7 sf 3.33% Impervious Runoff Depth=1.22" 1.8 min CN=50 Runoff=10.15 cfs 1.968 af |
| | 6 sf 0.00% Impervious Runoff Depth=1.69" :15.6 min CN=56 Runoff=2.74 cfs 0.278 af |
| Reach AP-1: Analysis Point - AP1 | Inflow=1.65 cfs 0.147 af Outflow=1.65 cfs 0.147 af |
| Reach AP-2: Analysis Point - AP2 | Inflow=2.74 cfs 0.278 af Outflow=2.74 cfs 0.278 af |
| | Storage=27,439 cf Inflow=10.15 cfs 1.968 af 1.65 cfs 0.147 af Outflow=3.71 cfs 1.968 af |

Total Runoff Area = 21.377 acRunoff Volume = 2.246 afAverage Runoff Depth = 1.26"96.98% Pervious = 20.731 ac3.02% Impervious = 0.646 ac

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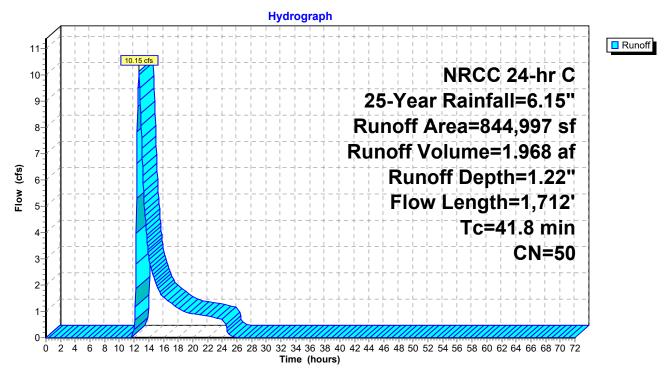
Summary for Subcatchment EX-1: Subcatchment to BVW

Runoff = 10.15 cfs @ 12.67 hrs, Volume= 1.968 af, Depth= 1.22"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 25-Year Rainfall=6.15"

| A | rea (sf) | CN [| Description | | |
|-------|----------|---------|-------------|-------------|--|
| 5 | 28,369 | 55 V | Voods, Go | od, HSG B | |
| | 20,766 | 61 > | 75% Gras | s cover, Go | bod, HSG B |
| 1 | 63,331 | 39 > | •75% Gras | s cover, Go | bod, HSG A |
| 1 | 04,370 | 30 V | Voods, Go | od, HSG A | |
| | 28,161 | 98 V | Vater Surfa | ace, HSG A | ι |
| 8 | 44,997 | 50 V | Veighted A | verage | |
| 8 | 16,836 | ç | 96.67% Pei | vious Area | |
| | 28,161 | 3 | 8.33% Impe | ervious Are | а |
| | | | | | |
| Tc | Length | Slope | Velocity | Capacity | Description |
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | |
| 7.0 | 50 | 0.0800 | 0.12 | | Sheet Flow, Segment A-B |
| | | | | | Woods: Light underbrush n= 0.400 P2= 3.26" |
| 0.9 | 78 | 0.0800 | 1.41 | | Shallow Concentrated Flow, Segment B-C |
| | | | | | Woodland Kv= 5.0 fps |
| 12.7 | 592 | 0.0240 | 0.77 | | Shallow Concentrated Flow, Segment C-D |
| | | | | | Woodland Kv= 5.0 fps |
| 14.1 | 581 | 0.0190 | 0.69 | | Shallow Concentrated Flow, Segment D-E |
| | | | | | Woodland Kv= 5.0 fps |
| 7.1 | 411 | 0.0190 | 0.96 | | Shallow Concentrated Flow, Segment E-F |
| | | | | | Short Grass Pasture Kv= 7.0 fps |
| 41.8 | 1,712 | Total | | | |

Subcatchment EX-1: Subcatchment to BVW



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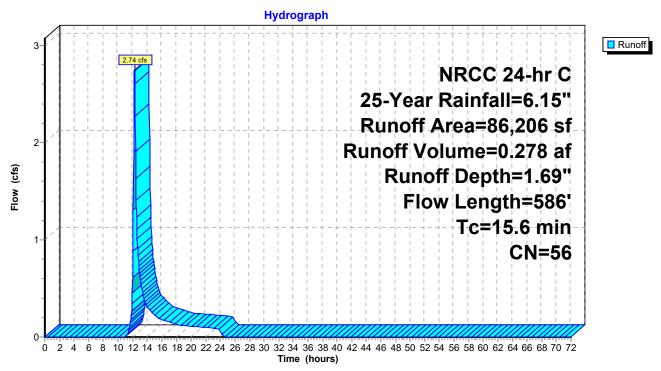
Summary for Subcatchment EX-2: To Blackstone Street

Runoff = 2.74 cfs @ 12.26 hrs, Volume= 0.278 af, Depth= 1.69"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 25-Year Rainfall=6.15"

| A | rea (sf) | CN | Description | | |
|-------|----------|---------|-------------|-------------|--|
| | 69,268 | 55 | Woods, Go | od, HSG B | |
| | 16,676 | 61 | >75% Gras | s cover, Go | bod, HSG B |
| | 131 | 39 | >75% Gras | s cover, Go | bod, HSG A |
| | 131 | 30 | Woods, Go | od, HSG A | |
| | 86,206 | 56 | Weighted A | verage | |
| | 86,206 | | 100.00% P | ervious Are | a |
| | | | | | |
| Tc | Length | Slope | | Capacity | Description |
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | |
| 7.8 | 50 | 0.0610 | 0.11 | | Sheet Flow, Segment A-B |
| | | | | | Woods: Light underbrush n= 0.400 P2= 3.26" |
| 2.8 | 215 | 0.0640 | 1.26 | | Shallow Concentrated Flow, Segment B-C |
| | | | | | Woodland Kv= 5.0 fps |
| 2.2 | 103 | 0.0240 | 0.77 | | Shallow Concentrated Flow, Segment C-D |
| | | | | | Woodland Kv= 5.0 fps |
| 2.8 | 218 | 0.0340 | 1.29 | | Shallow Concentrated Flow, Segment D-E |
| | | | | | Short Grass Pasture Kv= 7.0 fps |
| 15.6 | 586 | Total | | | |

Subcatchment EX-2: To Blackstone Street

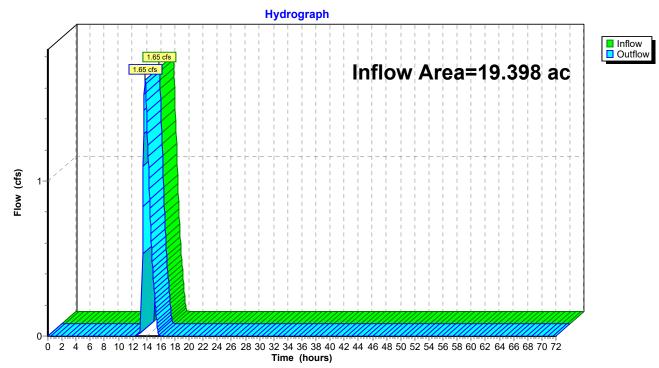


Summary for Reach AP-1: Analysis Point - AP1

[40] Hint: Not Described (Outflow=Inflow)

| Inflow Area = | 19.398 ac, | 3.33% Impervious, Inflow I | Depth = 0.09" | for 25-Year event |
|---------------|------------|----------------------------|----------------|----------------------|
| Inflow = | 1.65 cfs @ | 13.77 hrs, Volume= | 0.147 af | |
| Outflow = | 1.65 cfs @ | 13.77 hrs, Volume= | 0.147 af, Atte | en= 0%, Lag= 0.0 min |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



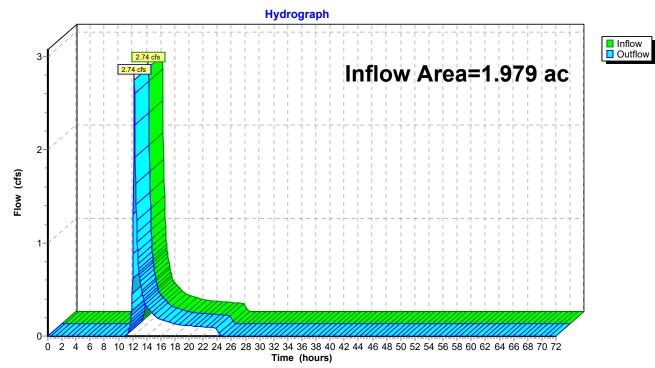
Reach AP-1: Analysis Point - AP1

Summary for Reach AP-2: Analysis Point - AP2

[40] Hint: Not Described (Outflow=Inflow)

| Inflow Area | a = | 1.979 ac, | 0.00% Impervious, | Inflow Depth = 1.6 | 9" for 25-Year event |
|-------------|-----|------------|-------------------|--------------------|-------------------------|
| Inflow | = | 2.74 cfs @ | 12.26 hrs, Volum | e= 0.278 af | |
| Outflow | = | 2.74 cfs @ | 12.26 hrs, Volume | e= 0.278 af, | Atten= 0%, Lag= 0.0 min |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



Reach AP-2: Analysis Point - AP2

Summary for Pond 1E: Existing Depression

| Inflow Area = | 19.398 ac, | 3.33% Impervious, Inflow D | epth = 1.22" for 25-Year event |
|---------------|-------------|----------------------------|-------------------------------------|
| Inflow = | 10.15 cfs @ | 12.67 hrs, Volume= | 1.968 af |
| Outflow = | 3.71 cfs @ | 13.77 hrs, Volume= | 1.968 af, Atten= 63%, Lag= 66.0 min |
| Discarded = | 2.06 cfs @ | 13.77 hrs, Volume= | 1.821 af |
| Primary = | 1.65 cfs @ | 13.77 hrs, Volume= | 0.147 af |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 309.13' @ 13.77 hrs Surf.Area= 30,032 sf Storage= 27,439 cf Flood Elev= 309.20' Surf.Area= 30,032 sf Storage= 29,481 cf

Plug-Flow detention time= 163.1 min calculated for 1.966 af (100% of inflow) Center-of-Mass det. time= 163.2 min (1,104.2 - 941.0)

| Volume | Invert | Avail.Sto | rage Storage | Description | |
|---|-----------------------------|---|---|---|----------------------------------|
| #1 | 307.30 | 53,50 | 07 cf Custom | n Stage Data (P | rismatic)Listed below (Recalc) |
| Elevatio (fee 307.3 308.0 309.0 309.7 310.0 | et) 30 00 00 10 | urf.Area (sq-ft) 48 11,143 28,160 30,032 30,032 | Inc.Store (cubic-feet) 0 3,917 19,652 2,910 27,029 | Cum.Store (cubic-feet) 0 3,917 23,568 26,478 53,507 | |
| Device | Routing | Invert | Outlet Device | | |
| #1 | Discarded | 307.30' | 2.410 in/hr E | xfiltration over | Surface area |
| #2 | Primary | 309.05' | 30.0' long x Head (feet) 0 2.50 3.00 3.4 Coef. (English | 5.0' breadth Br 0.20 0.40 0.60 50 4.00 4.50 5 | 70 2.68 2.68 2.66 2.65 2.65 2.65 |

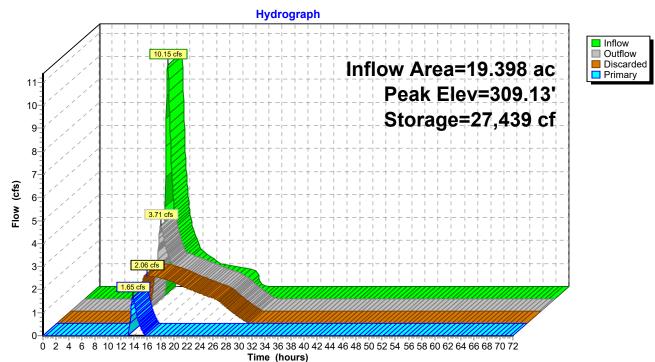
Discarded OutFlow Max=2.06 cfs @ 13.77 hrs HW=309.13' (Free Discharge) **1=Exfiltration** (Controls 2.06 cfs)

Primary OutFlow Max=1.65 cfs @ 13.77 hrs HW=309.13' TW=0.00' (Dynamic Tailwater) ←2=Broad-Crested Rectangular Weir (Weir Controls 1.65 cfs @ 0.67 fps)

Pre-Post Development REV 1-26-24

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Pond 1E: Existing Depression



| Pre-Post Development REV 1-26-24 Prepared by Guerriere & Halnon, Inc. HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD Software Sol | NRCC 24-hr C 100-Year Rainfall=8.74" Printed 2/20/2024 utions LLC Page 29 |
|--|--|
| Time span=0.00-72.00 hrs, dt=0.0 Runoff by SCS TR-20 method, UH= Reach routing by Dyn-Stor-Ind method - Pond | SCS, Weighted-CN |
| | ,997 sf 3.33% Impervious Runoff Depth=2.71" c=41.8 min CN=50 Runoff=26.44 cfs 4.387 af |
| | ,206 sf 0.00% Impervious Runoff Depth=3.42" Fc=15.6 min CN=56 Runoff=5.94 cfs 0.564 af |
| Reach AP-1: Analysis Point - AP1 | Inflow=19.70 cfs 1.933 af Outflow=19.70 cfs 1.933 af |
| Reach AP-2: Analysis Point - AP2 | Inflow=5.94 cfs 0.564 af Outflow=5.94 cfs 0.564 af |
| | ' Storage=37,263 cf Inflow=26.44 cfs 4.387 af 19.70 cfs 1.933 af Outflow=21.89 cfs 4.387 af |

Total Runoff Area = 21 377 ac. Runoff Volume = 4 951 af. Average Runoff Denth = 2 78

Total Runoff Area = 21.377 acRunoff Volume = 4.951 afAverage Runoff Depth = 2.78"96.98% Pervious = 20.731 ac3.02% Impervious = 0.646 ac

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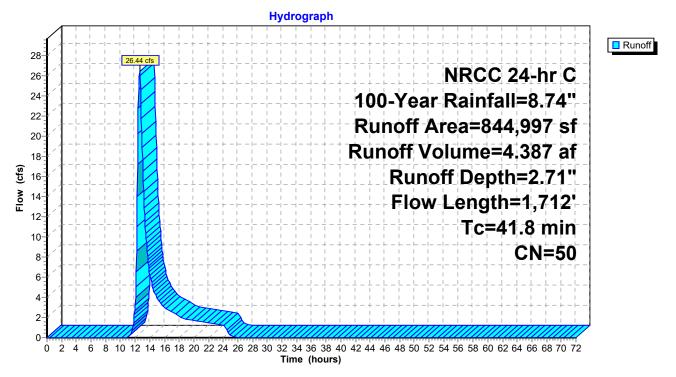
Summary for Subcatchment EX-1: Subcatchment to BVW

Runoff = 26.44 cfs @ 12.61 hrs, Volume= 4.387 af, Depth= 2.71"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 100-Year Rainfall=8.74"

| A | rea (sf) | CN [| Description | | |
|-------|----------|---------|-------------|-------------|--|
| 5 | 28,369 | 55 V | Voods, Go | od, HSG B | |
| | 20,766 | 61 > | 75% Gras | s cover, Go | bod, HSG B |
| 1 | 63,331 | 39 > | •75% Gras | s cover, Go | bod, HSG A |
| 1 | 04,370 | 30 V | Voods, Go | od, HSG A | |
| | 28,161 | 98 V | Vater Surfa | ace, HSG A | ι |
| 8 | 44,997 | 50 V | Veighted A | verage | |
| 8 | 16,836 | ç | 96.67% Pei | vious Area | |
| | 28,161 | 3 | 8.33% Impe | ervious Are | а |
| | | | | | |
| Tc | Length | Slope | Velocity | Capacity | Description |
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | |
| 7.0 | 50 | 0.0800 | 0.12 | | Sheet Flow, Segment A-B |
| | | | | | Woods: Light underbrush n= 0.400 P2= 3.26" |
| 0.9 | 78 | 0.0800 | 1.41 | | Shallow Concentrated Flow, Segment B-C |
| | | | | | Woodland Kv= 5.0 fps |
| 12.7 | 592 | 0.0240 | 0.77 | | Shallow Concentrated Flow, Segment C-D |
| | | | | | Woodland Kv= 5.0 fps |
| 14.1 | 581 | 0.0190 | 0.69 | | Shallow Concentrated Flow, Segment D-E |
| | | | | | Woodland Kv= 5.0 fps |
| 7.1 | 411 | 0.0190 | 0.96 | | Shallow Concentrated Flow, Segment E-F |
| | | | | | Short Grass Pasture Kv= 7.0 fps |
| 41.8 | 1,712 | Total | | | |

Subcatchment EX-1: Subcatchment to BVW



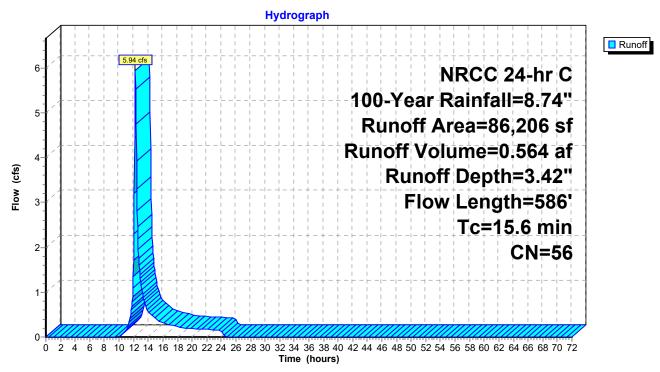
Summary for Subcatchment EX-2: To Blackstone Street

Runoff = 5.94 cfs @ 12.25 hrs, Volume= 0.564 af, Depth= 3.42"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 100-Year Rainfall=8.74"

| A | rea (sf) | CN | Description | | |
|-------|----------|---------|-------------|-------------|--|
| | 69,268 | 55 | Woods, Go | od, HSG B | |
| | 16,676 | 61 | >75% Gras | s cover, Go | bod, HSG B |
| | 131 | 39 | >75% Gras | s cover, Go | bod, HSG A |
| | 131 | 30 | Woods, Go | od, HSG A | |
| | 86,206 | 56 | Weighted A | verage | |
| | 86,206 | | 100.00% P | ervious Are | a |
| | | | | | |
| Tc | Length | Slope | | Capacity | Description |
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | |
| 7.8 | 50 | 0.0610 | 0.11 | | Sheet Flow, Segment A-B |
| | | | | | Woods: Light underbrush n= 0.400 P2= 3.26" |
| 2.8 | 215 | 0.0640 | 1.26 | | Shallow Concentrated Flow, Segment B-C |
| | | | | | Woodland Kv= 5.0 fps |
| 2.2 | 103 | 0.0240 | 0.77 | | Shallow Concentrated Flow, Segment C-D |
| | | | | | Woodland Kv= 5.0 fps |
| 2.8 | 218 | 0.0340 | 1.29 | | Shallow Concentrated Flow, Segment D-E |
| | | | | | Short Grass Pasture Kv= 7.0 fps |
| 15.6 | 586 | Total | | | |

Subcatchment EX-2: To Blackstone Street

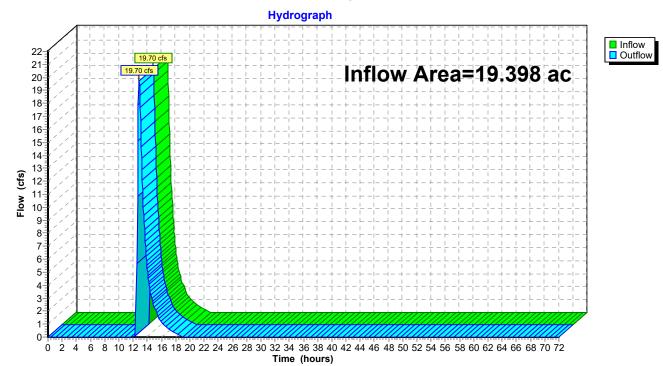


Summary for Reach AP-1: Analysis Point - AP1

[40] Hint: Not Described (Outflow=Inflow)

| Inflow Are | a = | 19.398 ac, | 3.33% Impervious | , Inflow Depth = 1.20 | 0" for 100-Year event |
|------------|-----|-------------|------------------|-----------------------|-------------------------|
| Inflow | = | 19.70 cfs @ | 12.85 hrs, Volum | ie= 1.933 af | |
| Outflow | = | 19.70 cfs @ | 12.85 hrs, Volum | e= 1.933 af, <i>i</i> | Atten= 0%, Lag= 0.0 min |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



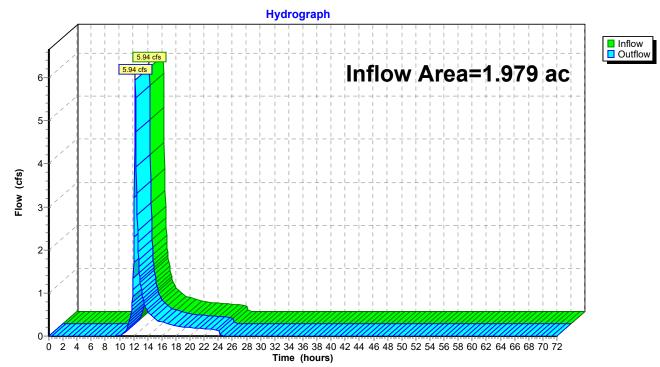
Reach AP-1: Analysis Point - AP1

Summary for Reach AP-2: Analysis Point - AP2

[40] Hint: Not Described (Outflow=Inflow)

| Inflow Area | = | 1.979 ac, | 0.00% Impervious, Inflow | / Depth = 3.42" | for 100-Year event |
|-------------|---|------------|--------------------------|-----------------|----------------------|
| Inflow | = | 5.94 cfs @ | 12.25 hrs, Volume= | 0.564 af | |
| Outflow | = | 5.94 cfs @ | 12.25 hrs, Volume= | 0.564 af, Atte | en= 0%, Lag= 0.0 min |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



Reach AP-2: Analysis Point - AP2

Summary for Pond 1E: Existing Depression

[58] Hint: Peaked 0.26' above defined flood level

| Inflow Area = | 19.398 ac, | 3.33% Impervious, Inflow D | epth = 2.71" for 100-Year event |
|---------------|-------------|----------------------------|-------------------------------------|
| Inflow = | 26.44 cfs @ | 12.61 hrs, Volume= | 4.387 af |
| Outflow = | 21.89 cfs @ | 12.85 hrs, Volume= | 4.387 af, Atten= 17%, Lag= 14.2 min |
| Discarded = | 2.20 cfs @ | 12.85 hrs, Volume= | 2.453 af |
| Primary = | 19.70 cfs @ | 12.85 hrs, Volume= | 1.933 af |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 309.46'@ 12.85 hrs Surf.Area= 30,032 sf Storage= 37,263 cf Flood Elev= 309.20' Surf.Area= 30,032 sf Storage= 29,481 cf

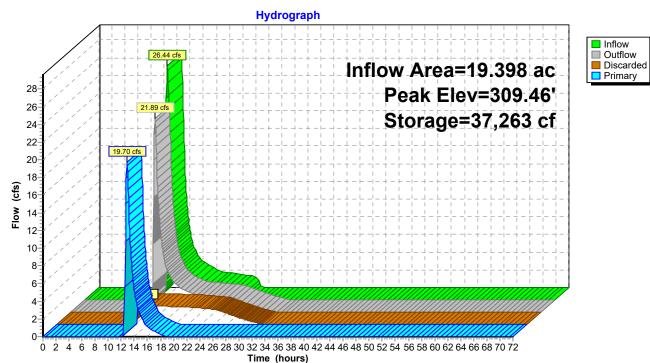
Plug-Flow detention time= 111.2 min calculated for 4.384 af (100% of inflow) Center-of-Mass det. time= 111.4 min (1,022.5 - 911.2)

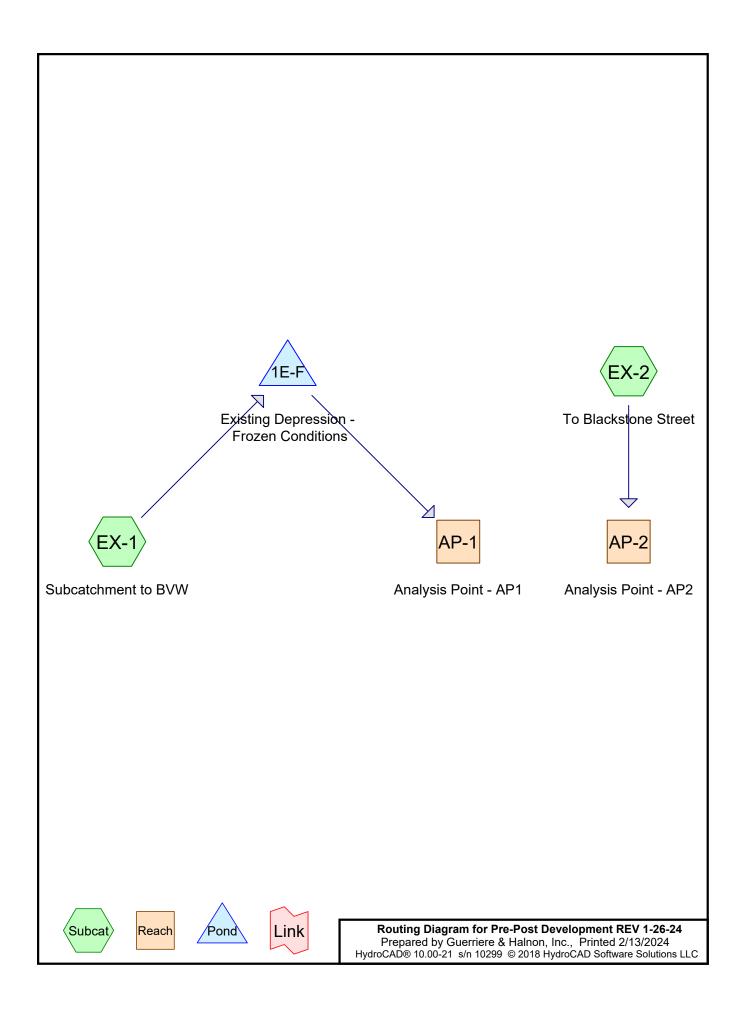
| Volume | Invert | Avail.Sto | rage Storage | Description | |
|------------|-----------|------------|----------------|------------------|-------------------------------------|
| #1 | 307.30 | 53,50 | 07 cf Custom | Stage Data (P | rismatic)Listed below (Recalc) |
| - 1 | | E A | | 0 | |
| Elevatio | | urf.Area | Inc.Store | Cum.Store | |
| (fee | et) | (sq-ft) | (cubic-feet) | (cubic-feet) | |
| 307.3 | 30 | 48 | 0 | 0 | |
| 308.0 | 00 | 11,143 | 3,917 | 3,917 | |
| 309.0 |)0 | 28,160 | 19,652 | 23,568 | |
| 309.1 | 0 | 30,032 | 2,910 | 26,478 | |
| 310.0 | 00 | 30,032 | 27,029 | 53,507 | |
| | | | | | |
| Device | Routing | Invert | Outlet Device | S | |
| #1 | Discarded | 307.30' | 2.410 in/hr E | xfiltration over | Surface area |
| | | | Conductivity t | o Groundwater | Elevation = 304.00' Phase-In= 0.01' |
| #2 | Primary | 309.05' | | | oad-Crested Rectangular Weir |
| | 5 | | | | 0.80 1.00 1.20 1.40 1.60 1.80 2.00 |
| | | | () | 50 4.00 4.50 5 | |
| | | | Coef. (Enalish | n) 2.34 2.50 2. | 70 2.68 2.68 2.66 2.65 2.65 2.65 |
| | | | | 66 2.68 2.70 2 | |
| | | | - | - | |

Discarded OutFlow Max=2.20 cfs @ 12.85 hrs HW=309.46' (Free Discharge) **1=Exfiltration** (Controls 2.20 cfs)

Primary OutFlow Max=19.70 cfs @ 12.85 hrs HW=309.46' TW=0.00' (Dynamic Tailwater) ←2=Broad-Crested Rectangular Weir (Weir Controls 19.70 cfs @ 1.60 fps) Prepared by Guerriere & Halnon, Inc. HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD Software Solutions LLC

Pond 1E: Existing Depression





Pre-Post Development REV 1-26-24 Prepared by Guerriere & Halnon, Inc. HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD Software Solutions LLC

Area Listing (selected nodes)

| Area | CN | Description |
|---------|----|--|
| (acres) | | (subcatchment-numbers) |
| 3.753 | 39 | >75% Grass cover, Good, HSG A (EX-1, EX-2) |
| 0.860 | 61 | >75% Grass cover, Good, HSG B (EX-1, EX-2) |
| 0.646 | 98 | Water Surface, HSG A (EX-1) |
| 2.399 | 30 | Woods, Good, HSG A (EX-1, EX-2) |
| 13.720 | 55 | Woods, Good, HSG B (EX-1, EX-2) |
| 21.377 | 51 | TOTAL AREA |

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Soil Listing (selected nodes)

| Area | Soil | Subcatchment |
|---------|-------|--------------|
| (acres) | Group | Numbers |
| 6.798 | HSG A | EX-1, EX-2 |
| 14.579 | HSG B | EX-1, EX-2 |
| 0.000 | HSG C | |
| 0.000 | HSG D | |
| 0.000 | Other | |
| 21.377 | | TOTAL AREA |
| | | |

Pre-Post Development REV 1-26-24

| Prepared by Guerriere & Halnon, Inc. | |
|---|--|
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| HSG-A (acres) | HSG-B (acres) | HSG-C (acres) | HSG-D (acres) | Other (acres) | Total (acres) | Ground Cover | Subcatchment Numbers |
|----------------------|------------------|------------------|------------------|------------------|------------------|------------------------|-------------------------|
| 3.753 | 0.860 | 0.000 | 0.000 | 0.000 | 4.612 | >75% Grass cover, Good | EX-1, |
| | | | | | | | EX-2 |
| 0.646 | 0.000 | 0.000 | 0.000 | 0.000 | 0.646 | Water Surface | EX-1 |
| 2.399 | 13.720 | 0.000 | 0.000 | 0.000 | 16.119 | Woods, Good | EX-1, |
| | | | | | | | EX-2 |
| 6.798 | 14.579 | 0.000 | 0.000 | 0.000 | 21.377 | TOTAL AREA | |

Ground Covers (selected nodes)

| Pre-Post Development REV 1-26-24 Prepared by Guerriere & Halnon, Inc. <u>HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD Software Solut</u> | NRCC 24-hr C 25-Year Rainfall=6.15" Printed 2/13/2024 ions LLC Page 5 |
|---|--|
| Time span=0.00-72.00 hrs, dt=0.05 Runoff by SCS TR-20 method, UH=S Reach routing by Dyn-Stor-Ind method - Pond ro | CS, Weighted-CN |
| | 97 sf 3.33% Impervious Runoff Depth=1.22" 41.8 min CN=50 Runoff=10.15 cfs 1.968 af |
| | 06 sf 0.00% Impervious Runoff Depth=1.69" =15.6 min CN=56 Runoff=2.74 cfs 0.278 af |
| Reach AP-1: Analysis Point - AP1 | Inflow=4.38 cfs 1.394 af Outflow=4.38 cfs 1.394 af |
| Reach AP-2: Analysis Point - AP2 | Inflow=2.74 cfs 0.278 af Outflow=2.74 cfs 0.278 af |
| Pond 1E-F: Existing Depression - Frozen Peak Elev=309.21' | Storage=29,702 cf Inflow=10.15 cfs 1.968 af Outflow=4.38 cfs 1.394 af |
| Total Runoff Area = 21.377 ac Runoff Volum 96.98% Pervious : | v . |

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Summary for Subcatchment EX-1: Subcatchment to BVW

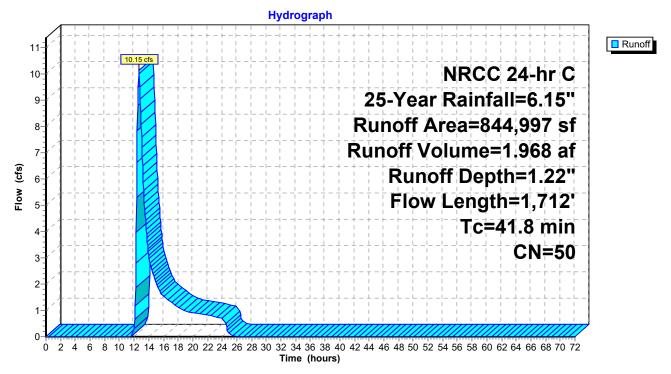
Runoff = 10.15 cfs @ 12.67 hrs, Volume= 1.968 af, Depth= 1.22"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 25-Year Rainfall=6.15"

| _ | A | rea (sf) | CN [| Description | | |
|----------------------------------|-------|----------|---------|-------------|-------------|--|
| 528,369 55 Woods, Good, HSG B | | | | | od, HSG B | |
| 20,766 61 >75% Grass cover, Goo | | | | | s cover, Go | bod, HSG B |
| 163,331 39 >75% Grass cover, Goo | | | | | , | , |
| 104,370 30 Woods, Good, HSG A | | | | | , | |
| | | 28,161 | 98 \ | Nater Surfa | ace, HSG A | l |
| | | 44,997 | | Neighted A | | |
| | | 16,836 | - | | rvious Area | |
| | | 28,161 | 3 | 3.33% Impe | ervious Are | а |
| | - | | | | 0 | |
| | Tc | Length | Slope | | Capacity | Description |
| _ | (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | |
| | 7.0 | 50 | 0.0800 | 0.12 | | Sheet Flow, Segment A-B |
| | | 70 | | | | Woods: Light underbrush n= 0.400 P2= 3.26" |
| | 0.9 | 78 | 0.0800 | 1.41 | | Shallow Concentrated Flow, Segment B-C |
| | 40 7 | 500 | 0 00 40 | 0.77 | | Woodland Kv= 5.0 fps |
| | 12.7 | 592 | 0.0240 | 0.77 | | Shallow Concentrated Flow, Segment C-D |
| | 111 | E01 | 0.0100 | 0.60 | | Woodland Kv= 5.0 fps |
| | 14.1 | 581 | 0.0190 | 0.69 | | Shallow Concentrated Flow, Segment D-E Woodland Kv= 5.0 fps |
| | 7.1 | 411 | 0.0190 | 0.96 | | Shallow Concentrated Flow, Segment E-F |
| | 1.1 | 411 | 0.0190 | 0.90 | | Short Grass Pasture Kv= 7.0 fps |
| _ | 41.8 | 1 712 | Total | | | |

41.8 1,712 Total

Subcatchment EX-1: Subcatchment to BVW



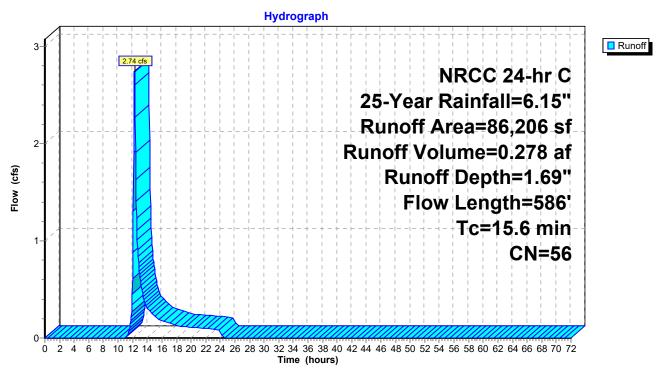
Summary for Subcatchment EX-2: To Blackstone Street

Runoff = 2.74 cfs @ 12.26 hrs, Volume= 0.278 af, Depth= 1.69"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 25-Year Rainfall=6.15"

| A | rea (sf) | CN | Description | | | | | | |
|-------|----------|---------|-------------------------------|-------------|--|--|--|--|--|
| | 69,268 | 55 | 55 Woods, Good, HSG B | | | | | | |
| | 16,676 | 61 | >75% Gras | s cover, Go | bod, HSG B | | | | |
| | 131 | | >75% Grass cover, Good, HSG A | | | | | | |
| | 131 | 30 | Woods, Go | od, HSG A | | | | | |
| | 86,206 | | Weighted A | | | | | | |
| | 86,206 | | 100.00% Pe | ervious Are | a | | | | |
| | | | | | | | | | |
| Tc | Length | Slope | | Capacity | Description | | | | |
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | | | | | |
| 7.8 | 50 | 0.0610 | 0.11 | | Sheet Flow, Segment A-B | | | | |
| | | | | | Woods: Light underbrush n= 0.400 P2= 3.26" | | | | |
| 2.8 | 215 | 0.0640 | 1.26 | | Shallow Concentrated Flow, Segment B-C | | | | |
| | | | | | Woodland Kv= 5.0 fps | | | | |
| 2.2 | 103 | 0.0240 | 0.77 | | Shallow Concentrated Flow, Segment C-D | | | | |
| | | | | | Woodland Kv= 5.0 fps | | | | |
| 2.8 | 218 | 0.0340 | 1.29 | | Shallow Concentrated Flow, Segment D-E | | | | |
| | | | | | Short Grass Pasture Kv= 7.0 fps | | | | |
| 15.6 | 586 | Total | | | | | | | |

Subcatchment EX-2: To Blackstone Street

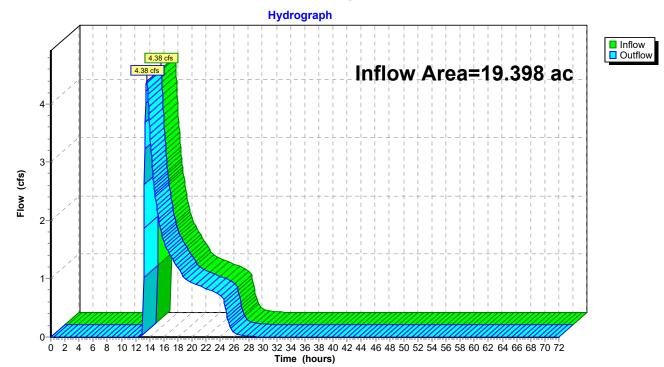


Summary for Reach AP-1: Analysis Point - AP1

[40] Hint: Not Described (Outflow=Inflow)

| Inflow Area = | 19.398 ac, | 3.33% Impervious, Inflow | Depth = 0.86" | for 25-Year event |
|---------------|------------|--------------------------|----------------|----------------------|
| Inflow = | 4.38 cfs @ | 13.57 hrs, Volume= | 1.394 af | |
| Outflow = | 4.38 cfs @ | 13.57 hrs, Volume= | 1.394 af, Atte | en= 0%, Lag= 0.0 min |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



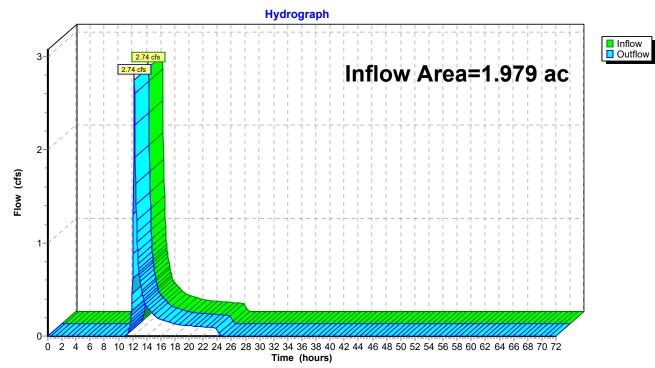
Reach AP-1: Analysis Point - AP1

Summary for Reach AP-2: Analysis Point - AP2

[40] Hint: Not Described (Outflow=Inflow)

| Inflow Area | a = | 1.979 ac, | 0.00% Impervious, | Inflow Depth = 1.6 | 9" for 25-Year event |
|-------------|-----|------------|-------------------|--------------------|-------------------------|
| Inflow | = | 2.74 cfs @ | 12.26 hrs, Volume | e= 0.278 af | |
| Outflow | = | 2.74 cfs @ | 12.26 hrs, Volume | e= 0.278 af, . | Atten= 0%, Lag= 0.0 min |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



Reach AP-2: Analysis Point - AP2

Summary for Pond 1E-F: Existing Depression - Frozen Conditions

[58] Hint: Peaked 0.01' above defined flood level

| Inflow Area = | 19.398 ac, | 3.33% Impervious, In | flow Depth = 1.22" for 25-Year event |
|---------------|-------------|----------------------|--------------------------------------|
| Inflow = | 10.15 cfs @ | 12.67 hrs, Volume= | 1.968 af |
| Outflow = | 4.38 cfs @ | 13.57 hrs, Volume= | 1.394 af, Atten= 57%, Lag= 54.0 min |
| Primary = | 4.38 cfs @ | 13.57 hrs, Volume= | 1.394 af |

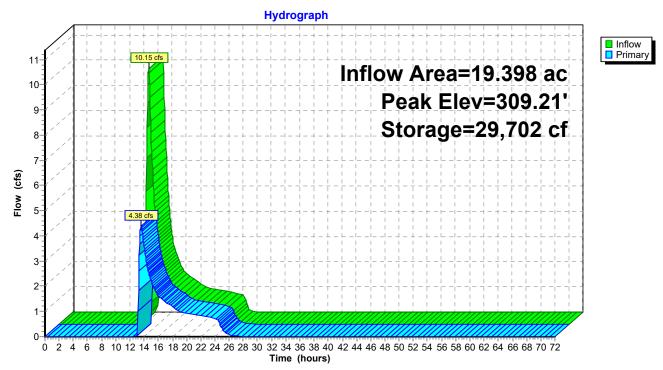
Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 309.21'@ 13.57 hrs Surf.Area= 30,032 sf Storage= 29,702 cf Flood Elev= 309.20' Surf.Area= 30,032 sf Storage= 29,481 cf

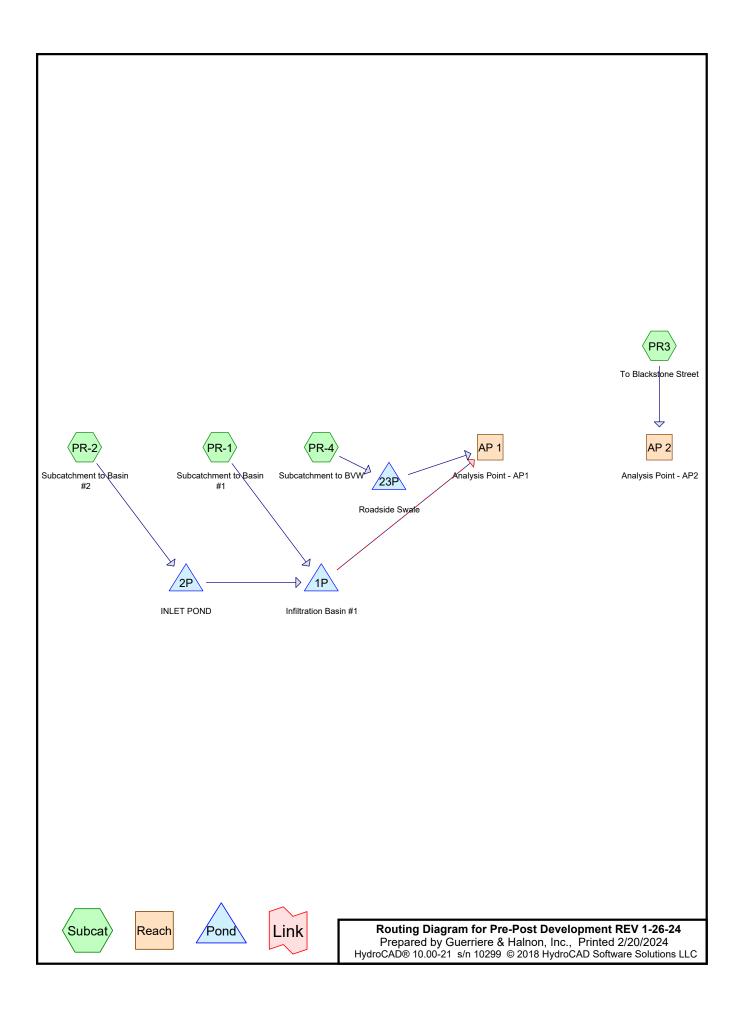
Plug-Flow detention time= 216.6 min calculated for 1.393 af (71% of inflow) Center-of-Mass det. time= 100.4 min (1,041.3 - 941.0)

| Volume | Inve | ert Avail.Sto | orage Storage D | escription | | |
|---------------------|---------|----------------------|---------------------------|---|------------------------------------|--|
| #1 | 307.3 | 30' 53,5 | 07 cf Custom S | cf Custom Stage Data (Prismatic)Listed below (Recalc) | | |
| Elevation (feet) | | Surf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) | | |
| 307.30 |) | 48 | 0 | 0 | | |
| 308.00 |) | 11,143 | 3,917 | 3,917 | | |
| 309.00 |) | 28,160 | 19,652 | 23,568 | | |
| 309.10 |) | 30,032 | 2,910 | 26,478 | | |
| 310.00 |) | 30,032 | 27,029 | 53,507 | | |
| Device I | Routing | Invert | Outlet Devices | | | |
| #1 I | Primary | 309.05' | 30.0' long x 5. | 0' breadth Br | oad-Crested Rectangular Weir | |
| | | | Head (feet) 0.2 | 0 0.40 0.60 | 0.80 1.00 1.20 1.40 1.60 1.80 2.00 | |
| | | | 2.50 3.00 3.50 | 4.00 4.50 5 | 5.00 5.50 | |
| | | | Coef. (English) | 2.34 2.50 2. | 70 2.68 2.68 2.66 2.65 2.65 2.65 | |
| | | | 2.65 2.67 2.66 | 2.68 2.70 2 | 2.74 2.79 2.88 | |
| | | | | | | |

Primary OutFlow Max=4.38 cfs @ 13.57 hrs HW=309.21' TW=0.00' (Dynamic Tailwater) **1=Broad-Crested Rectangular Weir** (Weir Controls 4.38 cfs @ 0.93 fps)

Pond 1E-F: Existing Depression - Frozen Conditions





Pre-Post Development REV 1-26-24 Prepared by Guerriere & Halnon, Inc. HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD Software Solutions LLC

Area Listing (selected nodes)

| Area | CN | Description | |
|---------|----|--|--|
| (acres) | | (subcatchment-numbers) | |
| 2.918 | 39 | >75% Grass cover, Good, HSG A (PR-1, PR-2, PR-4) | |
| 0.786 | 61 | >75% Grass cover, Good, HSG B (PR-2, PR3) | |
| 0.874 | 98 | Paved roads w/curbs & sewers (PR-1) | |
| 0.443 | 98 | Roofs (PR-1) | |
| 0.474 | 98 | Water Surface, HSG A (PR-1) | |
| 2.222 | 30 | Woods, Good, HSG A (PR-2) | |
| 13.663 | 55 | Woods, Good, HSG B (PR-2, PR3) | |
| 21.378 | 54 | TOTAL AREA | |

Pre-Post Development REV 1-26-24 Prepared by Guerriere & Halnon, Inc. HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD Software Solutions LLC

Soil Listing (selected nodes)

| Soil | Subcatchment |
|-------|---|
| Group | Numbers |
| HSG A | PR-1, PR-2, PR-4 |
| HSG B | PR-2, PR3 |
| HSG C | |
| HSG D | |
| Other | PR-1 |
| | TOTAL AREA |
| | Group HSG A HSG B HSG C HSG D |

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|------------------------------|--|
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Printed 2/20/2024 Page 4

| HSG-A | HSG-B | HSG-C | HSG-D | Other | Total | Ground | Subcatchment |
|-------------|---------|---------|---------|---------|---------|------------------------------|--------------|
| (acres) | (acres) | (acres) | (acres) | (acres) | (acres) | Cover | Numbers |
| 2.918 | 0.786 | 0.000 | 0.000 | 0.000 | 3.703 | >75% Grass cover, Good | PR |
| | | | | | | | -1, |
| | | | | | | | PR |
| | | | | | | | -2, |
| | | | | | | | PR |
| | | | | | | | -4, |
| | | | | | | | PR |
| | | | | | | | 3 |
| 0.000 | 0.000 | 0.000 | 0.000 | 0.874 | 0.874 | Paved roads w/curbs & sewers | PR |
| | | | | | | | -1 |
| 0.000 | 0.000 | 0.000 | 0.000 | 0.443 | 0.443 | Roofs | PR |
| | | | | | | | -1 |
| 0.474 | 0.000 | 0.000 | 0.000 | 0.000 | 0.474 | Water Surface | PR |
| | | | | | | | -1 |
| 2.222 | 13.663 | 0.000 | 0.000 | 0.000 | 15.884 | Woods, Good | PR |
| | | | | | | | -2, |
| | | | | | | | PR |
| | | | | | | | 3 |
| 5.613 | 14.448 | 0.000 | 0.000 | 1.317 | 21.378 | TOTAL AREA | |

Ground Covers (selected nodes)

| Prepared by Guerriere & Halnon, Inc. | | | | | |
|---|--|--|--|--|--|
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| Line# | Node Number | In-Invert (feet) | Out-Invert (feet) | Length (feet) | Slope (ft/ft) | n | Diam/Width (inches) | Height (inches) | Inside-Fill (inches) |
|-------|----------------|---------------------|----------------------|------------------|------------------|-------|------------------------|--------------------|-------------------------|
| 1 | PR-2 | 0.00 | 0.00 | 312.0 | 0.0230 | 0.013 | 24.0 | 0.0 | 0.0 |
| 2 | PR-4 | 0.00 | 0.00 | 47.0 | 0.0050 | 0.011 | 12.0 | 0.0 | 0.0 |
| 3 | 1P | 306.00 | 305.53 | 94.2 | 0.0050 | 0.011 | 24.0 | 0.0 | 0.0 |
| 4 | 2P | 310.60 | 307.00 | 363.4 | 0.0099 | 0.013 | 24.0 | 0.0 | 0.0 |

Pipe Listing (selected nodes)

| Pre-Post Development REV 1-26-24 Prepared by Guerriere & Halnon, Inc. HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD Softwa | NRCC 24-hr C 2-Year Rainfall=3.26" Printed 2/20/2024 are Solutions LLC Page 6 |
|---|--|
| Time span=0.00-72.00 hrs, o Runoff by SCS TR-20 method Reach routing by Dyn-Stor-Ind method - | , UH=SCS, Weighted-CN |
| SubcatchmentPR-1: Subcatchmentto Runoff Area | =141,517 sf 55.11% Impervious Runoff Depth=0.97" Tc=6.0 min CN=72 Runoff=3.71 cfs 0.262 af |
| | a=670,872 sf 0.00% Impervious Runoff Depth=0.16" 673' Tc=37.2 min CN=51 Runoff=0.42 cfs 0.210 af |
| SubcatchmentPR-4: Subcatchmentto BVW Runoff Are Flow Length=5 | ea=33,131 sf 0.00% Impervious Runoff Depth=0.00" 544' Tc=10.6 min CN=39 Runoff=0.00 cfs 0.000 af |
| | ea=85,707 sf 0.00% Impervious Runoff Depth=0.30" 572' Tc=15.5 min CN=56 Runoff=0.21 cfs 0.049 af |
| Reach AP 1: Analysis Point - AP1 | Inflow=0.00 cfs 0.000 af Outflow=0.00 cfs 0.000 af |
| Reach AP 2: Analysis Point - AP2 | Inflow=0.21 cfs 0.049 af Outflow=0.21 cfs 0.049 af |
| Pond 1P: Infiltration Basin #1Peak Eviscarded=2.07 cfs0.472 afPrimary=0.00 cfs0.000 afSec | lev=305.57' Storage=715 cf Inflow=3.71 cfs 0.472 af condary=0.00 cfs 0.000 af Outflow=2.07 cfs 0.472 af |
| | Elev=312.00' Storage=0 cf Inflow=0.42 cfs 0.210 af Primary=0.42 cfs 0.210 af Outflow=0.42 cfs 0.210 af |
| | Elev=306.01' Storage=0 cf Inflow=0.00 cfs 0.000 af Primary=0.00 cfs 0.000 af Outflow=0.00 cfs 0.000 af |
| | f Volume = 0.521 af Average Runoff Depth = 0.29 rvious = 19.588 ac 8.38% Impervious = 1.790 ac |

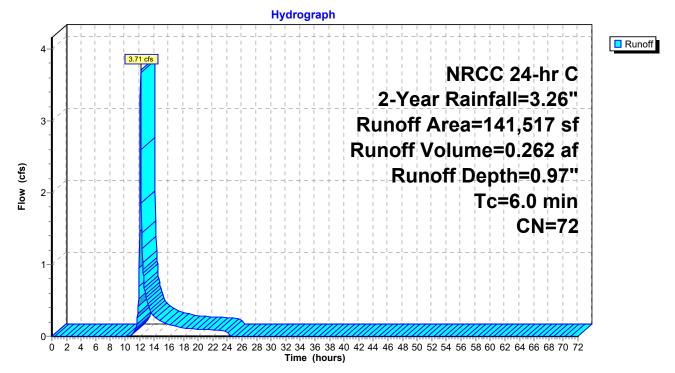
Summary for Subcatchment PR-1: Subcatchment to Basin #1

Runoff = 3.71 cfs @ 12.14 hrs, Volume= 0.262 af, Depth= 0.97"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 2-Year Rainfall=3.26"

| _ | Area (s | f) CN | Description | | | | |
|---|-----------|---------|---------------|-------------------------------|---------------|--|--|
| * | 38,06 | 98 26 | Paved road | ls w/curbs a | & sewers | | |
| * | 19,29 | 98 36 | Roofs | | | | |
| | 63,52 | 24 39 | >75% Gras | >75% Grass cover, Good, HSG A | | | |
| * | 20,63 | 88 98 | Water Surfa | ace, HSG A | Α | | |
| | 141,51 | 7 72 | Weighted A | verage | | | |
| | 63,52 | 24 | 44.89% Pe | 44.89% Pervious Area | | | |
| | 77,99 |)3 | 55.11% lm | 55.11% Impervious Area | | | |
| | | | | | | | |
| | Tc Leng | | | Capacity | | | |
| _ | (min) (fe | et) (ft | /ft) (ft/sec) | (cfs) | | | |
| | 6.0 | | | | Direct Entry, | | |

Subcatchment PR-1: Subcatchment to Basin #1



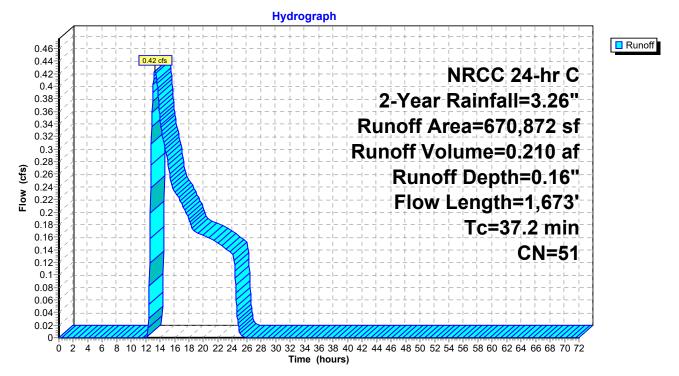
Summary for Subcatchment PR-2: Subcatchment to Basin #2

Runoff = 0.42 cfs @ 13.29 hrs, Volume= 0.210 af, Depth= 0.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 2-Year Rainfall=3.26"

| A | rea (sf) | CN D | escription | | | |
|-------|----------|---------|----------------------|-------------|---|--|
| 5 | 27,673 | 55 V | 5 Woods, Good, HSG B | | | |
| | 96,783 | 30 V | /oods, Go | od, HSG A | | |
| | 15,981 | 61 > | 75% Gras | s cover, Go | bod, HSG B | |
| | 30,435 | 39 > | 75% Gras | s cover, Go | ood, HSG A | |
| 6 | 70,872 | 51 V | /eighted A | verage | | |
| 6 | 70,872 | 1 | 00.00% Pe | ervious Are | а | |
| | | | | | | |
| Тс | Length | Slope | Velocity | | Description | |
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | | |
| 7.0 | 50 | 0.0800 | 0.12 | | Sheet Flow, Segment A-B | |
| | | | | | Woods: Light underbrush n= 0.400 P2= 3.26" | |
| 0.9 | 78 | 0.0800 | 1.41 | | Shallow Concentrated Flow, Segment B-C | |
| | | | | | Woodland Kv= 5.0 fps | |
| 12.7 | 592 | 0.0240 | 0.77 | | Shallow Concentrated Flow, Segment C-D | |
| | | | | | Woodland Kv= 5.0 fps | |
| 14.1 | 581 | 0.0190 | 0.69 | | Shallow Concentrated Flow, Segment D-E | |
| 0.0 | 00 | 0.0400 | 0.50 | | Woodland Kv= 5.0 fps | |
| 2.0 | 60 | 0.0100 | 0.50 | | Shallow Concentrated Flow, Segment E-F | |
| 0.5 | 040 | 0 0000 | 40.00 | 04.04 | Woodland Kv= 5.0 fps | |
| 0.5 | 312 | 0.0230 | 10.92 | 34.31 | Pipe Channel, Segment F-G | |
| | | | | | 24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50' | |
| 07.0 | 4.070 | | | | n= 0.013 Concrete pipe, straight & clean | |
| 37.2 | 1,673 | Total | | | | |

Subcatchment PR-2: Subcatchment to Basin #2



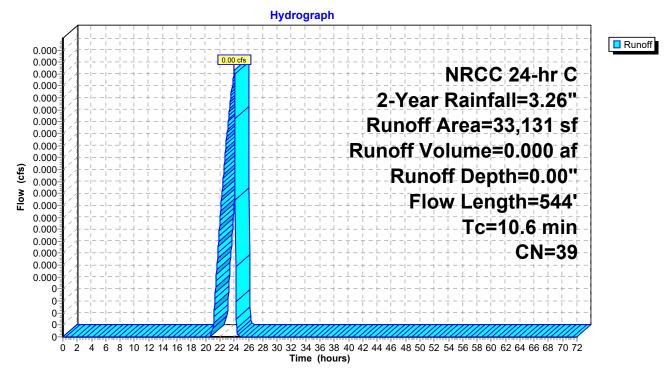
Summary for Subcatchment PR-4: Subcatchment to BVW

Runoff = 0.00 cfs @ 24.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 2-Year Rainfall=3.26"

| _ | A | rea (sf) | CN | Description | | | | | |
|---|-------------|------------------|------------------|----------------------------------|-------------------|---|--|--|--|
| | | 33,131 | 39 | 39 >75% Grass cover, Good, HSG A | | | | | |
| _ | | 33,131 | | 100.00% P | ervious Are | a | | | |
| | Tc (min) | Length (feet) | Slope (ft/ft) | | Capacity (cfs) | Description | | | |
| - | 5.6 | 50 | 0.0200 | 0.15 | | Sheet Flow, Segment A-B | | | |
| | | | | | | Grass: Short n= 0.150 P2= 3.26" | | | |
| | 2.0 | 194 | 0.0550 | 1.64 | | Shallow Concentrated Flow, Segment B-C | | | |
| | | <i>.</i> _ | | | | Short Grass Pasture Kv= 7.0 fps | | | |
| | 0.2 | 47 | 0.0050 | 3.79 | 2.98 | | | | |
| | | | | | | 12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25' | | | |
| | ~ ~ ~ | 050 | 0.0400 | 4 50 | | n= 0.011 Concrete pipe, straight & clean | | | |
| | 2.8 | 253 | 0.0100 | 1.50 | | Shallow Concentrated Flow, Segment D-E Grassed Waterway Kv= 15.0 fps | | | |
| - | 10.6 | 511 | Total | | | Glassed Waterway IN- 13.0 lps | | | |
| | 10.6 | 544 | Total | | | | | | |

Subcatchment PR-4: Subcatchment to BVW



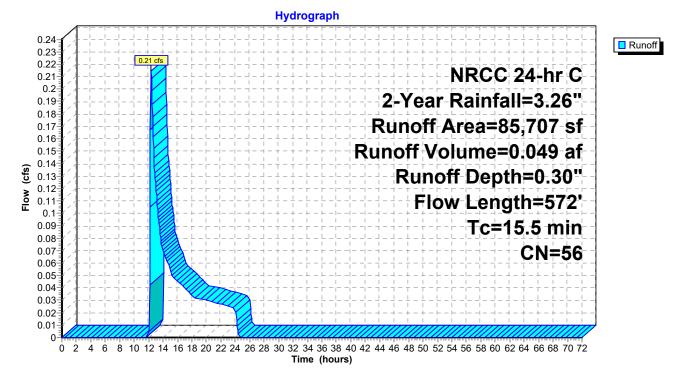
Summary for Subcatchment PR3: To Blackstone Street

Runoff = 0.21 cfs @ 12.36 hrs, Volume= 0.049 af, Depth= 0.30"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 2-Year Rainfall=3.26"

| Α | rea (sf) | CN D | escription | | |
|-------|----------|---------|------------|-------------|--|
| | 67,471 | 55 V | Voods, Go | od, HSG B | |
| | 18,236 | 61 > | 75% Gras | s cover, Go | ood, HSG B |
| | 85,707 | 56 V | Veighted A | verage | |
| | 85,707 | 1 | 00.00% Pe | ervious Are | а |
| | | | | | |
| Tc | Length | Slope | Velocity | Capacity | Description |
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | |
| 7.8 | 50 | 0.0610 | 0.11 | | Sheet Flow, Segment A-B |
| | | | | | Woods: Light underbrush n= 0.400 P2= 3.26" |
| 2.8 | 215 | 0.0640 | 1.26 | | Shallow Concentrated Flow, Segment B-C |
| | | | | | Woodland Kv= 5.0 fps |
| 2.2 | 103 | 0.0240 | 0.77 | | Shallow Concentrated Flow, Segment C-D |
| | | | | | Woodland Kv= 5.0 fps |
| 2.7 | 204 | 0.0320 | 1.25 | | Shallow Concentrated Flow, Segment D-E |
| | | | | | Short Grass Pasture Kv= 7.0 fps |
| 15.5 | 572 | Total | | | |

Subcatchment PR3: To Blackstone Street

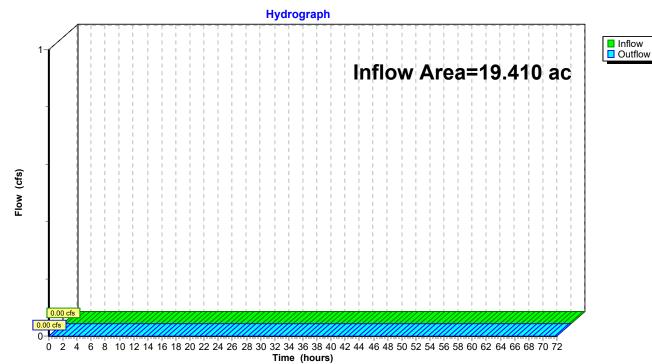


Summary for Reach AP 1: Analysis Point - AP1

[40] Hint: Not Described (Outflow=Inflow)

| Inflow Area = | 19.410 ac, | 9.22% Impervious, Inflow | Depth = 0.00" | for 2-Year event |
|---------------|------------|--------------------------|----------------|----------------------|
| Inflow = | 0.00 cfs @ | 0.00 hrs, Volume= | 0.000 af | |
| Outflow = | 0.00 cfs @ | 0.00 hrs, Volume= | 0.000 af, Atte | en= 0%, Lag= 0.0 min |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



Reach AP 1: Analysis Point - AP1

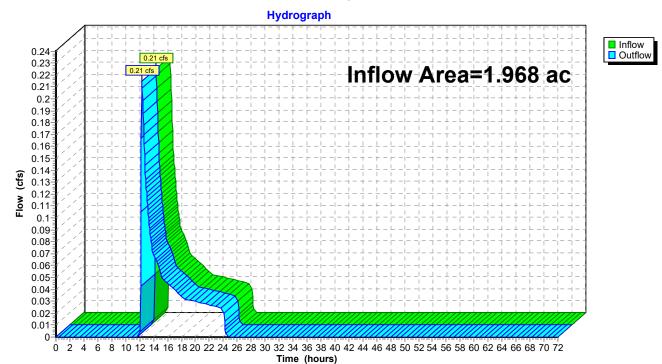
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Summary for Reach AP 2: Analysis Point - AP2

[40] Hint: Not Described (Outflow=Inflow)

| Inflow Area = | 1.968 ac, | 0.00% Impervious, Inflow D | Depth = $0.30"$ | for 2-Year event |
|---------------|------------|----------------------------|-----------------|----------------------|
| Inflow = | 0.21 cfs @ | 12.36 hrs, Volume= | 0.049 af | |
| Outflow = | 0.21 cfs @ | 12.36 hrs, Volume= | 0.049 af, Atte | en= 0%, Lag= 0.0 min |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



Reach AP 2: Analysis Point - AP2

Summary for Pond 1P: Infiltration Basin #1

| Inflow Area = | 18.650 ac, | 9.60% Impervious, Inflow | Depth = 0.30" for 2-Year event |
|---------------|------------|--------------------------|------------------------------------|
| Inflow = | 3.71 cfs @ | 12.14 hrs, Volume= | 0.472 af |
| Outflow = | 2.07 cfs @ | 12.24 hrs, Volume= | 0.472 af, Atten= 44%, Lag= 6.0 min |
| Discarded = | 2.07 cfs @ | 12.24 hrs, Volume= | 0.472 af |
| Primary = | 0.00 cfs @ | 0.00 hrs, Volume= | 0.000 af |
| Secondary = | 0.00 cfs @ | 0.00 hrs, Volume= | 0.000 af |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 305.57' @ 12.24 hrs Surf.Area= 10,581 sf Storage= 715 cf Flood Elev= 310.50' Surf.Area= 20,637 sf Storage= 77,211 cf

Plug-Flow detention time= 1.3 min calculated for 0.472 af (100% of inflow) Center-of-Mass det. time= 1.3 min (954.8 - 953.5)

| Volume | Invert | Avail.Stor | rage Storage | |
|----------|-----------|------------|------------------|--|
| #1 | 305.50' | 87,52 | 29 cf Custom | n Stage Data (Prismatic)Listed below (Recalc) |
| Elevatio | | rf.Area | Inc.Store | Cum.Store |
| (fee | / | (sq-ft) | (cubic-feet) | (cubic-feet) |
| 305.5 | | 10,451 | 0 | 0 |
| 306.0 | | 11,407 | 5,465 | 5,465 |
| 308.0 | | 15,368 | 26,775 | 32,240 |
| 310.0 | | 19,555 | 34,923 | 67,163 |
| 310.5 | | 20,637 | 10,048 | 77,211 |
| 311.0 | 00 | 20,637 | 10,319 | 87,529 |
| Device | Routing | Invert | Outlet Device | es |
| #1 | Primary | 306.00' | 24.0" Round | d Culvert |
| | | | L= 94.2' RC | CP, groove end w/headwall, Ke= 0.200 |
| | | | Inlet / Outlet I | Invert= 306.00' / 305.53' S= 0.0050 '/' Cc= 0.900 |
| | | | n= 0.011 Co | oncrete pipe, straight & clean, Flow Area= 3.14 sf |
| #2 | Device 1 | 308.55' | 48.0" x 48.0" | "Horiz. Orifice/Grate C= 0.600 |
| | | | Limited to we | eir flow at low heads |
| #3 | Device 1 | 307.00' | 12.0" W x 9.0 | 0" H Vert. Orifice/Grate C= 0.600 |
| #4 | Discarded | 305.50' | 8.270 in/hr E | Exfiltration over Horizontal area |
| | | | Conductivity | to Groundwater Elevation = 302.70' Phase-In= 0.01' |
| #5 | Secondary | 309.90' | | 10.0' breadth Broad-Crested Rectangular Weir |
| | 2 | | Head (feet) (| 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 |
| | | | | sh) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64 |
| | | | | |

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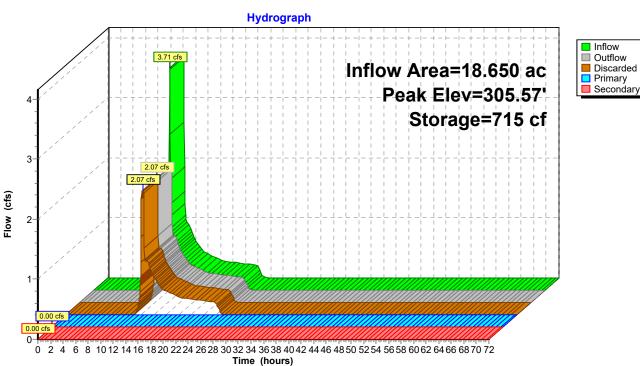
Discarded OutFlow Max=2.07 cfs @ 12.24 hrs HW=305.57' (Free Discharge) **4=Exfiltration** (Controls 2.07 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=305.50' TW=0.00' (Dynamic Tailwater)

-2=Orifice/Grate (Controls 0.00 cfs)

3=Orifice/Grate (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=305.50' TW=0.00' (Dynamic Tailwater) 5=Broad-Crested Rectangular Weir(Controls 0.00 cfs)



Pond 1P: Infiltration Basin #1

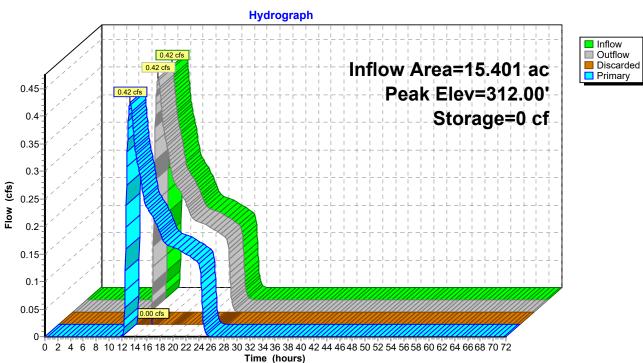
Summary for Pond 2P: INLET POND

| Inflow Ar Inflow Outflow Discarde Primary | = = ed = | 0.42 cfs @ 13 0.42 cfs @ 13 0.00 cfs @ 14 | 00% Impervious 3.29 hrs, Volum 3.29 hrs, Volum 4.47 hrs, Volum 3.29 hrs, Volum | e= 0.2 e= 0.2 e= 0.0 | n = 0.16" for 2-Ye 210 af 210 af, Atten= 0%, L 000 af 210 af | | |
|--|--|---|--|----------------------------|--|-------------------|--|
| | Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 312.00' @ 0.00 hrs Surf.Area= 1,182 sf Storage= 0 cf | | | | | | |
| Center-o | Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 0.0 min(1,043.8 - 1,043.8) | | | | | | |
| Volume | Inver | | rage Storage D | | | | |
| #1 | 312.00 |)' 3,48 | 30 cf Custom | Stage Data (P | rismatic)Listed below | w (Recalc) | |
| Elevatio (feet | | Surf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) | | | |
| 312.0 | / | 1,182 | 0 | | | | |
| 313.0 | - | 1,690 | 1,436 | 1,436 | | | |
| 314.0 | | 2,398 | 2,044 | 3,480 | | | |
| Device | Routing | Invert | Outlet Devices | , | | | |
| #1 | Primary | 310.60' | 24.0" Round | Culvert | | | |
| | | | | | e headwall, Ke= 0.50 | | |
| | | | | | ' 307.00' S= 0.0099 | | |
| | | | | | ids & connections, F | low Area= 3.14 sf | |
| #2 | Discarded | I 312.00' | 8.270 in/hr Ex | | | | |
| | | | Conductivity to | Groundwater | Elevation = 304.67' | Phase-In= 0.01' | |
| Bis sended OctEless Marcol 0.00 (Fr. O. 44, 47 has 1004, 040,001, (Fr. S. Bissharras) | | | | | | | |

Discarded OutFlow Max=0.00 cfs @ 14.47 hrs HW=312.00' (Free Discharge) **2=Exfiltration** (Controls 0.00 cfs)

Primary OutFlow Max=0.00 cfs @ 13.29 hrs HW=312.00' TW=305.50' (Dynamic Tailwater) **1=Culvert** (Passes 0.00 cfs of 9.46 cfs potential flow)

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Pond 2P: INLET POND

Summary for Pond 23P: Roadside Swale

| Inflow Area = | 0.761 ac, | 0.00% Impervious, Inflow De | epth = 0.00" for 2-Year event |
|---------------|------------|-----------------------------|-----------------------------------|
| Inflow = | 0.00 cfs @ | 24.00 hrs, Volume= | 0.000 af |
| Outflow = | 0.00 cfs @ | 24.00 hrs, Volume= | 0.000 af, Atten= 0%, Lag= 0.4 min |
| Discarded = | 0.00 cfs @ | 24.00 hrs, Volume= | 0.000 af |
| Primary = | 0.00 cfs @ | 0.00 hrs, Volume= | 0.000 af |

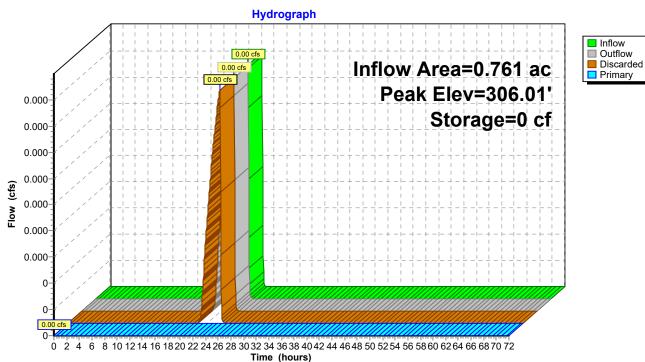
Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 306.01' @ 24.00 hrs Surf.Area= 4 sf Storage= 0 cf

Plug-Flow detention time= 0.4 min calculated for 0.000 af (100% of inflow) Center-of-Mass det. time= 0.4 min (1,382.4 - 1,382.0)

| Volume | Invert | Avail.Sto | rage Storage | e Description | |
|--|----------------------|---------------------|--|---|--|
| #1 | 306.00' | 1,36 | 65 cf Custon | n Stage Data (P | rismatic)Listed below (Recalc) |
| Elevatio (fee | | urf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) | |
| 306.0 | 00 | 0 | 0 | 0 | |
| 307.0 | 00 | 700 | 350 | 350 | |
| 308.0 | 00 | 1,330 | 1,015 | 1,365 | |
| Device | Routing | Invert | Outlet Device | es | |
| #1 #2 | Discarded Primary | 306.00' 307.25' | 8.270 in/hr E 10.0' long x Head (feet) (2.50 3.00 3. | 2.0' breadth Br 0.20 0.40 0.60 50 h) 2.54 2.61 2. | Surface area Phase-In= 0.01' oad-Crested Rectangular Weir 0.80 1.00 1.20 1.40 1.60 1.80 2.00 61 2.60 2.66 2.70 2.77 2.89 2.88 |
| Disconded QuitFlow May-0.00 of @ 24.00 km UN/-200 041 (Erec Discharge) | | | | | |

Discarded OutFlow Max=0.00 cfs @ 24.00 hrs HW=306.01' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.00 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=306.00' TW=0.00' (Dynamic Tailwater) 2=Broad-Crested Rectangular Weir(Controls 0.00 cfs)



Pond 23P: Roadside Swale

| Pre-Post Development REV 1-26- Prepared by Guerriere & Halnon, Inc. HydroCAD® 10.00-21 s/n 10299 © 2018 Hy | | | C 10-Year Rainfall=4.88" Printed 2/20/2024 Page 20 |
|--|------------------------------------|-------------------|--|
| | | =SCS, Weighted-Cl | |
| SubcatchmentPR-1: Subcatchmentto | Runoff Area=141, | | ervious Runoff Depth=2.11" 2 Runoff=8.38 cfs 0.570 af |
| SubcatchmentPR-2: Subcatchmentto | | | ervious Runoff Depth=0.70" 1 Runoff=4.09 cfs 0.894 af |
| SubcatchmentPR-4: Subcatchmentto I | | | ervious Runoff Depth=0.18" 9 Runoff=0.02 cfs 0.011 af |
| SubcatchmentPR3: To Blackstone Stre | | | ervious Runoff Depth=0.98" 6 Runoff=1.42 cfs 0.161 af |
| Reach AP 1: Analysis Point - AP1 | | | Inflow=0.00 cfs 0.000 af Outflow=0.00 cfs 0.000 af |
| Reach AP 2: Analysis Point - AP2 | | | Inflow=1.42 cfs 0.161 af Outflow=1.42 cfs 0.161 af |
| Pond 1P: Infiltration Basin #1 Discarded=3.07 cfs 1.464 af Primary=0.00 cfs | | 0 | cf Inflow=8.58 cfs 1.464 af Outflow=3.07 cfs 1.464 af |
| Pond 2P: INLET POND Discarded=0.00 | | | cf Inflow=4.09 cfs 0.894 af Outflow=4.09 cfs 0.894 af |
| Pond 23P: Roadside Swale Discarded=0.02 | | | cf Inflow=0.02 cfs 0.011 af Outflow=0.02 cfs 0.011 af |
| Total Runoff Area = 21.3 | 78 ac Runoff Vol 91.62% Perviou | | verage Runoff Depth = 0.92" 38% Impervious = 1.790 ac |

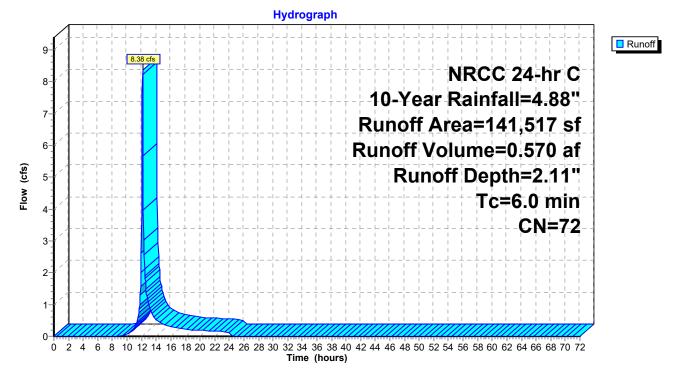
Summary for Subcatchment PR-1: Subcatchment to Basin #1

Runoff = 8.38 cfs @ 12.13 hrs, Volume= 0.570 af, Depth= 2.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 10-Year Rainfall=4.88"

| | Area (sf) | CN | Description | | |
|---|-------------|-------|--------------|-------------|---------------|
| * | 38,062 | 98 | Paved road | s w/curbs a | & sewers |
| * | 19,293 | 98 | Roofs | | |
| | 63,524 | 39 | >75% Gras | s cover, Go | lood, HSG A |
| * | 20,638 | 98 | Water Surfa | ace, HSG A | Α |
| | 141,517 | 72 | Weighted A | verage | |
| | 63,524 | | 44.89% Per | vious Area | a |
| | 77,993 | | 55.11% lmp | pervious Ar | rea |
| | | | | | |
| | Tc Length | | | Capacity | • |
| (| min) (feet) | (ft/1 | ft) (ft/sec) | (cfs) | |
| | 6.0 | | | | Direct Entry, |

Subcatchment PR-1: Subcatchment to Basin #1



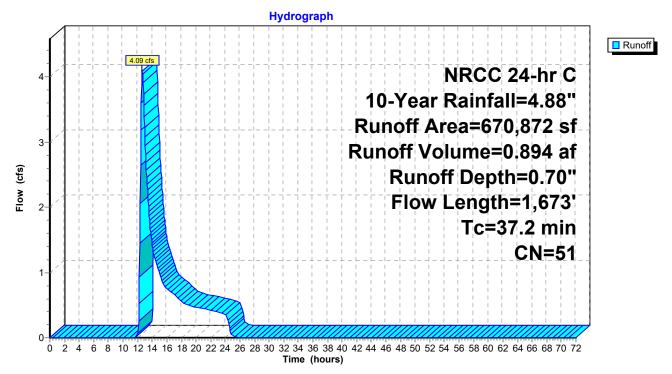
Summary for Subcatchment PR-2: Subcatchment to Basin #2

Runoff = 4.09 cfs @ 12.65 hrs, Volume= 0.894 af, Depth= 0.70"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 10-Year Rainfall=4.88"

| A | rea (sf) | CN D | escription | | | | |
|-------|----------|---------|-----------------------|-------------|---|--|--|
| 5 | 27,673 | 55 V | 55 Woods, Good, HSG B | | | | |
| | 96,783 | 30 V | /oods, Go | od, HSG A | | | |
| | 15,981 | 61 > | 75% Gras | s cover, Go | bod, HSG B | | |
| | 30,435 | 39 > | 75% Gras | s cover, Go | ood, HSG A | | |
| 6 | 70,872 | 51 V | /eighted A | verage | | | |
| 6 | 70,872 | 1 | 00.00% Pe | ervious Are | а | | |
| | | | | | | | |
| Тс | Length | Slope | Velocity | | Description | | |
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | | | |
| 7.0 | 50 | 0.0800 | 0.12 | | Sheet Flow, Segment A-B | | |
| | | | | | Woods: Light underbrush n= 0.400 P2= 3.26" | | |
| 0.9 | 78 | 0.0800 | 1.41 | | Shallow Concentrated Flow, Segment B-C | | |
| | | | | | Woodland Kv= 5.0 fps | | |
| 12.7 | 592 | 0.0240 | 0.77 | | Shallow Concentrated Flow, Segment C-D | | |
| | | | | | Woodland Kv= 5.0 fps | | |
| 14.1 | 581 | 0.0190 | 0.69 | | Shallow Concentrated Flow, Segment D-E | | |
| 0.0 | 00 | 0.0400 | 0.50 | | Woodland Kv= 5.0 fps | | |
| 2.0 | 60 | 0.0100 | 0.50 | | Shallow Concentrated Flow, Segment E-F | | |
| 0.5 | 040 | 0 0000 | 40.00 | 04.04 | Woodland Kv= 5.0 fps | | |
| 0.5 | 312 | 0.0230 | 10.92 | 34.31 | Pipe Channel, Segment F-G | | |
| | | | | | 24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50' | | |
| 07.0 | 4.070 | | | | n= 0.013 Concrete pipe, straight & clean | | |
| 37.2 | 1,673 | Total | | | | | |

Subcatchment PR-2: Subcatchment to Basin #2



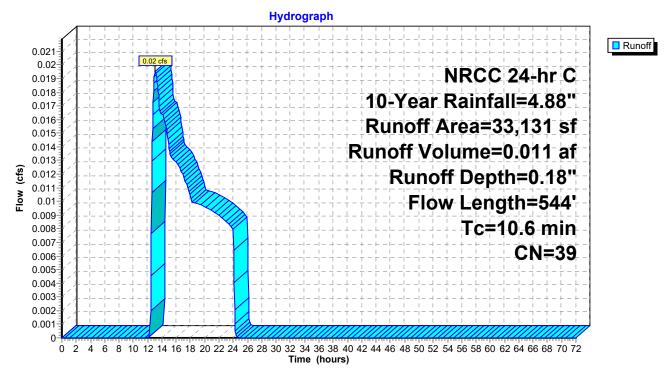
Summary for Subcatchment PR-4: Subcatchment to BVW

Runoff = 0.02 cfs @ 13.06 hrs, Volume= 0.011 af, Depth= 0.18"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 10-Year Rainfall=4.88"

| _ | A | rea (sf) | CN | Description | | | | | |
|---|-------------|------------------|------------------|----------------------------------|-------------------|---|--|--|--|
| | | 33,131 | 39 | 39 >75% Grass cover, Good, HSG A | | | | | |
| _ | | 33,131 | | 100.00% P | ervious Are | a | | | |
| | Tc (min) | Length (feet) | Slope (ft/ft) | | Capacity (cfs) | Description | | | |
| - | 5.6 | 50 | 0.0200 | 0.15 | | Sheet Flow, Segment A-B | | | |
| | | | | | | Grass: Short n= 0.150 P2= 3.26" | | | |
| | 2.0 | 194 | 0.0550 | 1.64 | | Shallow Concentrated Flow, Segment B-C | | | |
| | | | | | | Short Grass Pasture Kv= 7.0 fps | | | |
| | 0.2 | 47 | 0.0050 | 3.79 | 2.98 | | | | |
| | | | | | | 12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25' | | | |
| | ~ ~ ~ | 050 | 0.0400 | 4 50 | | n= 0.011 Concrete pipe, straight & clean | | | |
| | 2.8 | 253 | 0.0100 | 1.50 | | Shallow Concentrated Flow, Segment D-E Grassed Waterway Kv= 15.0 fps | | | |
| - | 10.6 | 511 | Total | | | Glassed Waterway IN- 13.0 lps | | | |
| | 10.6 | 544 | Total | | | | | | |

Subcatchment PR-4: Subcatchment to BVW



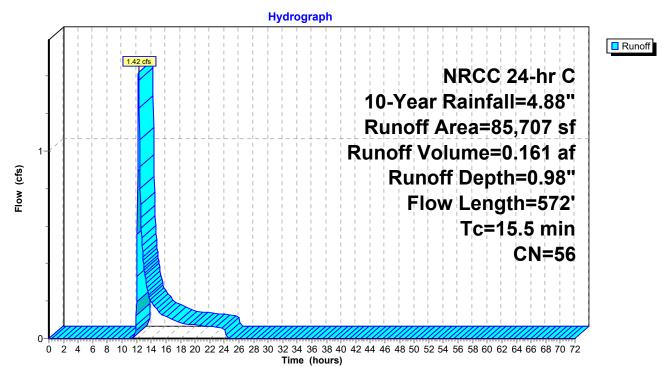
Summary for Subcatchment PR3: To Blackstone Street

Runoff = 1.42 cfs @ 12.27 hrs, Volume= 0.161 af, Depth= 0.98"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 10-Year Rainfall=4.88"

| A | rea (sf) | CN D | escription | | |
|--------------|----------|---------|------------|-------------|--|
| | 67,471 | 55 V | loods, Go | od, HSG B | |
| | 18,236 | 61 > | 75% Gras | s cover, Go | ood, HSG B |
| | 85,707 | 56 V | Veighted A | verage | |
| | 85,707 | 1 | 00.00% Pe | ervious Are | а |
| | | | | | |
| Tc | Length | Slope | Velocity | Capacity | Description |
| <u>(min)</u> | (feet) | (ft/ft) | (ft/sec) | (cfs) | |
| 7.8 | 50 | 0.0610 | 0.11 | | Sheet Flow, Segment A-B |
| | | | | | Woods: Light underbrush n= 0.400 P2= 3.26" |
| 2.8 | 215 | 0.0640 | 1.26 | | Shallow Concentrated Flow, Segment B-C |
| | | | | | Woodland Kv= 5.0 fps |
| 2.2 | 103 | 0.0240 | 0.77 | | Shallow Concentrated Flow, Segment C-D |
| | | | | | Woodland Kv= 5.0 fps |
| 2.7 | 204 | 0.0320 | 1.25 | | Shallow Concentrated Flow, Segment D-E |
| | | | | | Short Grass Pasture Kv= 7.0 fps |
| 15.5 | 572 | Total | | | |

Subcatchment PR3: To Blackstone Street



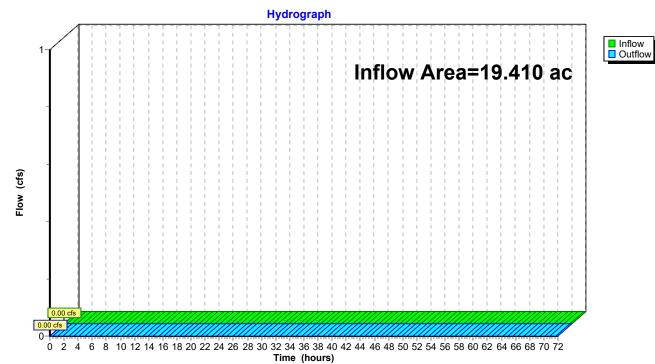
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Summary for Reach AP 1: Analysis Point - AP1

[40] Hint: Not Described (Outflow=Inflow)

| Inflow Area = | 19.410 ac, | 9.22% Impervious, Int | flow Depth = 0.00" | for 10-Year event |
|---------------|------------|-----------------------|--------------------|----------------------|
| Inflow = | 0.00 cfs @ | 0.00 hrs, Volume= | 0.000 af | |
| Outflow = | 0.00 cfs @ | 0.00 hrs, Volume= | 0.000 af, Att | en= 0%, Lag= 0.0 min |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



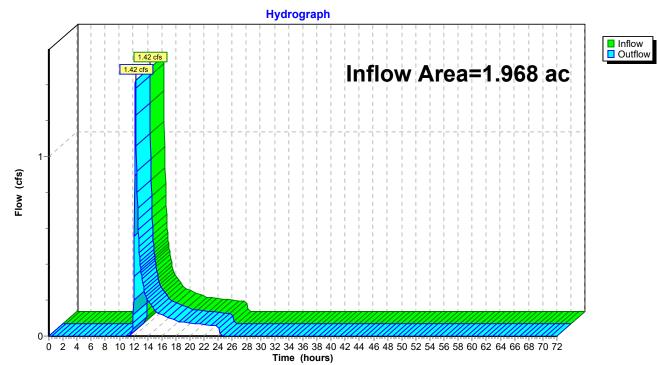
Reach AP 1: Analysis Point - AP1

Summary for Reach AP 2: Analysis Point - AP2

[40] Hint: Not Described (Outflow=Inflow)

| Inflow Area = | 1.968 ac, | 0.00% Impervious, Inflow D | epth = 0.98" | for 10-Year event |
|---------------|------------|----------------------------|----------------|----------------------|
| Inflow = | 1.42 cfs @ | 12.27 hrs, Volume= | 0.161 af | |
| Outflow = | 1.42 cfs @ | 12.27 hrs, Volume= | 0.161 af, Atte | en= 0%, Lag= 0.0 min |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



Reach AP 2: Analysis Point - AP2

Summary for Pond 1P: Infiltration Basin #1

| Inflow Area = | 18.650 ac, | 9.60% Impervious, Infl | ow Depth = 0.94" for 10-Year event |
|---------------|------------|------------------------|-------------------------------------|
| Inflow = | 8.58 cfs @ | 12.14 hrs, Volume= | 1.464 af |
| Outflow = | 3.07 cfs @ | 13.33 hrs, Volume= | 1.464 af, Atten= 64%, Lag= 71.5 min |
| Discarded = | 3.07 cfs @ | 13.33 hrs, Volume= | 1.464 af |
| Primary = | 0.00 cfs @ | 0.00 hrs, Volume= | 0.000 af |
| Secondary = | 0.00 cfs @ | 0.00 hrs, Volume= | 0.000 af |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 306.44' @ 13.33 hrs Surf.Area= 12,280 sf Storage= 10,684 cf Flood Elev= 310.50' Surf.Area= 20,637 sf Storage= 77,211 cf

Plug-Flow detention time= 25.6 min calculated for 1.463 af (100% of inflow) Center-of-Mass det. time= 25.6 min (944.3 - 918.7)

| Volume | Invert | Avail.Stor | rage Storage | e Description |
|------------------|-----------|--------------------------|---------------------------|---|
| #1 | 305.50' | 87,52 | 29 cf Custom | n Stage Data (Prismatic)Listed below (Recalc) |
| Elevatio | | uf Aug a | Inc. Ctore | Curre Chare |
| Elevatio (fee | | rf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) |
| 305.5 | / | <u>(34-11)</u> 10,451 | 0 | 0 |
| 306.0 | | 11,407 | 5,465 | 5,465 |
| 308.0 | | 15,368 | 26,775 | 32,240 |
| 310.0 | | 19,555 | 34,923 | 67,163 |
| 310.5 | | 20,637 | 10,048 | 77,211 |
| 311.0 | 00 | 20,637 | 10,319 | 87,529 |
| Device | Routing | Invert | Outlet Device | es |
| #1 | Primary | 306.00' | 24.0" Round | d Culvert |
| | | | | P, groove end w/headwall, Ke= 0.200 |
| | | | | Invert= 306.00' / 305.53' S= 0.0050 '/' Cc= 0.900 |
| | During | | | ncrete pipe, straight & clean, Flow Area= 3.14 sf |
| #2 | Device 1 | 308.55' | | ' Horiz. Orifice/Grate C= 0.600 Fir flow at low heads |
| #3 | Device 1 | 307.00' | | 0" H Vert. Orifice/Grate C= 0.600 |
| #0 #4 | Discarded | 305.50' | | Exfiltration over Horizontal area |
| | | | | to Groundwater Elevation = 302.70' Phase-In= 0.01' |
| #5 | Secondary | 309.90' | 30.0' long x | 10.0' breadth Broad-Crested Rectangular Weir |
| | | | | 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 |
| | | | Coef. (Englisl | h) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64 |

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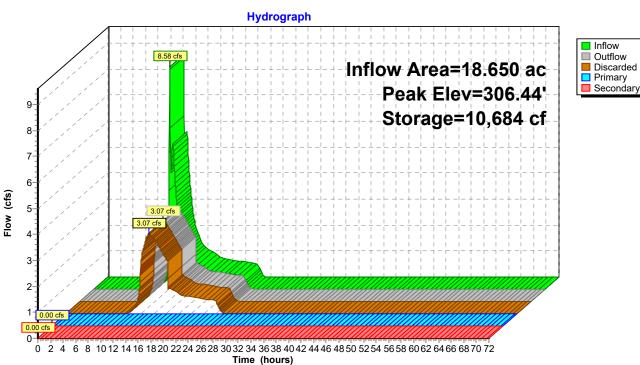
Discarded OutFlow Max=3.07 cfs @ 13.33 hrs HW=306.44' (Free Discharge) **4=Exfiltration** (Controls 3.07 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=305.50' TW=0.00' (Dynamic Tailwater)

2=Orifice/Grate (Controls 0.00 cfs)

-3=Orifice/Grate (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=305.50' TW=0.00' (Dynamic Tailwater) 5=Broad-Crested Rectangular Weir(Controls 0.00 cfs)



Pond 1P: Infiltration Basin #1

Summary for Pond 2P: INLET POND

| Inflow Area = | 15.401 ac, | 0.00% Impervious, Inflow De | epth = 0.70" for 10-Year event |
|---------------|------------|-----------------------------|-----------------------------------|
| Inflow = | 4.09 cfs @ | 12.65 hrs, Volume= | 0.894 af |
| Outflow = | 4.09 cfs @ | 12.65 hrs, Volume= | 0.894 af, Atten= 0%, Lag= 0.0 min |
| Discarded = | 0.00 cfs @ | 24.91 hrs, Volume= | 0.000 af |
| Primary = | 4.09 cfs @ | 12.65 hrs, Volume= | 0.894 af |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 312.00' @ 12.65 hrs Surf.Area= 1,182 sf Storage= 0 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 0.0 min (959.3 - 959.3)

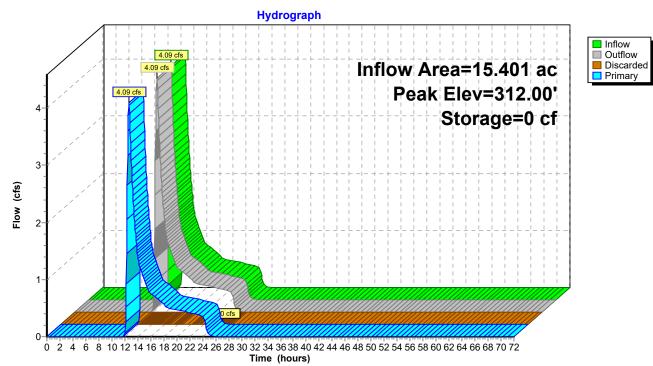
| Volume | Invert | Avail.Sto | rage Storage | Description | |
|----------|--------------|-----------|--|------------------|---------------------------------|
| #1 | 312.00' | 3,48 | 30 cf Custom | Stage Data (P | rismatic)Listed below (Recalc) |
| Elevatio | on Su | ırf.Area | Inc.Store | Cum.Store | |
| (fee | et) | (sq-ft) | (cubic-feet) | (cubic-feet) | |
| 312.0 | 312.00 1,182 | | 0 | 0 | |
| 313.0 | 313.00 1,690 | | 1,436 | 1,436 | |
| 314.00 | | 2,398 | 2,044 | 3,480 | |
| Device | Routing | Invert | Outlet Device | S | |
| #1 | Primary | 310.60' | 24.0" Round Culvert L= 363.4' RCP, square edge headwall, Ke= 0 Inlet / Outlet Invert= 310.60' / 307.00' S= 0.00 n= 0.013 Concrete pipe, bends & connections | | 307.00' S= 0.0099 '/' Cc= 0.900 |
| #2 | Discarded | 312.00' | 8.270 in/hr E | xfiltration over | |

Discarded OutFlow Max=0.00 cfs @ 24.91 hrs HW=312.00' (Free Discharge) **2=Exfiltration** (Controls 0.00 cfs)

Primary OutFlow Max=9.46 cfs @ 12.65 hrs HW=312.00' TW=306.19' (Dynamic Tailwater) **1=Culvert** (Inlet Controls 9.46 cfs @ 4.03 fps)

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Pond 2P: INLET POND



Summary for Pond 23P: Roadside Swale

| Inflow Area = | 0.761 ac, | 0.00% Impervious, Inflow D | epth = 0.18" for 10-Year event |
|---------------|------------|----------------------------|------------------------------------|
| Inflow = | 0.02 cfs @ | 13.06 hrs, Volume= | 0.011 af |
| Outflow = | 0.02 cfs @ | 13.35 hrs, Volume= | 0.011 af, Atten= 4%, Lag= 17.3 min |
| Discarded = | 0.02 cfs @ | 13.35 hrs, Volume= | 0.011 af |
| Primary = | 0.00 cfs @ | 0.00 hrs, Volume= | 0.000 af |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 306.14' @ 13.35 hrs Surf.Area= 98 sf Storage= 7 cf

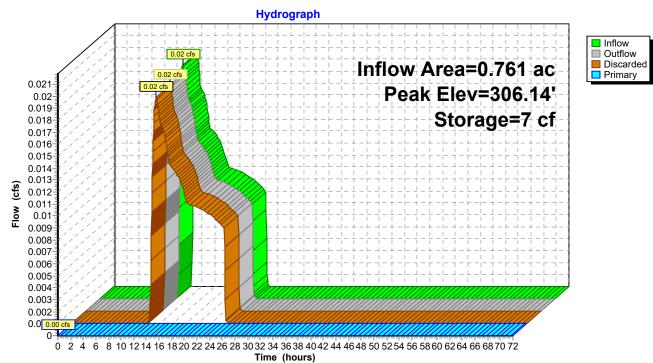
Plug-Flow detention time= 4.0 min calculated for 0.011 af (100% of inflow) Center-of-Mass det. time= 4.0 min (1,053.4 - 1,049.4)

| Volume | Invert | Avail.Sto | rage Storage | e Description | | | |
|---|----------------------|---------------------|--|--|--|--|--|
| #1 | #1 306.00' 1,365 | | 65 cf Custon | n Stage Data (P | rismatic)Listed below (Recalc) | | |
| Elevatio (fee | | urf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) | | | |
| 306.0 | 306.00 0 | | 0 | 0 | | | |
| 307.0 | 307.00 700 | | 350 | 350 | | | |
| 308.0 | 308.00 1,330 | | 1,015 | 1,365 | | | |
| Device | Routing | Invert | Outlet Device | es | | | |
| #1 #2 | Discarded Primary | 306.00' 307.25' | 10.0' long x Head (feet) (2.50 3.00 3. | 2.0' breadth Br 0.20 0.40 0.60 .50 h) 2.54 2.61 2. | Surface area Phase-In= 0.01' oad-Crested Rectangular Weir 0.80 1.00 1.20 1.40 1.60 1.80 2.00 61 2.60 2.66 2.70 2.77 2.89 2.88 | | |
| Discorded OutFlow May-0.02 of @ 12.25 hrs. LIW-206.14! (Free Discharge) | | | | | | | |

Discarded OutFlow Max=0.02 cfs @ 13.35 hrs HW=306.14' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.02 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=306.00' TW=0.00' (Dynamic Tailwater) 2=Broad-Crested Rectangular Weir(Controls 0.00 cfs)





| Pre-Post Development REV 1-26-24 Prepared by Guerriere & Halnon, Inc. HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD Soft | NRCC 24-hr C 25-Year Rainfall=6.15" Printed 2/20/2024 ware Solutions LLC Page 34 |
|---|---|
| Time span=0.00-72.00 hrs Runoff by SCS TR-20 metho Reach routing by Dyn-Stor-Ind method | , dt=0.05 hrs, 1441 points od, UH=SCS, Weighted-CN |
| SubcatchmentPR-1: Subcatchmentto Runoff Are | ea=141,517 sf 55.11% Impervious Runoff Depth=3.12" Tc=6.0 min CN=72 Runoff=12.42 cfs 0.844 af |
| | rea=670,872 sf 0.00% Impervious Runoff Depth=1.29" 1,673' Tc=37.2 min CN=51 Runoff=9.42 cfs 1.658 af |
| SubcatchmentPR-4: Subcatchmentto BVW Runoff Flow Length | Area=33,131 sf 0.00% Impervious Runoff Depth=0.49" n=544' Tc=10.6 min CN=39 Runoff=0.12 cfs 0.031 af |
| | Area=85,707 sf 0.00% Impervious Runoff Depth=1.69" n=572' Tc=15.5 min CN=56 Runoff=2.73 cfs 0.276 af |
| Reach AP 1: Analysis Point - AP1 | Inflow=1.30 cfs 0.124 af Outflow=1.30 cfs 0.124 af |
| Reach AP 2: Analysis Point - AP2 | Inflow=2.73 cfs 0.276 af Outflow=2.73 cfs 0.276 af |
| Pond 1P: Infiltration Basin #1Peak ElevDiscarded=4.45 cfs2.377 afPrimary=1.30 cfs0.124 afS | v=307.55' Storage=25,472 cf Inflow=13.81 cfs 2.501 af econdary=0.00 cfs 0.000 af Outflow=5.75 cfs 2.501 af |
| | ak Elev=312.01' Storage=6 cf Inflow=9.42 cfs 1.658 af Primary=9.30 cfs 1.657 af Outflow=9.42 cfs 1.658 af |
| | Elev=306.55' Storage=105 cf Inflow=0.12 cfs 0.031 af Primary=0.00 cfs 0.000 af Outflow=0.07 cfs 0.031 af |
| | off Volume = 2.810 af Average Runoff Depth = 1.58 Pervious = 19.588 ac 8.38% Impervious = 1.790 ac |

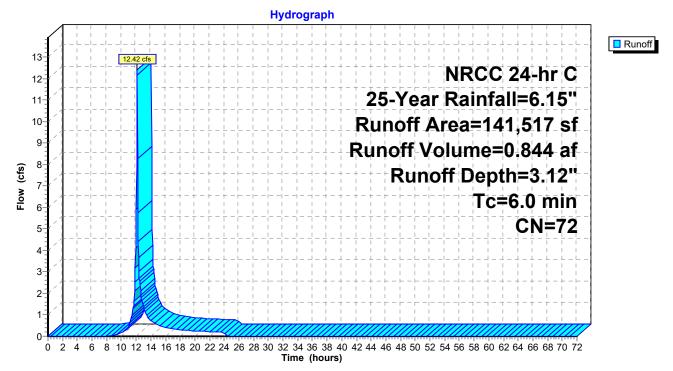
Summary for Subcatchment PR-1: Subcatchment to Basin #1

Runoff = 12.42 cfs @ 12.13 hrs, Volume= 0.844 af, Depth= 3.12"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 25-Year Rainfall=6.15"

| | Area (sf) | CN | Description | | | | | | |
|---|--------------|------|--------------|------------------------|---------------|--|--|--|--|
| * | 38,062 | 98 | Paved road | s w/curbs & | & sewers | | | | |
| * | 19,293 | 98 | Roofs | | | | | | |
| | 63,524 | 39 | >75% Gras | s cover, Go | lood, HSG A | | | | |
| * | 20,638 | 98 | Water Surfa | ace, HSG A | Α | | | | |
| | 141,517 | 72 | Weighted A | Weighted Average | | | | | |
| | 63,524 | | 44.89% Pe | 44.89% Pervious Area | | | | | |
| | 77,993 | | 55.11% lmp | 55.11% Impervious Area | | | | | |
| | | | | | | | | | |
| | Tc Length | | | Capacity | • | | | | |
| _ | (min) (feet) | (ft/ | ft) (ft/sec) | (cfs) | | | | | |
| | 6.0 | | | | Direct Entry, | | | | |

Subcatchment PR-1: Subcatchment to Basin #1



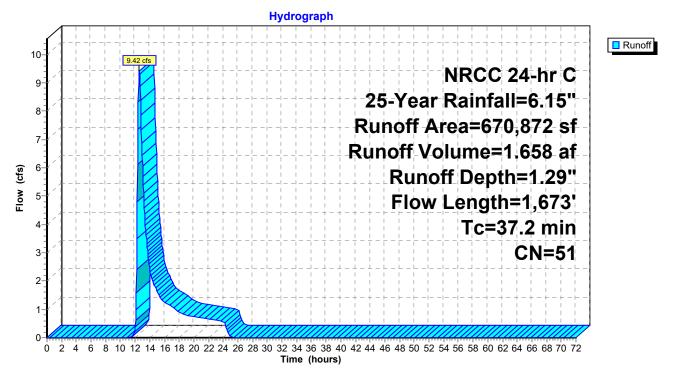
Summary for Subcatchment PR-2: Subcatchment to Basin #2

Runoff = 9.42 cfs @ 12.59 hrs, Volume= 1.658 af, Depth= 1.29"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 25-Year Rainfall=6.15"

| A | rea (sf) | CN D | escription | | |
|-------|----------|---------|------------|-------------|--|
| 5 | 27,673 | 55 V | /oods, Go | od, HSG B | |
| | 96,783 | 30 V | /oods, Go | od, HSG A | |
| | 15,981 | | | | bod, HSG B |
| | 30,435 | 39 > | 75% Gras | s cover, Go | bod, HSG A |
| 6 | 70,872 | | /eighted A | | |
| 6 | 70,872 | 1 | 00.00% Pe | ervious Are | a |
| _ | | | | • • | — • • • |
| , Tc | Length | Slope | Velocity | | Description |
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | |
| 7.0 | 50 | 0.0800 | 0.12 | | Sheet Flow, Segment A-B |
| | 70 | 0 0000 | | | Woods: Light underbrush n= 0.400 P2= 3.26" |
| 0.9 | 78 | 0.0800 | 1.41 | | Shallow Concentrated Flow, Segment B-C |
| 40.7 | 500 | 0 00 40 | 0.77 | | Woodland Kv= 5.0 fps |
| 12.7 | 592 | 0.0240 | 0.77 | | Shallow Concentrated Flow, Segment C-D |
| 14.1 | 581 | 0.0190 | 0.69 | | Woodland Kv= 5.0 fps Shallow Concentrated Flow, Segment D-E |
| 14.1 | 501 | 0.0190 | 0.09 | | Woodland Kv= 5.0 fps |
| 2.0 | 60 | 0.0100 | 0.50 | | Shallow Concentrated Flow, Segment E-F |
| 2.0 | 00 | 0.0100 | 0.00 | | Woodland Kv= 5.0 fps |
| 0.5 | 312 | 0.0230 | 10.92 | 34.31 | Pipe Channel, Segment F-G |
| 0.0 | 0.2 | 0.0200 | 10.02 | 0 110 1 | 24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50' |
| | | | | | n= 0.013 Concrete pipe, straight & clean |
| 37.2 | 1,673 | Total | | | |

Subcatchment PR-2: Subcatchment to Basin #2



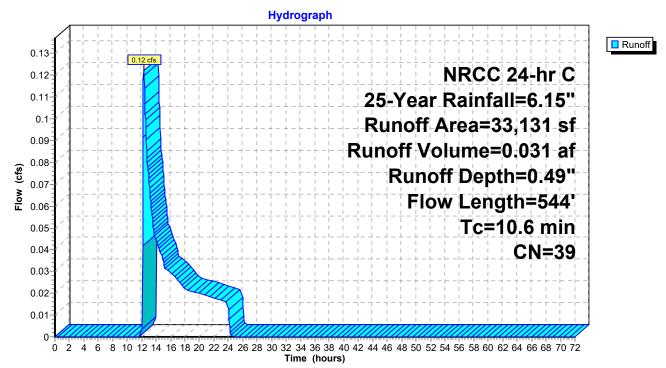
Summary for Subcatchment PR-4: Subcatchment to BVW

Runoff = 0.12 cfs @ 12.31 hrs, Volume= 0.031 af, Depth= 0.49"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 25-Year Rainfall=6.15"

| _ | A | rea (sf) | CN | Description | | |
|---|-------------|------------------|-----------------|-------------|-------------------|---|
| | | 33,131 | 39 | >75% Gras | s cover, Go | bod, HSG A |
| _ | | 33,131 | | 100.00% P | ervious Are | a |
| | Tc (min) | Length (feet) | Slope (ft/ft | | Capacity (cfs) | Description |
| - | 5.6 | 50 | 0.0200 | 0.15 | | Sheet Flow, Segment A-B |
| | | | | | | Grass: Short n= 0.150 P2= 3.26" |
| | 2.0 | 194 | 0.0550 |) 1.64 | | Shallow Concentrated Flow, Segment B-C |
| | | | | | | Short Grass Pasture Kv= 7.0 fps |
| | 0.2 | 47 | 0.0050 |) 3.79 | 2.98 | |
| | | | | | | 12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25' |
| | 0.0 | 050 | 0.0400 | 4 50 | | n= 0.011 Concrete pipe, straight & clean |
| | 2.8 | 253 | 0.0100 |) 1.50 | | Shallow Concentrated Flow, Segment D-E Grassed Waterway Kv= 15.0 fps |
| - | 10.6 | 544 | Total | | | Glassed Waterway INV- 10.0 lps |
| | 10.0 | 044 | rolai | | | |

Subcatchment PR-4: Subcatchment to BVW



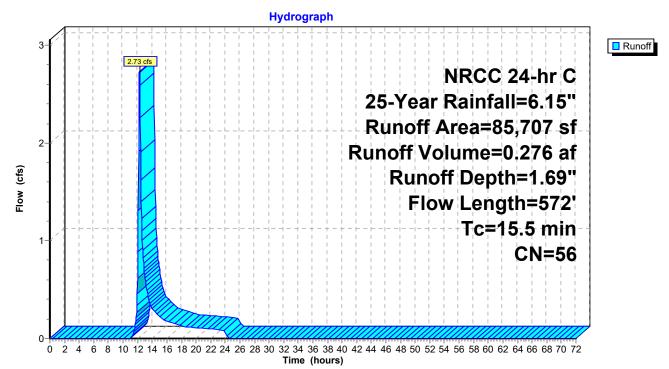
Summary for Subcatchment PR3: To Blackstone Street

Runoff = 2.73 cfs @ 12.26 hrs, Volume= 0.276 af, Depth= 1.69"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 25-Year Rainfall=6.15"

| Α | rea (sf) | CN D | escription | | |
|-------|----------|---------|------------|-------------|--|
| | 67,471 | 55 V | Voods, Go | od, HSG B | |
| | 18,236 | 61 > | 75% Gras | s cover, Go | bod, HSG B |
| | 85,707 | 56 V | Veighted A | verage | |
| | 85,707 | 1 | 00.00% Pe | ervious Are | а |
| | | | | | |
| Tc | Length | Slope | Velocity | Capacity | Description |
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | |
| 7.8 | 50 | 0.0610 | 0.11 | | Sheet Flow, Segment A-B |
| | | | | | Woods: Light underbrush n= 0.400 P2= 3.26" |
| 2.8 | 215 | 0.0640 | 1.26 | | Shallow Concentrated Flow, Segment B-C |
| | | | | | Woodland Kv= 5.0 fps |
| 2.2 | 103 | 0.0240 | 0.77 | | Shallow Concentrated Flow, Segment C-D |
| | | | | | Woodland Kv= 5.0 fps |
| 2.7 | 204 | 0.0320 | 1.25 | | Shallow Concentrated Flow, Segment D-E |
| | | | | | Short Grass Pasture Kv= 7.0 fps |
| 15.5 | 572 | Total | | | |

Subcatchment PR3: To Blackstone Street

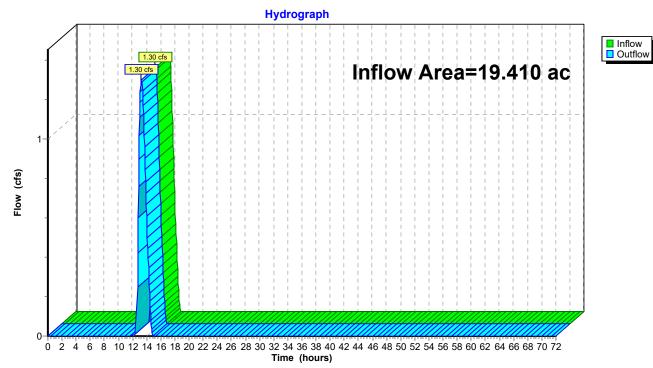


Summary for Reach AP 1: Analysis Point - AP1

[40] Hint: Not Described (Outflow=Inflow)

| Inflow Area = | 19.410 ac, | 9.22% Impervious, Inflow E | Depth = 0.08" | for 25-Year event |
|---------------|------------|----------------------------|----------------|----------------------|
| Inflow = | 1.30 cfs @ | 13.25 hrs, Volume= | 0.124 af | |
| Outflow = | 1.30 cfs @ | 13.25 hrs, Volume= | 0.124 af, Atte | en= 0%, Lag= 0.0 min |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



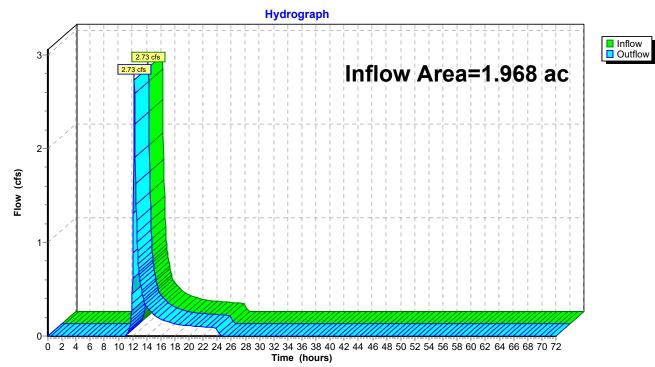
Reach AP 1: Analysis Point - AP1

Summary for Reach AP 2: Analysis Point - AP2

[40] Hint: Not Described (Outflow=Inflow)

| Inflow Area | a = | 1.968 ac, | 0.00% Impervious | , Inflow Depth = 1.6 | 69" for 25-Year event |
|-------------|-----|------------|------------------|------------------------|-------------------------|
| Inflow | = | 2.73 cfs @ | 12.26 hrs, Volum | e= 0.276 af | |
| Outflow | = | 2.73 cfs @ | 12.26 hrs, Volum | e= 0.276 af, | Atten= 0%, Lag= 0.0 min |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



Reach AP 2: Analysis Point - AP2

Summary for Pond 1P: Infiltration Basin #1

| Inflow Area = | 18.650 ac, | 9.60% Impervious, Infl | ow Depth = 1.61" for 25-Year event |
|---------------|-------------|------------------------|-------------------------------------|
| Inflow = | 13.81 cfs @ | 12.14 hrs, Volume= | 2.501 af |
| Outflow = | 5.75 cfs @ | 13.25 hrs, Volume= | 2.501 af, Atten= 58%, Lag= 66.4 min |
| Discarded = | 4.45 cfs @ | 13.25 hrs, Volume= | 2.377 af |
| Primary = | 1.30 cfs @ | 13.25 hrs, Volume= | 0.124 af |
| Secondary = | 0.00 cfs @ | 0.00 hrs, Volume= | 0.000 af |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 307.55' @ 13.25 hrs Surf.Area= 14,470 sf Storage= 25,472 cf Flood Elev= 310.50' Surf.Area= 20,637 sf Storage= 77,211 cf

Plug-Flow detention time= 48.2 min calculated for 2.499 af (100% of inflow) Center-of-Mass det. time= 48.2 min (950.5 - 902.4)

| Volume | Invert | Avail.Stor | rage Storage | e Description | | |
|----------------------|---------------|---|--|--|--|--|
| #1 | 305.50' 87,52 | | 29 cf Custom | n Stage Data (Prismatic)Listed below (Recalc) | | |
| - 1 | | | | | | |
| Elevatio | | rf.Area | Inc.Store | Cum.Store | | |
| (fee | / | <u>(sq-ft)</u> | (cubic-feet) | (cubic-feet) | | |
| 305.5 | | 10,451 | 0 | 0 | | |
| 306.0 | | 11,407 | 5,465 | 5,465 | | |
| 308.0 | | 15,368 | 26,775 | 32,240 | | |
| 310.0 | | 19,555 | 34,923 | 67,163 | | |
| 310.5 | | 20,637 | 10,048 | 77,211 | | |
| 311.0 | 00 | 20,637 | 10,319 | 87,529 | | |
| Davias | Douting | Invert | Outlet Device | | | |
| Device | Routing | Invert | Outlet Device | | | |
| #1 | Primary | 306.00' | 24.0" Round | | | |
| | | | | CP, groove end w/headwall, Ke= 0.200 | | |
| | | | Inlet / Outlet Invert= 306.00' / 305.53' S= 0.0050 '/' Cc= 0.900 | | | |
| | | | | oncrete pipe, straight & clean, Flow Area= 3.14 sf | | |
| #2 | Device 1 | 308.55' | | "Horiz. Orifice/Grate C= 0.600 | | |
| | | | Limited to weir flow at low heads | | | |
| #3 | Device 1 | 307.00' | 12.0" W x 9.0" H Vert. Orifice/Grate C= 0.600 | | | |
| #4 | Discarded | 305.50' | | Exfiltration over Horizontal area | | |
| | | | Conductivity | to Groundwater Elevation = 302.70' Phase-In= 0.01' | | |
| #5 Secondary 309.90' | | 30.0' long x 10.0' breadth Broad-Crested Rectangular Weir | | | | |
| | | | Head (feet) (| 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 | | |
| | | | Coef. (Englis | sh) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64 | | |
| | | | | | | |

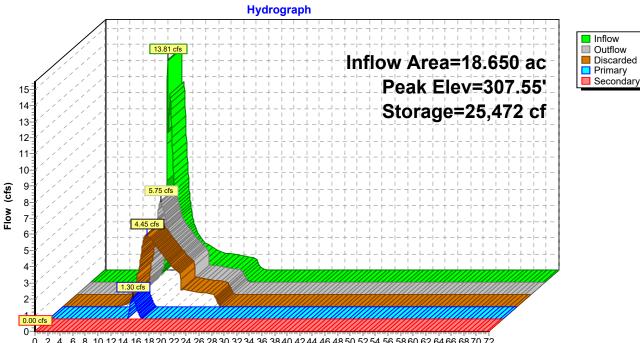
Discarded OutFlow Max=4.45 cfs @ 13.25 hrs HW=307.55' (Free Discharge) **4=Exfiltration** (Controls 4.45 cfs)

Primary OutFlow Max=1.30 cfs @ 13.25 hrs HW=307.55' TW=0.00' (Dynamic Tailwater) **1=Culvert** (Passes 1.30 cfs of 10.05 cfs potential flow)

2=Orifice/Grate (Controls 0.00 cfs)

-3=Orifice/Grate (Orifice Controls 1.30 cfs @ 2.37 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=305.50' TW=0.00' (Dynamic Tailwater) 5=Broad-Crested Rectangular Weir(Controls 0.00 cfs)



Pond 1P: Infiltration Basin #1

0 2 4 6 8 10 12 14 16 18 20 22 24 26 28 30 32 34 36 38 40 42 44 46 48 50 52 54 56 58 60 62 64 66 68 70 72 Time (hours)

Summary for Pond 2P: INLET POND

| Inflow Area = Inflow = Outflow = Discarded = Primary = | 9.42 cfs @ 9.42 cfs @ 0.12 cfs @ | 0.00% Impervious, Infl 12.59 hrs, Volume= 12.59 hrs, Volume= 12.59 hrs, Volume= 12.59 hrs, Volume= | ow Depth = 1.29" for 25-Year event 1.658 af 1.658 af, Atten= 0%, Lag= 0.2 min 0.001 af 1.657 af | | | |
|---|--|--|---|--|--|--|
| Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 312.01' @ 12.59 hrs Surf.Area= 1,185 sf Storage= 6 cf | | | | | | |
| Plug-Flow detention | on time= (not | calculated: outflow prec | edes inflow) | | | |

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 0.0 min (932.7 - 932.7)

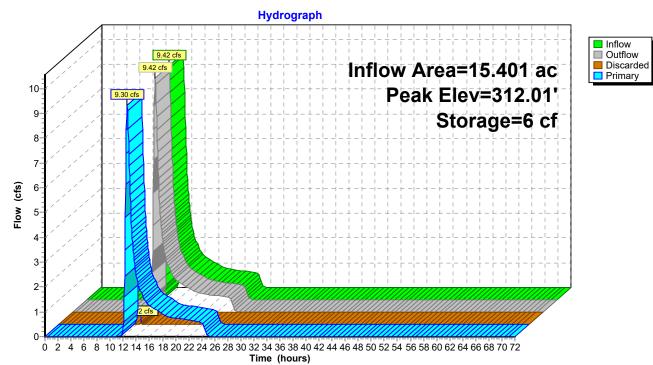
| Volume | Inver | t Avail.Sto | rage Storage | Description | | |
|------------------|---|----------------------|---|---------------------------|--|--|
| #1 | 312.00 |)' 3,48 | 30 cf Custom | n Stage Data (P | rismatic)Listed below (Recalc) | |
| Elevatio (fee | | Surf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) | | |
| 312.0 | , , , , , | | 0 | 0 | | |
| 313.0 | , | | 1,436 | 1,436 | | |
| 314.0 | 314.00 2,398 | | 2,044 | 3,480 | | |
| Device | Routing | Invert | Outlet Device | es | | |
| #1 | Primary | 310.60' | | CP, square edge | e headwall, Ke= 0.500 / 307.00' S= 0.0099 '/' Cc= 0.900 | |
| #2 | Discarded | 312.00' | n= 0.013 Concrete pipe, bends & connections, Flow Area= 3.14 sf 8.270 in/hr Exfiltration over Surface area Conductivity to Groundwater Elevation = 304.67' Phase-In= 0.01' | | | |
| Dieserd | Discourded OutFlow May-0.10 at @ 10 50 hrs. UW-210.01 (Free Discharge) | | | | | |

Discarded OutFlow Max=0.12 cfs @ 12.59 hrs HW=312.01' (Free Discharge) **2=Exfiltration** (Controls 0.12 cfs)

Primary OutFlow Max=9.52 cfs @ 12.59 hrs HW=312.01' TW=306.98' (Dynamic Tailwater) ☐ 1=Culvert (Inlet Controls 9.52 cfs @ 4.04 fps)

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Pond 2P: INLET POND



Summary for Pond 23P: Roadside Swale

| Inflow Area = | 0.761 ac, | 0.00% Impervious, Inflow D | epth = 0.49" for 25-Year event |
|---------------|------------|----------------------------|-------------------------------------|
| Inflow = | 0.12 cfs @ | 12.31 hrs, Volume= | 0.031 af |
| Outflow = | 0.07 cfs @ | 12.98 hrs, Volume= | 0.031 af, Atten= 40%, Lag= 40.4 min |
| Discarded = | 0.07 cfs @ | 12.98 hrs, Volume= | 0.031 af |
| Primary = | 0.00 cfs @ | 0.00 hrs, Volume= | 0.000 af |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 306.55' @ 12.98 hrs Surf.Area= 384 sf Storage= 105 cf

Plug-Flow detention time= 13.2 min calculated for 0.031 af (100% of inflow) Center-of-Mass det. time= 13.2 min (992.6 - 979.5)

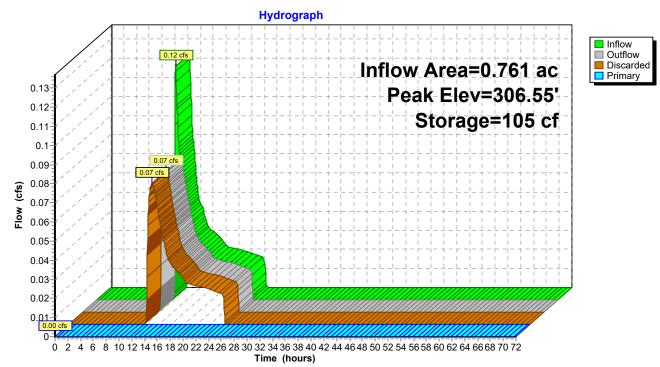
| Volume | Invert | Avail.Sto | rage Storage | Description | |
|--|---------------------------------|--|--|--|---|
| #1 | 306.00' | 1,36 | 65 cf Custom | n Stage Data (P | rismatic)Listed below (Recalc) |
| Elevatio (fee 306.0 307.0 308.0 |)0 00 00 | urf.Area (sq-ft) 0 700 1,330 | Inc.Store (cubic-feet) 0 350 1,015 | Cum.Store (cubic-feet) 0 350 1,365 | |
| Device #1 #2 | Routing Discarded Primary | Invert 306.00' 307.25' | 10.0' long x Head (feet) (2.50 3.00 3. | xfiltration over 2.0' breadth Br 0.20 0.40 0.60 50 h) 2.54 2.61 2. | Surface area Phase-In= 0.01' road-Crested Rectangular Weir 0.80 1.00 1.20 1.40 1.60 1.80 2.00 61 2.60 2.66 2.70 2.77 2.89 2.88 |
| Discarded OutFlow Max=0.07 cfs @ 12.98 hrs HW=306.55' (Free Discharge) | | | | | |

1=Exfiltration (Exfiltration Controls 0.07 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=306.00' TW=0.00' (Dynamic Tailwater) —2=Broad-Crested Rectangular Weir(Controls 0.00 cfs)

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Pond 23P: Roadside Swale



| Pre-Post Development REV 1-26- Prepared by Guerriere & Halnon, Inc. | Printed 2/20/2024 |
|---|---|
| HydroCAD® 10.00-21 s/n 10299 © 2018 Hy | droCAD Software Solutions LLC Page 48 |
| Runoff by SCS | 00-72.00 hrs, dt=0.05 hrs, 1441 points TR-20 method, UH=SCS, Weighted-CN Ind method . Pond routing by Dyn-Stor-Ind method |
| SubcatchmentPR-1: Subcatchmentto | Runoff Area=141,517 sf 55.11% Impervious Runoff Depth=5.35" Tc=6.0 min CN=72 Runoff=21.07 cfs 1.448 af |
| SubcatchmentPR-2: Subcatchmentto | Runoff Area=670,872 sf 0.00% Impervious Runoff Depth=2.83" ow Length=1,673' Tc=37.2 min CN=51 Runoff=23.64 cfs 3.632 af |
| SubcatchmentPR-4: Subcatchmentto E | SVW Runoff Area=33,131 sf 0.00% Impervious Runoff Depth=1.48" Flow Length=544' Tc=10.6 min CN=39 Runoff=0.90 cfs 0.094 af |
| SubcatchmentPR3: To Blackstone Stre | et Runoff Area=85,707 sf 0.00% Impervious Runoff Depth=3.42" Flow Length=572' Tc=15.5 min CN=56 Runoff=5.90 cfs 0.561 af |
| Reach AP 1: Analysis Point - AP1 | Inflow=15.87 cfs 1.339 af Outflow=15.87 cfs 1.339 af |
| Reach AP 2: Analysis Point - AP2 | Inflow=5.90 cfs 0.561 af Outflow=5.90 cfs 0.561 af |
| Pond 1P: Infiltration Basin #1 carded=6.31 cfs 3.721 af Primary=15.79 cfs | Peak Elev=308.91' Storage=47,100 cf Inflow=27.57 cfs 5.050 af 1.329 af Secondary=0.00 cfs 0.000 af Outflow=22.10 cfs 5.050 af |
| Pond 2P: INLET POND Discarded=0.50 cf | Peak Elev=313.74' Storage=2,886 cf Inflow=23.64 cfs 3.632 af s 0.031 af Primary=22.14 cfs 3.601 af Outflow=22.64 cfs 3.632 af |
| Pond 23P: Roadside Swale Discarded=0.17 | Peak Elev=307.32' Storage=603 cf Inflow=0.90 cfs 0.094 af cfs 0.083 af Primary=0.42 cfs 0.011 af Outflow=0.59 cfs 0.094 af |
| Total Runoff Area = 21.3 | 78 ac Runoff Volume = 5.735 af Average Runoff Depth = 3.2 91.62% Pervious = 19.588 ac 8.38% Impervious = 1.790 a |

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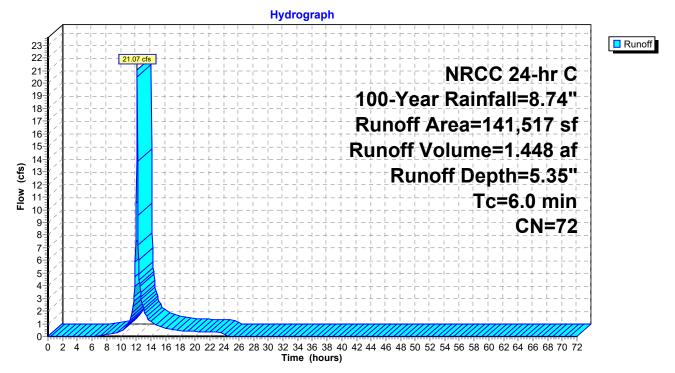
Summary for Subcatchment PR-1: Subcatchment to Basin #1

Runoff = 21.07 cfs @ 12.13 hrs, Volume= 1.448 af, Depth= 5.35"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 100-Year Rainfall=8.74"

| _ | Area (sf) | CN | Description | Description | | | | | |
|---|--------------|------|--------------------|------------------------|---------------|--|--|--|--|
| * | 38,062 | 98 | Paved road | s w/curbs & | & sewers | | | | |
| * | 19,293 | 98 | Roofs | | | | | | |
| | 63,524 | 39 | >75% Gras | s cover, Go | lood, HSG A | | | | |
| * | 20,638 | 98 | Water Surfa | ace, HSG A | Α | | | | |
| | 141,517 | 72 | Weighted A | verage | | | | | |
| | 63,524 | | 44.89% Pei | vious Area | а | | | | |
| | 77,993 | | 55.11% Imp | 55.11% Impervious Area | | | | | |
| | | | | | | | | | |
| | Tc Length | Slop | | Capacity | 1 | | | | |
| _ | (min) (feet) | (ft/ | ft) (ft/sec) (cfs) | | | | | | |
| | 6.0 | | | | Direct Entry, | | | | |

Subcatchment PR-1: Subcatchment to Basin #1



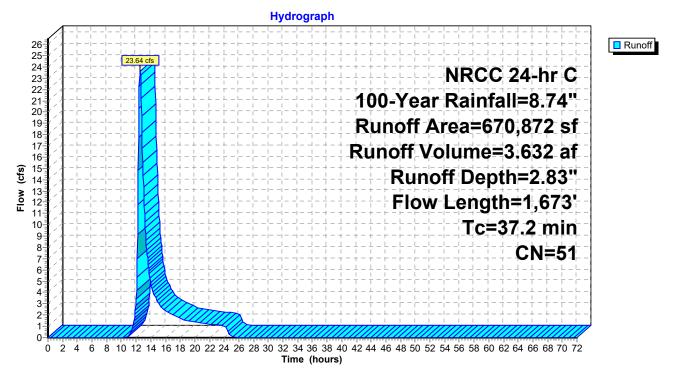
Summary for Subcatchment PR-2: Subcatchment to Basin #2

Runoff = 23.64 cfs @ 12.55 hrs, Volume= 3.632 af, Depth= 2.83"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 100-Year Rainfall=8.74"

| A | rea (sf) | CN D | escription | | | | | |
|-------|----------|---------|-----------------------|-------------|---|--|--|--|
| 5 | 27,673 | 55 V | 55 Woods, Good, HSG B | | | | | |
| | 96,783 | 30 V | 30 Woods, Good, HSG A | | | | | |
| | 15,981 | 61 > | 75% Gras | s cover, Go | bod, HSG B | | | |
| | 30,435 | 39 > | 75% Gras | s cover, Go | ood, HSG A | | | |
| 6 | 70,872 | 51 V | /eighted A | verage | | | | |
| 6 | 70,872 | 1 | 00.00% Pe | ervious Are | а | | | |
| | | | | | | | | |
| Тс | Length | Slope | Velocity | | Description | | | |
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | | | | |
| 7.0 | 50 | 0.0800 | 0.12 | | Sheet Flow, Segment A-B | | | |
| | | | | | Woods: Light underbrush n= 0.400 P2= 3.26" | | | |
| 0.9 | 78 | 0.0800 | 1.41 | | Shallow Concentrated Flow, Segment B-C | | | |
| | | | | | Woodland Kv= 5.0 fps | | | |
| 12.7 | 592 | 0.0240 | 0.77 | | Shallow Concentrated Flow, Segment C-D | | | |
| | | | | | Woodland Kv= 5.0 fps | | | |
| 14.1 | 581 | 0.0190 | 0.69 | | Shallow Concentrated Flow, Segment D-E | | | |
| 0.0 | 00 | 0.0400 | 0.50 | | Woodland Kv= 5.0 fps | | | |
| 2.0 | 60 | 0.0100 | 0.50 | | Shallow Concentrated Flow, Segment E-F | | | |
| 0.5 | 040 | 0 0000 | 40.00 | 04.04 | Woodland Kv= 5.0 fps | | | |
| 0.5 | 312 | 0.0230 | 10.92 | 34.31 | Pipe Channel, Segment F-G | | | |
| | | | | | 24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50' | | | |
| 07.0 | 4.070 | | | | n= 0.013 Concrete pipe, straight & clean | | | |
| 37.2 | 1,673 | Total | | | | | | |

Subcatchment PR-2: Subcatchment to Basin #2



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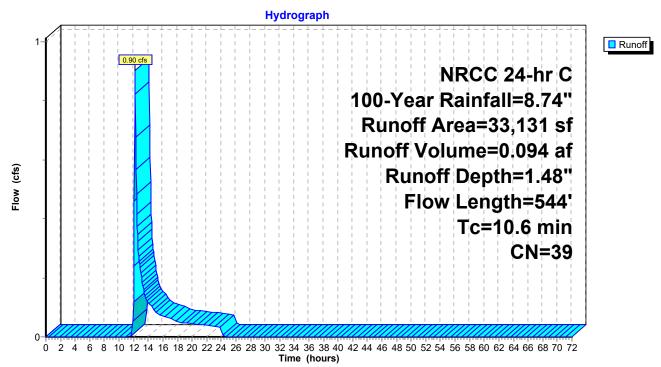
Summary for Subcatchment PR-4: Subcatchment to BVW

Runoff = 0.90 cfs @ 12.21 hrs, Volume= 0.094 af, Depth= 1.48"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 100-Year Rainfall=8.74"

| A | rea (sf) | CN | Description | | | | | |
|-------------|------------------|------------------|----------------------------------|-------------------|--|--|--|--|
| | 33,131 | 39 | 39 >75% Grass cover, Good, HSG A | | | | | |
| | 33,131 | | 100.00% P | ervious Are | a | | | |
| Tc (min) | Length (feet) | Slope (ft/ft) | | Capacity (cfs) | Description | | | |
| 5.6 | 50 | 0.0200 | 0.15 | | Sheet Flow, Segment A-B | | | |
| 2.0 | 194 | 0.0550 | 1.64 | | Grass: Short n= 0.150 P2= 3.26" Shallow Concentrated Flow, Segment B-C Short Grass Pasture Kv= 7.0 fps | | | |
| 0.2 | 47 | 0.0050 | 3.79 | 2.98 | | | | |
| 2.8 | 253 | 0.0100 | 1.50 | | 12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25' n= 0.011 Concrete pipe, straight & clean Shallow Concentrated Flow, Segment D-E Grassed Waterway Kv= 15.0 fps | | | |
| 10.6 | 544 | Total | | | | | | |

Subcatchment PR-4: Subcatchment to BVW



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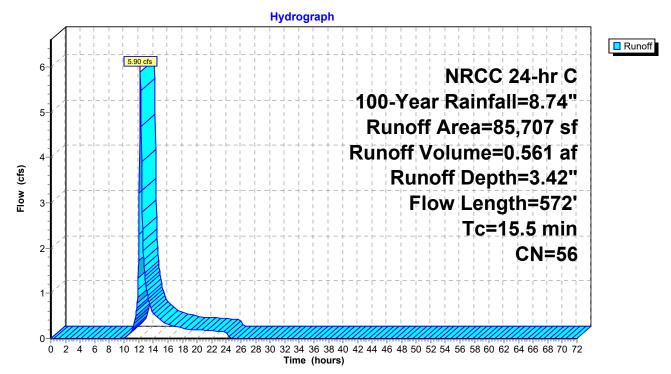
Summary for Subcatchment PR3: To Blackstone Street

Runoff = 5.90 cfs @ 12.25 hrs, Volume= 0.561 af, Depth= 3.42"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 100-Year Rainfall=8.74"

| A | rea (sf) | CN D | escription | | |
|-------|----------|---------|------------|-------------|--|
| | 67,471 | 55 V | Voods, Go | od, HSG B | |
| | 18,236 | 61 > | 75% Gras | s cover, Go | ood, HSG B |
| | 85,707 | 56 V | Veighted A | verage | |
| | 85,707 | 1 | 00.00% Pe | ervious Are | а |
| _ | | | | | |
| Tc | Length | Slope | Velocity | Capacity | Description |
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | |
| 7.8 | 50 | 0.0610 | 0.11 | | Sheet Flow, Segment A-B |
| | | | | | Woods: Light underbrush n= 0.400 P2= 3.26" |
| 2.8 | 215 | 0.0640 | 1.26 | | Shallow Concentrated Flow, Segment B-C |
| | | | | | Woodland Kv= 5.0 fps |
| 2.2 | 103 | 0.0240 | 0.77 | | Shallow Concentrated Flow, Segment C-D |
| | | | | | Woodland Kv= 5.0 fps |
| 2.7 | 204 | 0.0320 | 1.25 | | Shallow Concentrated Flow, Segment D-E |
| | | | | | Short Grass Pasture Kv= 7.0 fps |
| 15.5 | 572 | Total | | | |

Subcatchment PR3: To Blackstone Street

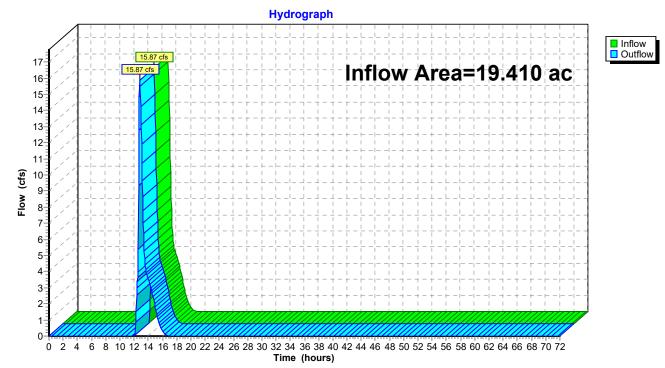


Summary for Reach AP 1: Analysis Point - AP1

[40] Hint: Not Described (Outflow=Inflow)

| Inflow Area = | = 19.410 a | ac, 9.22% Imperviou | s, Inflow Depth = 0.8 | 33" for 100-Year event |
|---------------|------------|----------------------|-----------------------|-------------------------|
| Inflow = | 15.87 cfs | s @ 12.83 hrs, Volur | ne= 1.339 af | |
| Outflow = | 15.87 cfs | s @ 12.83 hrs, Volur | ne= 1.339 af, | Atten= 0%, Lag= 0.0 min |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



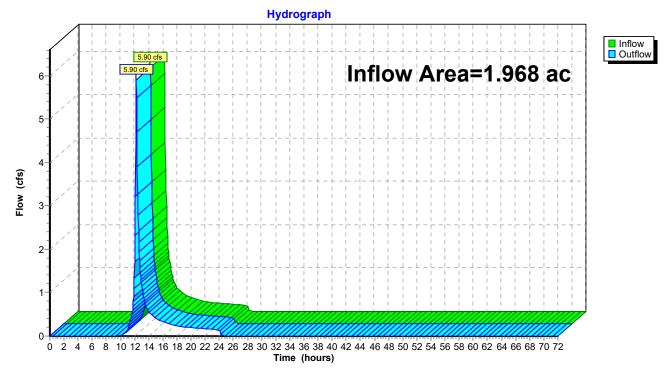
Reach AP 1: Analysis Point - AP1

Summary for Reach AP 2: Analysis Point - AP2

[40] Hint: Not Described (Outflow=Inflow)

| Inflow Area | a = | 1.968 ac, | 0.00% Impervious, Inflow | / Depth = 3.42" | for 100-Year event |
|-------------|-----|------------|--------------------------|-----------------|----------------------|
| Inflow | = | 5.90 cfs @ | 12.25 hrs, Volume= | 0.561 af | |
| Outflow | = | 5.90 cfs @ | 12.25 hrs, Volume= | 0.561 af, Atte | en= 0%, Lag= 0.0 min |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



Reach AP 2: Analysis Point - AP2

Summary for Pond 1P: Infiltration Basin #1

| Inflow Area = | 18.650 ac, | 9.60% Impervious, Infle | ow Depth = 3.25" for 100-Year event |
|---------------|-------------|-------------------------|-------------------------------------|
| Inflow = | 27.57 cfs @ | 12.14 hrs, Volume= | 5.050 af |
| Outflow = | 22.10 cfs @ | 12.83 hrs, Volume= | 5.050 af, Atten= 20%, Lag= 41.1 min |
| Discarded = | 6.31 cfs @ | 12.83 hrs, Volume= | 3.721 af |
| Primary = | 15.79 cfs @ | 12.83 hrs, Volume= | 1.329 af |
| Secondary = | 0.00 cfs @ | 0.00 hrs, Volume= | 0.000 af |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 308.91' @ 12.83 hrs Surf.Area= 17,274 sf Storage= 47,100 cf Flood Elev= 310.50' Surf.Area= 20,637 sf Storage= 77,211 cf

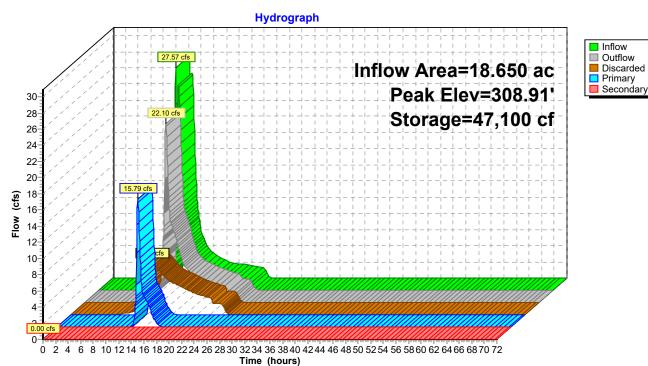
Plug-Flow detention time= 52.1 min calculated for 5.046 af (100% of inflow) Center-of-Mass det. time= 52.0 min (934.8 - 882.8)

| Volume | Invert | Avail.Stor | rage Storage | e Description |
|------------|-----------|----------------|---------------|--|
| #1 | 305.50' | 87,52 | 29 cf Custom | n Stage Data (Prismatic)Listed below (Recalc) |
| - 1 | | | | |
| Elevatio | | rf.Area | Inc.Store | Cum.Store |
| (fee | / | <u>(sq-ft)</u> | (cubic-feet) | (cubic-feet) |
| 305.5 | | 10,451 | 0 | 0 |
| 306.0 | | 11,407 | 5,465 | 5,465 |
| 308.0 | | 15,368 | 26,775 | 32,240 |
| 310.0 | | 19,555 | 34,923 | 67,163 |
| 310.5 | | 20,637 | 10,048 | 77,211 |
| 311.0 | 00 | 20,637 | 10,319 | 87,529 |
| Davias | Douting | Invort | Outlet Device | |
| Device | Routing | Invert | Outlet Device | |
| #1 | Primary | 306.00' | 24.0" Round | |
| | | | | CP, groove end w/headwall, Ke= 0.200 |
| | | | | Invert= 306.00' / 305.53' S= 0.0050 '/' Cc= 0.900 |
| | | | | oncrete pipe, straight & clean, Flow Area= 3.14 sf |
| #2 | Device 1 | 308.55' | | "Horiz. Orifice/Grate C= 0.600 |
| | | | | eir flow at low heads |
| #3 | Device 1 | 307.00' | 12.0" W x 9.0 | 0" H Vert. Orifice/Grate C= 0.600 |
| #4 | Discarded | 305.50' | | Exfiltration over Horizontal area |
| | | | Conductivity | to Groundwater Elevation = 302.70' Phase-In= 0.01' |
| #5 | Secondary | 309.90' | 30.0' long x | 10.0' breadth Broad-Crested Rectangular Weir |
| | | | Head (feet) (| 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 |
| | | | Coef. (Englis | sh) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64 |
| | | | | |

Discarded OutFlow Max=6.31 cfs @ 12.83 hrs HW=308.91' (Free Discharge) **4=Exfiltration** (Controls 6.31 cfs)

Primary OutFlow Max=15.71 cfs @ 12.83 hrs HW=308.91' TW=0.00' (Dynamic Tailwater) 1=Culvert (Passes 15.71 cfs of 20.72 cfs potential flow) 2=Orifice/Grate (Weir Controls 11.25 cfs @ 1.96 fps) 3=Orifice/Grate (Orifice Controls 4.46 cfs @ 5.95 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=305.50' TW=0.00' (Dynamic Tailwater) 5=Broad-Crested Rectangular Weir(Controls 0.00 cfs)



Pond 1P: Infiltration Basin #1

Summary for Pond 2P: INLET POND

| Inflow Area = | 15.401 ac, | 0.00% Impervious, Inflow De | epth = 2.83" for 100-Year event |
|---------------|-------------|-----------------------------|-----------------------------------|
| Inflow = | 23.64 cfs @ | 12.55 hrs, Volume= | 3.632 af |
| Outflow = | 22.64 cfs @ | 12.64 hrs, Volume= | 3.632 af, Atten= 4%, Lag= 5.4 min |
| Discarded = | 0.50 cfs @ | 12.64 hrs, Volume= | 0.031 af |
| Primary = | 22.14 cfs @ | 12.64 hrs, Volume= | 3.601 af |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 313.74' @ 12.64 hrs Surf.Area= 2,216 sf Storage= 2,886 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 0.5 min (904.6 - 904.1)

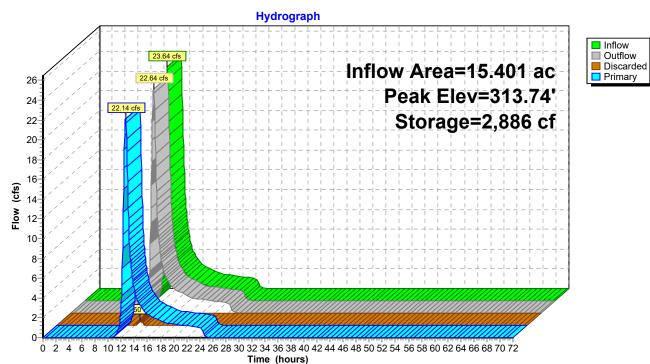
| Volume | Invert | Avail.Sto | rage Storage | Description | | |
|------------|-----------|-----------|------------------|-------------------------------------|---|-----------------|
| #1 | 312.00' | 3,48 | 30 cf Custom | n Stage Data (P | rismatic)Listed below | w (Recalc) |
| Elevatio | on Su | ırf.Area | Inc.Store | Cum.Store | | |
| (fee | | (sq-ft) | (cubic-feet) | (cubic-feet) | | |
| 312.0 | 00 | 1,182 | 0 | 0 | | |
| 313.0 | 00 | 1,690 | 1,436 | 1,436 | | |
| 314.0 | 00 | 2,398 | 2,044 | 3,480 | | |
| Device | Routing | Invert | Outlet Device | s | | |
| #1 | Primary | 310.60' | Inlet / Outlet I | CP, square edge nvert= 310.60' / | e headwall, Ke= 0.50 307.00' S= 0.0099 ds & connections, Fl | '/' Cc= 0.900 |
| #2 | Discarded | 312.00' | 8.270 in/hr E | xfiltration over | | Phase-In= 0.01' |
| D . | | | | | | |

Discarded OutFlow Max=0.50 cfs @ 12.64 hrs HW=313.74' (Free Discharge) **2=Exfiltration** (Controls 0.50 cfs)

Primary OutFlow Max=22.11 cfs @ 12.64 hrs HW=313.74' TW=308.73' (Dynamic Tailwater) **1=Culvert** (Inlet Controls 22.11 cfs @ 7.04 fps)

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Pond 2P: INLET POND



Summary for Pond 23P: Roadside Swale

| Inflow Area = | 0.761 ac, | 0.00% Impervious, Inflow D | Pepth = 1.48" for 100-Year event |
|---------------|------------|----------------------------|------------------------------------|
| Inflow = | 0.90 cfs @ | 12.21 hrs, Volume= | 0.094 af |
| Outflow = | 0.59 cfs @ | 12.37 hrs, Volume= | 0.094 af, Atten= 35%, Lag= 9.8 min |
| Discarded = | 0.17 cfs @ | 12.37 hrs, Volume= | 0.083 af |
| Primary = | 0.42 cfs @ | 12.37 hrs, Volume= | 0.011 af |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 307.32' @ 12.37 hrs Surf.Area= 899 sf Storage= 603 cf

Plug-Flow detention time= 31.8 min calculated for 0.094 af (100% of inflow) Center-of-Mass det. time= 31.7 min (954.3 - 922.5)

| Volume | Invert | Avail.Sto | rage Storage | e Description | | |
|----------|--|---------------------|----------------------------|---|--|--|
| #1 | 306.00' | 1,30 | 65 cf Custon | n Stage Data (P | rismatic)Listed below (Recalc) | |
| Elevatio | t) | urf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) | | |
| 306.0 | - | 0 | 0 | 0 | | |
| 307.0 | - | 700 | 350 | 350 | | |
| 308.0 | 00 | 1,330 | 1,015 | 1,365 | | |
| Device | Routing | Invert | Outlet Device | es | | |
| #1 | Discarded | 306.00' | 8.270 in/hr E | Exfiltration over | Surface area Phase-In= 0.01' | |
| #2 | Primary | 307.25' | 10.0' long x | 2.0' breadth Br | oad-Crested Rectangular Weir | |
| | | 001120 | Head (feet) 2.50 3.00 3 | 0.20 0.40 0.60 .50 :h) 2.54 2.61 2. | 0.80 1.00 1.20 1.40 1.60 1.80 2.00 61 2.60 2.66 2.70 2.77 2.89 2.88 | |
| Discord | Discourded OutElow Max = 0.17 of $(0, 12, 27)$ http://www.commun.commun.commun.com/ | | | | | |

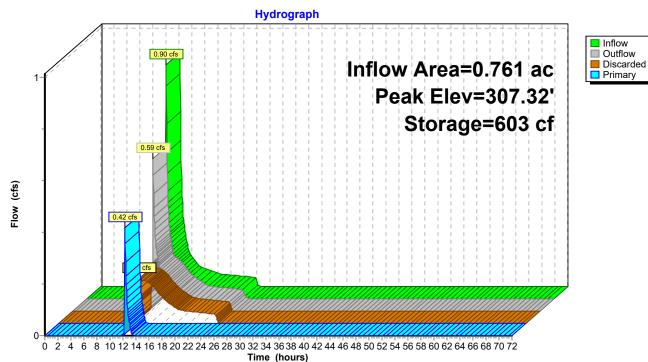
Discarded OutFlow Max=0.17 cfs @ 12.37 hrs HW=307.31' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.17 cfs)

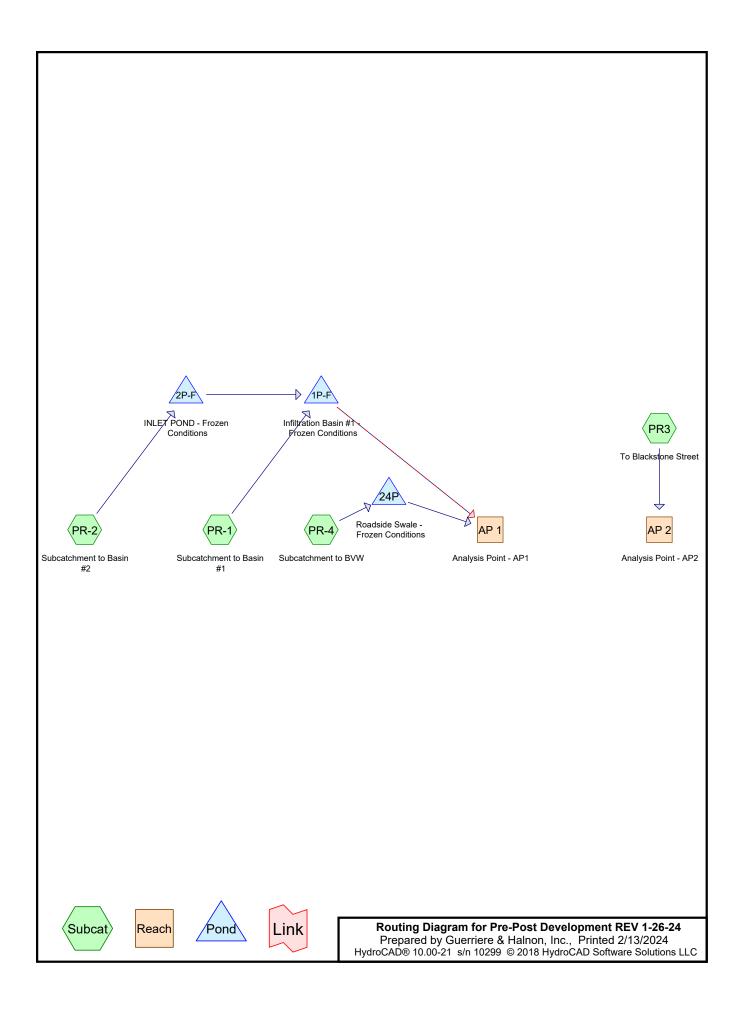
Primary OutFlow Max=0.37 cfs @ 12.37 hrs HW=307.31' TW=0.00' (Dynamic Tailwater) 2=Broad-Crested Rectangular Weir (Weir Controls 0.37 cfs @ 0.62 fps)

NRCC 24-hr C 100-Year Rainfall=8.74" Printed 2/20/2024 ions LLC Page 61

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Pond 23P: Roadside Swale





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Area Listing (selected nodes)

| Area | CN | Description |
|---------|----|--|
| (acres) | | (subcatchment-numbers) |
| 2.918 | 39 | >75% Grass cover, Good, HSG A (PR-1, PR-2, PR-4) |
| 0.786 | 61 | >75% Grass cover, Good, HSG B (PR-2, PR3) |
| 0.874 | 98 | Paved roads w/curbs & sewers (PR-1) |
| 0.443 | 98 | Roofs (PR-1) |
| 0.474 | 98 | Water Surface, HSG A (PR-1) |
| 2.222 | 30 | Woods, Good, HSG A (PR-2) |
| 13.663 | 55 | Woods, Good, HSG B (PR-2, PR3) |
| 21.378 | 54 | TOTAL AREA |

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Soil Listing (selected nodes)

| Soil | Subcatchment |
|-------|---|
| Group | Numbers |
| HSG A | PR-1, PR-2, PR-4 |
| HSG B | PR-2, PR3 |
| HSG C | |
| HSG D | |
| Other | PR-1 |
| | TOTAL AREA |
| | Group HSG A HSG B HSG C HSG D |

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|--------------------|--|---------|
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| HSG-A (acres) | HSG-B (acres) | HSG-C (acres) | HSG-D (acres) | Other (acres) | Total (acres) | Ground Cover | Subcatchment Numbers |
|------------------|------------------|------------------|------------------|------------------|------------------|------------------------------|-------------------------|
| 2.918 | 0.786 | 0.000 | 0.000 | 0.000 | 3.703 | >75% Grass cover, Good | PR |
| 2.010 | 0.700 | 0.000 | 0.000 | 0.000 | 0.700 | | -1, |
| | | | | | | | PR |
| | | | | | | | -2, |
| | | | | | | | PR |
| | | | | | | | -4, |
| | | | | | | | PR |
| | | | | | | | 3 |
| 0.000 | 0.000 | 0.000 | 0.000 | 0.874 | 0.874 | Paved roads w/curbs & sewers | PR |
| | | | | | | | -1 |
| 0.000 | 0.000 | 0.000 | 0.000 | 0.443 | 0.443 | Roofs | PR |
| | | | | | | | -1 |
| 0.474 | 0.000 | 0.000 | 0.000 | 0.000 | 0.474 | Water Surface | PR |
| | | | | | | | -1 |
| 2.222 | 13.663 | 0.000 | 0.000 | 0.000 | 15.884 | Woods, Good | PR |
| | | | | | | | -2, |
| | | | | | | | PR |
| | | | | | | | 3 |
| 5.613 | 14.448 | 0.000 | 0.000 | 1.317 | 21.378 | TOTAL AREA | |

Ground Covers (selected nodes)

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|---|--|--|--|--|--|--|
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| | Line# | Node | In-Invert | Out-Invert | Length | Slope | n | Diam/Width | Height | Inside-Fill |
|---|-------|--------|-----------|------------|--------|---------|-------|------------|----------|-------------|
| _ | | Number | (feet) | (feet) | (feet) | (ft/ft) | | (inches) | (inches) | (inches) |
| | 1 | PR-2 | 0.00 | 0.00 | 312.0 | 0.0230 | 0.013 | 24.0 | 0.0 | 0.0 |
| | 2 | PR-4 | 0.00 | 0.00 | 47.0 | 0.0050 | 0.011 | 12.0 | 0.0 | 0.0 |
| | 3 | 1P-F | 306.00 | 305.52 | 96.0 | 0.0050 | 0.011 | 24.0 | 0.0 | 0.0 |
| | 4 | 2P-F | 310.60 | 307.00 | 363.4 | 0.0099 | 0.013 | 24.0 | 0.0 | 0.0 |

Pipe Listing (selected nodes)

| Pre-Post Development REV 1-26-24 Prepared by Guerriere & Halnon, Inc. HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCA | NRCC 24-hr C 25-Year Rainfall=6.15" Printed 2/13/2024 D Software Solutions LLC Page 6 |
|---|--|
| Runoff by SCS TR-20 | 00 hrs, dt=0.05 hrs, 1441 points method, UH=SCS, Weighted-CN ethod - Pond routing by Dyn-Stor-Ind method |
| SubcatchmentPR-1: Subcatchmentto Run | noff Area=141,517 sf 55.11% Impervious Runoff Depth=3.12" Tc=6.0 min CN=72 Runoff=12.42 cfs 0.844 af |
| | unoff Area=670,872 sf 0.00% Impervious Runoff Depth=1.29" ength=1,673' Tc=37.2 min CN=51 Runoff=9.42 cfs 1.658 af |
| | Runoff Area=33,131 sf 0.00% Impervious Runoff Depth=0.49" Length=544' Tc=11.2 min CN=39 Runoff=0.12 cfs 0.031 af |
| | Runoff Area=85,707 sf 0.00% Impervious Runoff Depth=1.69" Length=572' Tc=15.5 min CN=56 Runoff=2.73 cfs 0.276 af |
| Reach AP 1: Analysis Point - AP1 | Inflow=4.34 cfs 2.110 af Outflow=4.34 cfs 2.110 af |
| Reach AP 2: Analysis Point - AP2 | Inflow=2.73 cfs 0.276 af Outflow=2.73 cfs 0.276 af |
| | ak Elev=308.59' Storage=41,633 cf Inflow=13.81 cfs 2.502 af 1 af Secondary=0.00 cfs 0.000 af Outflow=4.34 cfs 2.091 af |
| | Peak Elev=312.01' Storage=11 cf Inflow=9.42 cfs 1.658 af ert n=0.013 L=363.4' S=0.0099 '/' Outflow=9.41 cfs 1.658 af |
| Pond 24P: Roadside Swale - Frozen | Peak Elev=307.26' Storage=556 cf Inflow=0.12 cfs 0.031 af Outflow=0.04 cfs 0.019 af |
| | |

Total Runoff Area = 21.378 acRunoff Volume = 2.810 afAverage Runoff Depth = 1.58"91.62% Pervious = 19.588 ac8.38% Impervious = 1.790 ac

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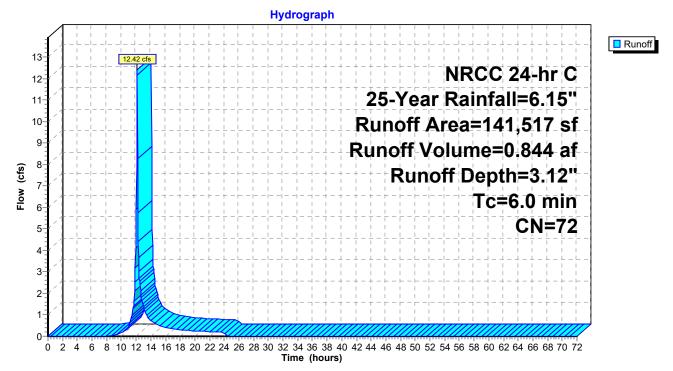
Summary for Subcatchment PR-1: Subcatchment to Basin #1

Runoff = 12.42 cfs @ 12.13 hrs, Volume= 0.844 af, Depth= 3.12"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 25-Year Rainfall=6.15"

| | Area (sf) | CN | Description | | |
|---|--------------|------|--------------|-------------|---------------|
| * | 38,062 | 98 | Paved road | s w/curbs & | & sewers |
| * | 19,293 | 98 | Roofs | | |
| | 63,524 | 39 | >75% Gras | s cover, Go | Good, HSG A |
| * | 20,638 | 98 | Water Surfa | ace, HSG A | Α |
| | 141,517 | 72 | Weighted A | verage | |
| | 63,524 | | 44.89% Per | vious Area | а |
| | 77,993 | | 55.11% lmp | pervious Ar | rea |
| | | | | | |
| | Tc Length | Slop | | Capacity | |
| _ | (min) (feet) | (ft/ | ft) (ft/sec) | (cfs) | |
| | 6.0 | | | | Direct Entry, |

Subcatchment PR-1: Subcatchment to Basin #1



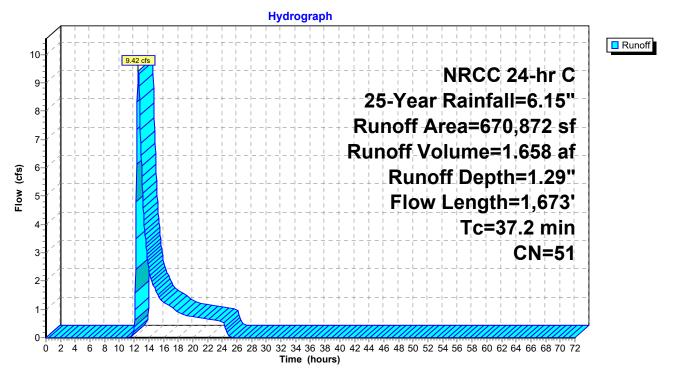
Summary for Subcatchment PR-2: Subcatchment to Basin #2

Runoff = 9.42 cfs @ 12.59 hrs, Volume= 1.658 af, Depth= 1.29"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 25-Year Rainfall=6.15"

| A | rea (sf) | CN D | escription | | | | |
|-------|----------|-----------------------|------------|-------------|---|--|--|
| 5 | 27,673 | 55 Woods, Good, HSG B | | | | | |
| | 96,783 | 30 V | /oods, Go | od, HSG A | | | |
| | 15,981 | | | | ood, HSG B | | |
| | 30,435 | 39 > | 75% Gras | s cover, Go | ood, HSG A | | |
| 6 | 70,872 | 51 V | /eighted A | verage | | | |
| 6 | 70,872 | 1 | 00.00% P | ervious Are | а | | |
| | | | | | | | |
| Тс | Length | Slope | Velocity | | Description | | |
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | | | |
| 7.0 | 50 | 0.0800 | 0.12 | | Sheet Flow, Segment A-B | | |
| | | | | | Woods: Light underbrush n= 0.400 P2= 3.26" | | |
| 0.9 | 78 | 0.0800 | 1.41 | | Shallow Concentrated Flow, Segment B-C | | |
| | | | | | Woodland Kv= 5.0 fps | | |
| 12.7 | 592 | 0.0240 | 0.77 | | Shallow Concentrated Flow, Segment C-D | | |
| | | | | | Woodland Kv= 5.0 fps | | |
| 14.1 | 581 | 0.0190 | 0.69 | | Shallow Concentrated Flow, Segment D-E | | |
| 0.0 | 00 | 0.0400 | 0.50 | | Woodland Kv= 5.0 fps | | |
| 2.0 | 60 | 0.0100 | 0.50 | | Shallow Concentrated Flow, Segment E-F | | |
| 0.5 | 040 | 0 0000 | 40.00 | 04.04 | Woodland Kv= 5.0 fps | | |
| 0.5 | 312 | 0.0230 | 10.92 | 34.31 | Pipe Channel, Segment F-G | | |
| | | | | | 24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50' | | |
| | 4 070 | - · · | | | n= 0.013 Concrete pipe, straight & clean | | |
| 37.2 | 1,673 | Total | | | | | |

Subcatchment PR-2: Subcatchment to Basin #2



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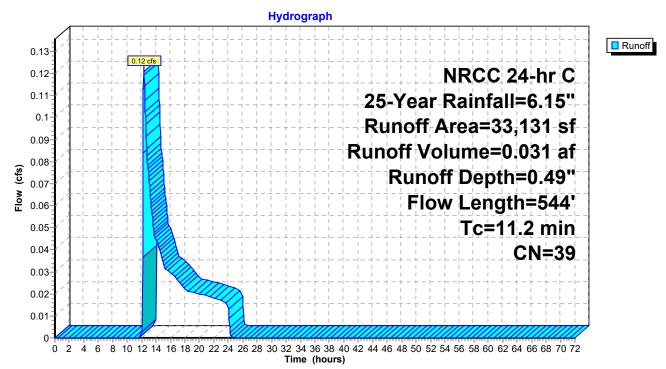
Summary for Subcatchment PR-4: Subcatchment to BVW

Runoff = 0.12 cfs @ 12.32 hrs, Volume= 0.031 af, Depth= 0.49"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 25-Year Rainfall=6.15"

| A | rea (sf) | CN | Description | | | | | |
|-------------|------------------|-------------------------------------|-------------|-------------------|--|--|--|--|
| | 33,131 | 31 39 >75% Grass cover, Good, HSG A | | | | | | |
| | 33,131 | | 100.00% P | ervious Are | a | | | |
| Tc (min) | Length (feet) | Slope (ft/ft) | | Capacity (cfs) | Description | | | |
| 5.6 | 50 | 0.0200 | 0.15 | | Sheet Flow, Segment A-B | | | |
| 2.0 | 194 | 0.0550 | 1.64 | | Grass: Short n= 0.150 P2= 3.26" Shallow Concentrated Flow, Segment B-C | | | |
| 0.2 | 47 | 0.0050 | 3.79 | 2.98 | Short Grass Pasture Kv= 7.0 fps Pipe Channel, RCP_Round 12'' 12.0'' Round Area= 0.8 sf Perim= 3.1' r= 0.25' | | | |
| 3.4 | 253 | 0.0070 | 1.25 | | n= 0.011 Concrete pipe, straight & clean Shallow Concentrated Flow, Segment D-E Grassed Waterway Kv= 15.0 fps | | | |
| 11.2 | 544 | Total | | | | | | |

Subcatchment PR-4: Subcatchment to BVW



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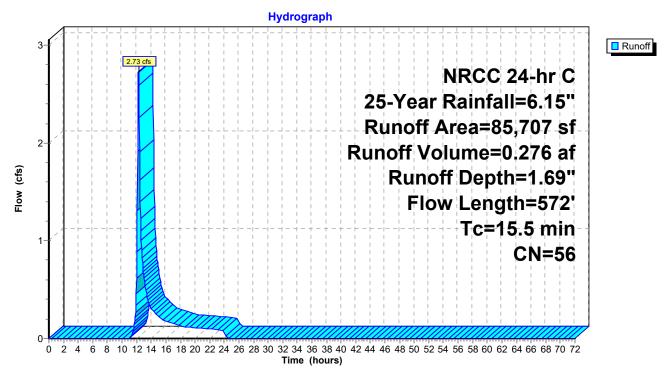
Summary for Subcatchment PR3: To Blackstone Street

Runoff = 2.73 cfs @ 12.26 hrs, Volume= 0.276 af, Depth= 1.69"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 25-Year Rainfall=6.15"

| A | rea (sf) | CN D | escription | | |
|-------|----------|---------|------------|-------------|--|
| | 67,471 | 55 V | Voods, Go | od, HSG B | |
| | 18,236 | 61 > | 75% Gras | s cover, Go | ood, HSG B |
| | 85,707 | 56 V | Veighted A | verage | |
| | 85,707 | 1 | 00.00% Pe | ervious Are | а |
| _ | | | | | |
| Tc | Length | Slope | Velocity | Capacity | Description |
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | |
| 7.8 | 50 | 0.0610 | 0.11 | | Sheet Flow, Segment A-B |
| | | | | | Woods: Light underbrush n= 0.400 P2= 3.26" |
| 2.8 | 215 | 0.0640 | 1.26 | | Shallow Concentrated Flow, Segment B-C |
| | | | | | Woodland Kv= 5.0 fps |
| 2.2 | 103 | 0.0240 | 0.77 | | Shallow Concentrated Flow, Segment C-D |
| | | | | | Woodland Kv= 5.0 fps |
| 2.7 | 204 | 0.0320 | 1.25 | | Shallow Concentrated Flow, Segment D-E |
| | | | | | Short Grass Pasture Kv= 7.0 fps |
| 15.5 | 572 | Total | | | |

Subcatchment PR3: To Blackstone Street

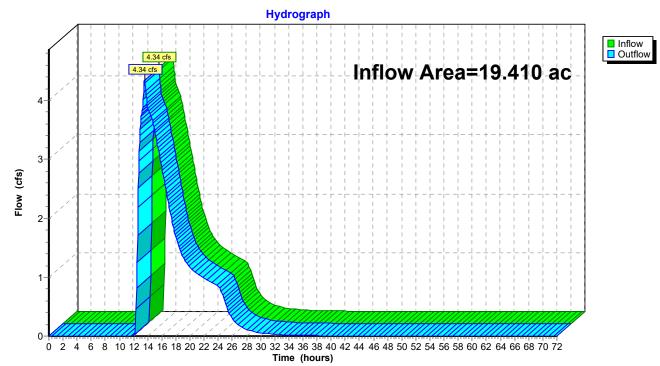


Summary for Reach AP 1: Analysis Point - AP1

[40] Hint: Not Described (Outflow=Inflow)

| Inflow Area = | 19.410 ac, | 9.22% Impervious, Inflow E | Depth = 1.30" | for 25-Year event |
|---------------|------------|----------------------------|----------------|----------------------|
| Inflow = | 4.34 cfs @ | 13.56 hrs, Volume= | 2.110 af | |
| Outflow = | 4.34 cfs @ | 13.56 hrs, Volume= | 2.110 af, Atte | en= 0%, Lag= 0.0 min |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



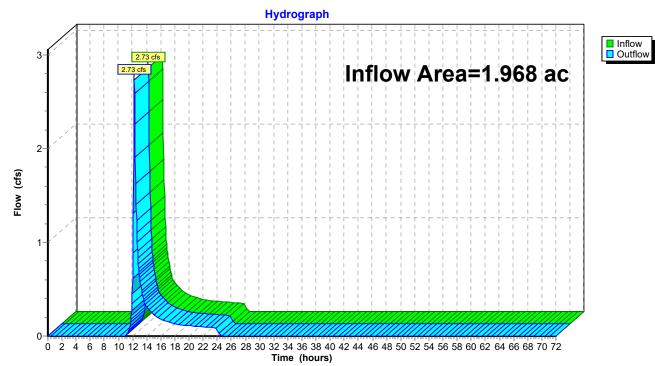
Reach AP 1: Analysis Point - AP1

Summary for Reach AP 2: Analysis Point - AP2

[40] Hint: Not Described (Outflow=Inflow)

| Inflow Area | a = | 1.968 ac, | 0.00% Impervious | , Inflow Depth = 1.6 | 69" for 25-Year event |
|-------------|-----|------------|------------------|----------------------|-------------------------|
| Inflow | = | 2.73 cfs @ | 12.26 hrs, Volum | e= 0.276 af | |
| Outflow | = | 2.73 cfs @ | 12.26 hrs, Volum | e= 0.276 af, | Atten= 0%, Lag= 0.0 min |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



Reach AP 2: Analysis Point - AP2

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Summary for Pond 1P-F: Infiltration Basin #1 - Frozen Conditions

| Inflow Area = | 18.650 ac, | 9.60% Impervious, Inflow E | Depth = 1.61" for 25-Year event |
|---------------|-------------|----------------------------|-------------------------------------|
| Inflow = | 13.81 cfs @ | 12.14 hrs, Volume= | 2.502 af |
| Outflow = | 4.34 cfs @ | 13.56 hrs, Volume= | 2.091 af, Atten= 69%, Lag= 84.9 min |
| Primary = | 4.34 cfs @ | 13.56 hrs, Volume= | 2.091 af |
| Secondary = | 0.00 cfs @ | 0.00 hrs, Volume= | 0.000 af |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 308.59'@ 13.56 hrs Surf.Area= 16,598 sf Storage= 41,633 cf Flood Elev= 310.50' Surf.Area= 20,637 sf Storage= 77,211 cf

Plug-Flow detention time= 214.5 min calculated for 2.091 af (84% of inflow) Center-of-Mass det. time= 137.9 min (1,040.2 - 902.3)

| Volume | Invert | Avail.Stor | rage Storage | Description | | | | |
|----------|---|------------|-------------------|--------------------|--------------------------------|--|--|--|
| #1 | 305.50' | 87,52 | 29 cf Custom | Stage Data (Pris | smatic)Listed below (Recalc) | | | |
| | | | | | | | | |
| Elevatio | on Surf | .Area | Inc.Store | Cum.Store | | | | |
| (fee | et) (| (sq-ft) | (cubic-feet) | (cubic-feet) | | | | |
| 305.5 | 50 1 | 0,451 | 0 | 0 | | | | |
| 306.0 | 00 1 | 1,407 | 5,465 | 5,465 | | | | |
| 308.0 | 00 1 | 5,368 | 26,775 | 32,240 | | | | |
| 310.0 | 00 1 | 9,555 | 34,923 | 67,163 | | | | |
| 310.5 | 50 2 | 0,637 | 10,048 | 77,211 | | | | |
| 311.0 | 0 2 | 0,637 | 10,319 | 87,529 | | | | |
| | | | | | | | | |
| Device | Routing | Invert | Outlet Devices | 5 | | | | |
| #1 | Primary | 306.00' | 24.0" Round | Culvert | | | | |
| | - | | L= 96.0' RCF | P, groove end w/h | neadwall, Ke= 0.200 | | | |
| | | | Inlet / Outlet Ir | nvert= 306.00' / 3 | 05.52' S= 0.0050 '/' Cc= 0.900 | | | |
| | | | n= 0.011 Con | crete pipe, straig | ht & clean, Flow Area= 3.14 sf | | | |
| #2 | Device 1 | 308.55' | 48.0" x 48.0" | Horiz. Orifice/G | rate C= 0.600 | | | |
| | | | Limited to weil | r flow at low head | ls | | | |
| #3 | Device 1 | 307.00' | 12.0" W x 9.0 | " H Vert. Orifice/ | /Grate C= 0.600 | | | |
| #4 | Secondary | 309.90' | 10.0' long x 1 | 10.0' breadth Bro | oad-Crested Rectangular Weir | | | |
| | | | Head (feet) 0. | .20 0.40 0.60 0. | .80 1.00 1.20 1.40 1.60 | | | |
| | | | Coef. (English |) 2.49 2.56 2.70 | 0 2.69 2.68 2.69 2.67 2.64 | | | |
| | Primary OutElow May - 4 24 at $(2.12 \text{ from } 1.10)$ - 200 EQL TM-0.001 (Dynamic Tailwater) | | | | | | | |

Primary OutFlow Max=4.34 cfs @ 13.56 hrs HW=308.59' TW=0.00' (Dynamic Tailwater)

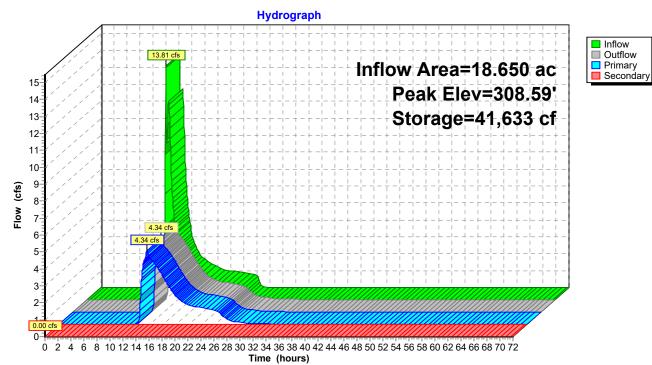
-1=Culvert (Passes 4.34 cfs of 19.04 cfs potential flow)

2=Orifice/Grate (Weir Controls 0.38 cfs @ 0.63 fps)

-3=Orifice/Grate (Orifice Controls 3.96 cfs @ 5.28 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=305.50' TW=0.00' (Dynamic Tailwater) 4=Broad-Crested Rectangular Weir(Controls 0.00 cfs)

Pond 1P-F: Infiltration Basin #1 - Frozen Conditions



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Summary for Pond 2P-F: INLET POND - Frozen Conditions

| Inflow Area = | 15.401 ac, | 0.00% Impervious, Inflov | w Depth = 1.29" for 25-Year event | |
|---------------|------------|--------------------------|-----------------------------------|-----|
| Inflow = | 9.42 cfs @ | 12.59 hrs, Volume= | 1.658 af | |
| Outflow = | 9.41 cfs @ | 12.60 hrs, Volume= | 1.658 af, Atten= 0%, Lag= 0.4 min | i i |
| Primary = | 9.41 cfs @ | 12.60 hrs, Volume= | 1.658 af | |

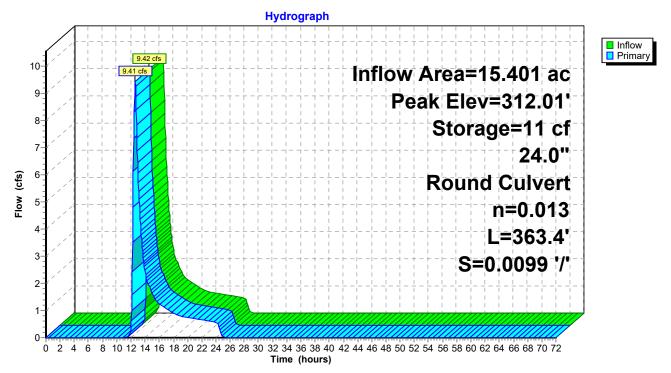
Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 312.01' @ 12.60 hrs Surf.Area= 1,187 sf Storage= 11 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 0.0 min (932.7 - 932.7)

| Volume | Inve | ert Avail.Sto | rage Storage [| Description | |
|---|---------|----------------------|---------------------------|---------------------------|--|
| #1 | 312.0 | 0' 3,48 | B0 cf Custom | Stage Data (Pri | smatic)Listed below (Recalc) |
| Elevation (feet) | | Surf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) | |
| 312.00 | | 1,182 | 0 | 0 | |
| 313.00 | | 1,690 | 1,436 | 1,436 | |
| 314.00 | | 2,398 | 2,044 | 3,480 | |
| Device R | Routing | Invert | Outlet Devices | 5 | |
| #1 F | Primary | 310.60' | 24.0" Round | Culvert | |
| | • | | L= 363.4' RC | P, square edge | headwall, Ke= 0.500 |
| | | | Inlet / Outlet In | vert= 310.60 / 3 | 807.00' S= 0.0099 '/' Cc= 0.900 s & connections, Flow Area= 3.14 sf |
| Primary OutElow Max-0.56 atc. $(2.60 \text{ brg} + 1)/(-212.01!)$ T/(-207.77!) (Dynamic Tailwater) | | | | | |

Primary OutFlow Max=9.56 cfs @ 12.60 hrs HW=312.01' TW=307.77' (Dynamic Tailwater) **1=Culvert** (Inlet Controls 9.56 cfs @ 4.04 fps)

Pond 2P-F: INLET POND - Frozen Conditions



Summary for Pond 24P: Roadside Swale - Frozen Conditions

| Inflow Area = | 0.761 ac, 0.00% Impervious, Inflow | Depth = 0.49" for 25-Year event |
|---------------|------------------------------------|--------------------------------------|
| Inflow = | 0.12 cfs @ 12.32 hrs, Volume= | 0.031 af |
| Outflow = | 0.04 cfs @ 14.62 hrs, Volume= | 0.019 af, Atten= 68%, Lag= 138.3 min |
| Primary = | 0.04 cfs @ 14.62 hrs, Volume= | 0.019 af |

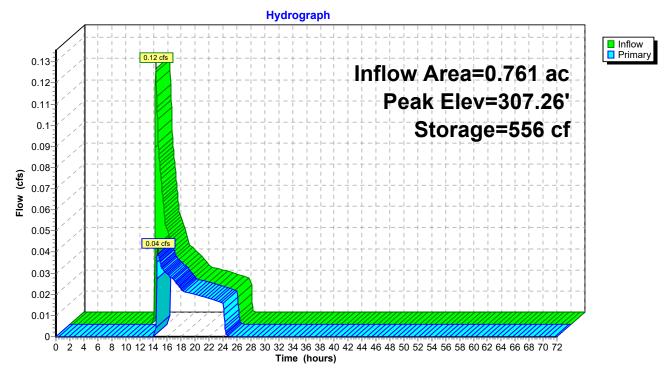
Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 307.26' @ 14.62 hrs Surf.Area= 866 sf Storage= 556 cf

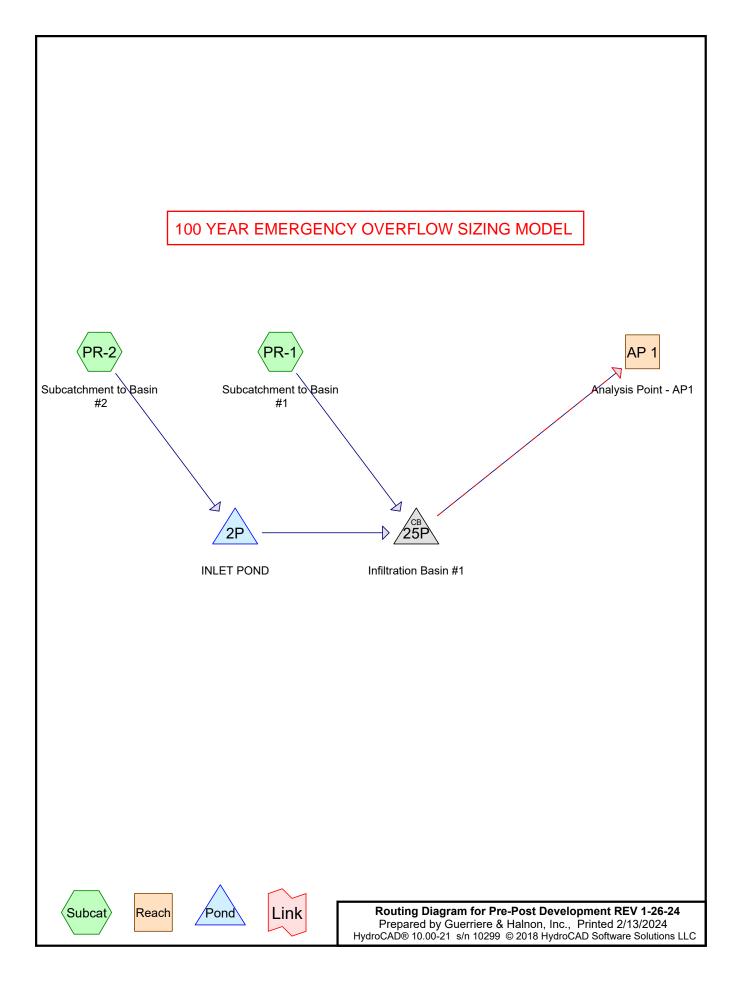
Plug-Flow detention time= 290.8 min calculated for 0.019 af (60% of inflow) Center-of-Mass det. time= 139.2 min (1,119.2 - 980.0)

| Volume | Inv | ert Avail.Sto | orage Storage | e Description | |
|---|----------------|---|--|--|--|
| #1 | 306. | 00' 1,3 | 65 cf Custon | n Stage Data (P | rismatic)Listed below (Recalc) |
| Elevatio (fee 306.0 307.0 308.0 | 51 50 50 | Surf.Area (sq-ft) 0 700 1,330 | Inc.Store (cubic-feet) 0 350 1,015 | Cum.Store (cubic-feet) 0 350 1,365 | |
| Device | Routing | Invert | Outlet Device | es | |
| #1 | Primary | 307.25' | Head (feet) (2.50 3.00 3. | 0.20 0.40 0.60 .50 h) 2.54 2.61 2. | oad-Crested Rectangular Weir 0.80 1.00 1.20 1.40 1.60 1.80 2.00 61 2.60 2.66 2.70 2.77 2.89 2.88 |

Primary OutFlow Max=0.04 cfs @ 14.62 hrs HW=307.26' TW=0.00' (Dynamic Tailwater) **1=Broad-Crested Rectangular Weir**(Weir Controls 0.04 cfs @ 0.29 fps)

Pond 24P: Roadside Swale - Frozen Conditions





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|---|--|
| Runoff by SCS TR | 72.00 hrs, dt=0.05 hrs, 1441 points -20 method, UH=SCS, Weighted-CN method - Pond routing by Dyn-Stor-Ind method |
| SubcatchmentPR-1: Subcatchmentto | Runoff Area=141,517 sf 55.11% Impervious Runoff Depth=5.35" Tc=6.0 min CN=72 Runoff=21.07 cfs 1.448 af |
| SubcatchmentPR-2: Subcatchmentto Flow | Runoff Area=670,872 sf 0.00% Impervious Runoff Depth=2.83" Length=1,673' Tc=37.2 min CN=51 Runoff=23.64 cfs 3.632 af |
| Reach AP 1: Analysis Point - AP1 | Inflow=29.39 cfs 5.050 af Outflow=29.39 cfs 5.050 af |
| Pond 2P: INLET POND Discarded=0.70 cfs 0 | Peak Elev=316.66' Storage=3,480 cf Inflow=23.64 cfs 3.632 af 0.041 af Primary=25.79 cfs 3.591 af Outflow=26.49 cfs 3.632 af |
| Pond 25P: Infiltration Basin #1 | Peak Elev=310.41' Inflow=29.22 cfs 5.039 af Outflow=29.22 cfs 5.039 af |
| Total Bunoff Aroa - 19 650 | ac Bunoff Volume = 5.081 of Average Bunoff Depth = 3.27 |

Total Runoff Area = 18.650 acRunoff Volume = 5.081 afAverage Runoff Depth = 3.27"90.40% Pervious = 16.859 ac9.60% Impervious = 1.790 ac

NRCC 24-hr C 100-Year Rainfall=8.74" Pre-Post Development REV 1-26-24 Prepared by Guerriere & Halnon, Inc. HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD Software Solutions LLC

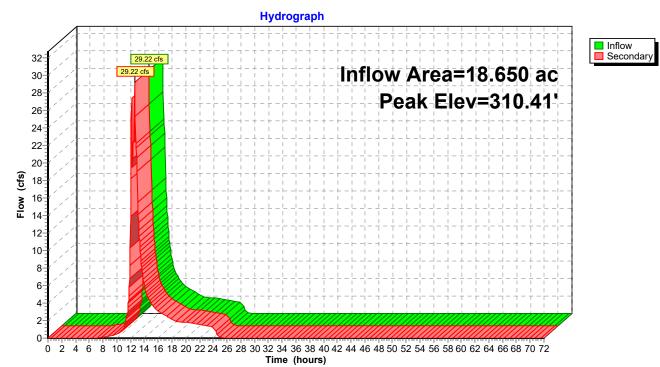
Summary for Pond 25P: Infiltration Basin #1

18.650 ac, 9.60% Impervious, Inflow Depth = 3.24" for 100-Year event Inflow Area = Inflow 29.22 cfs @ 12.60 hrs, Volume= = 5.039 af 29.22 cfs @ 12.60 hrs, Volume= 5.039 af, Atten= 0%, Lag= 0.0 min Outflow = Secondary = 29.22 cfs @ 12.60 hrs, Volume= 5.039 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 310.41'@ 12.60 hrs Flood Elev= 310.50'

| Device | Routing | Invert | Outlet Devices |
|--------|-----------|---------|--|
| #1 | Secondary | 309.90' | 30.0' long x 10.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64 |

Secondary OutFlow Max=28.96 cfs @ 12.60 hrs HW=310.41' TW=0.00' (Dynamic Tailwater) =Broad-Crested Rectangular Weir (Weir Controls 28.96 cfs @ 1.89 fps)



Pond 25P: Infiltration Basin #1

Printed 2/13/2024

100 YEAR WEIR BYPASS MODEL

<u>Stage-Area-Storage Calculations</u> Appendix 5

NRCC 24-hr C 100-Year Rainfall=8.74" Printed 2/13/2024

Pre-Post Development REV 1-26-24NRCC 24Prepared by Guerriere & Halnon, Inc.HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD Software Solutions LLC

Stage-Area-Storage for Pond 2P: INLET POND

| Elevation (feet) | Surface (sq-ft) | Storage (cubic-feet) |
|---------------------|--------------------|-------------------------|
| 312.00 | 1,182 | 0 |
| 312.05 | 1,207 | 60 |
| 312.10 | 1,233 | 121 |
| 312.15 | 1,258 | 183 |
| 312.20 | 1,284 | 247 |
| 312.25 | 1,309 | 311 |
| 312.30 | 1,334 | 377 |
| 312.35 | 1,360 | 445 |
| 312.40 | 1,385 | 513 |
| 312.45 | 1,411 | 583 |
| 312.50 312.55 | 1,436 1,461 | 655 727 |
| 312.60 | 1,487 | 801 |
| 312.65 | 1,512 | 876 |
| 312.70 | 1,538 | 952 |
| 312.75 | 1,563 | 1,029 |
| 312.80 | 1,588 | 1,108 |
| 312.85 | 1,614 | 1,188 |
| 312.90 | 1,639 | 1,270 |
| 312.95 | 1,665 | 1,352 |
| 313.00 313.05 | 1,690 | 1,436 1,521 |
| 313.10 | 1,725 1,761 | 1,609 |
| 313.15 | 1,796 | 1,697 |
| 313.20 | 1,832 | 1,788 |
| 313.25 | 1,867 | 1,881 |
| 313.30 | 1,902 | 1,975 |
| 313.35 | 1,938 | 2,071 |
| 313.40 | 1,973 | 2,169 |
| 313.45 | 2,009 | 2,268 |
| 313.50 | 2,044 | 2,370 |
| 313.55 313.60 | 2,079 2,115 | 2,473 2,577 |
| 313.65 | 2,113 | 2,684 |
| 313.70 | 2,186 | 2,792 |
| 313.75 | 2,221 | 2,903 |
| 313.80 | 2,256 | 3,015 |
| 313.85 | 2,292 | 3,128 |
| 313.90 | 2,327 | 3,244 |
| 313.95 | 2,363 | 3,361 |
| 314.00 | 2,398 | 3,480 |

Pre-Post Development REV 1-26-24NRCC 24Prepared by Guerriere & Halnon, Inc.HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD Software Solutions LLC

Stage-Area-Storage for Pond 1P: Infiltration Basin #1

| ElevationSurfaceHorizontalStorage(feet)(sq-ft)(cubic-feet)305.5010,45110,4510305.5610,56610,566631305.6210,68010,6801,268305.6810,79510,7951,912305.7410,91010,9102,563305.8011,02511,0253,221305.8611,13911,1393,886305.9211,2544,558305.9211,2544,558305.9311,36911,3695.9411,6056,615306.1011,60511,605306.1611,72411,7247,315306.2211,962306.2411,9628,736306.3412,08012,0809,457306.4012,19912,19912,19910,186306.6412,67512,675306.7612,91212,437306.7612,91214,706306.8213,03113,031306.7612,91214,706307.0013,38813,388307.1213,625307.2413,66313,663307.4814,33844,33814,33824,516307.4414,576307.6014,576307.6114,932307.7214,813307.7414,33844,33844,338307.7514,932307.7614,932307 | | | | - |
|--|--------|--------|--------|--------|
| 305.50 $10,451$ $10,451$ 0 305.56 $10,566$ $10,566$ 631 305.62 $10,680$ $10,680$ $1,268$ 305.68 $10,795$ $10,795$ $1,912$ 305.74 $10,910$ $10,910$ $2,563$ 305.86 $11,025$ $11,025$ $3,221$ 305.86 $11,399$ $11,399$ $3,886$ 305.92 $11,254$ $11,254$ $4,558$ 305.98 $11,369$ $11,369$ $5,237$ 306.04 $11,486$ $11,486$ $5,922$ 306.10 $11,605$ $11,605$ $6,615$ 306.16 $11,724$ $11,724$ $7,315$ 306.22 $11,962$ $8,736$ 306.34 $12,080$ $12,080$ $9,457$ 306.40 $12,199$ $12,199$ $10,186$ 306.52 $12,437$ $12,437$ $11,664$ 306.55 $12,556$ $12,556$ $12,414$ 306.64 $12,675$ $12,793$ $13,935$ 306.76 $12,912$ $12,912$ $14,706$ 306.84 $13,269$ $13,269$ $17,062$ 307.06 $13,506$ $13,506$ $18,669$ 307.12 $13,625$ $13,625$ $19,483$ 307.14 $13,744$ $13,744$ $20,304$ 307.44 $14,576$ $14,576$ $26,251$ 307.60 $14,576$ $14,576$ $26,251$ 307.60 $14,576$ $14,576$ $26,251$ 307.66 $14,695$ $27,129$ 307 | | | | |
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| 305.68 $10,795$ $10,795$ $1,912$ 305.74 $10,910$ $10,910$ $2,563$ 305.86 $11,025$ $11,025$ $3,221$ 305.86 $11,369$ $11,139$ $3,886$ 305.92 $11,254$ $11,254$ $4,558$ 305.98 $11,369$ $11,369$ $5,237$ 306.04 $11,486$ $11,486$ $5,922$ 306.10 $11,605$ $11,605$ $6,615$ 306.16 $11,724$ $11,724$ $7,315$ 306.22 $11,843$ $11,843$ $8,022$ 306.28 $11,962$ $11,962$ $8,736$ 306.34 $12,080$ $12,080$ $9,457$ 306.40 $12,199$ $12,199$ $10,186$ 306.52 $12,437$ $12,437$ $11,664$ 306.56 $12,556$ $12,556$ $12,414$ 306.56 $12,556$ $12,556$ $12,414$ 306.70 $12,793$ $12,793$ $13,935$ 306.76 $12,912$ $12,912$ $14,706$ 306.82 $13,031$ $13,031$ $15,484$ 306.84 $13,506$ $13,506$ $18,669$ 307.12 $13,625$ $13,625$ $19,483$ 307.14 $13,744$ $13,744$ $20,304$ 307.24 $13,883$ $14,338$ $24,516$ 307.42 $14,457$ $14,457$ $25,380$ 307.42 $14,932$ $14,932$ $28,906$ 307.76 $14,576$ $14,576$ $26,251$ 307.60 $15,787$ $15,7$ | | | | |
| 305.74 10.910 2.563 305.80 11.025 11.025 3.221 305.86 11.139 11.139 3.886 305.92 11.254 11.254 4.558 305.92 11.254 11.254 4.558 305.98 11.369 5.237 306.04 11.486 11.486 5.922 306.10 11.605 11.605 6.615 306.16 11.724 11.724 7.315 306.22 11.843 11.843 8.022 306.34 12.080 2.080 9.457 306.40 12.199 12.199 10.186 306.46 12.318 12.318 10.921 306.52 12.2437 12.437 11.664 306.52 12.256 12.556 12.414 306.64 12.675 12.675 13.171 306.70 12.793 12.793 13.935 306.76 12.912 12.912 14.706 306.82 13.031 13.031 15.484 306.84 13.269 13.269 17.062 307.00 13.388 13.388 17.862 307.18 13.744 13.744 20.304 307.24 13.863 13.863 21.132 307.48 14.338 14.338 24.516 307.72 14.813 14.813 28.014 307.74 14.992 14.995 27.129 307.754 14.992 14.932 28.906 <t< td=""><td></td><td></td><td></td><td></td></t<> | | | | |
| 305.80 $11,025$ $11,025$ $3,221$ 305.86 $11,139$ $11,139$ $3,886$ 305.92 $11,254$ $11,254$ $4,558$ 305.98 $11,369$ $11,369$ $5,237$ 306.04 $11,486$ $11,486$ $5,922$ 306.10 $11,605$ $11,605$ $6,615$ 306.16 $11,724$ $11,724$ $7,315$ 306.22 $11,843$ $11,843$ $8,022$ 306.28 $11,962$ $11,962$ $8,736$ 306.40 $12,199$ $12,199$ $10,186$ 306.40 $12,199$ $12,199$ $10,186$ 306.46 $12,318$ $12,556$ $12,556$ $12,556$ $12,556$ $12,414$ 306.670 $12,793$ $12,793$ $13,935$ 306.76 $12,912$ $12,912$ $14,706$ 306.82 $13,031$ $15,484$ 306.88 $13,150$ $13,150$ $16,270$ 306.94 $13,269$ $13,269$ $17,062$ 307.00 $13,388$ $13,863$ $21,132$ 307.12 $13,625$ $13,625$ $19,483$ 307.14 $13,744$ $3,744$ $20,304$ 307.24 $13,863$ $13,863$ $21,132$ 307.30 $13,982$ $13,982$ $21,967$ 307.42 $14,457$ $14,457$ $25,380$ 307.44 $14,576$ $14,576$ $26,251$ 307.66 $14,695$ $14,695$ $27,129$ 307.76 $14,576$ $14,576$ $26,251$ < | | | | |
| 305.86 $11,139$ $11,139$ $3,886$ 305.92 $11,254$ $11,254$ $4,558$ 305.98 $11,369$ $11,369$ $5,237$ 306.04 $11,486$ $11,486$ $5,922$ 306.10 $11,605$ $11,605$ $6,615$ 306.16 $11,724$ $11,724$ $7,315$ 306.22 $11,843$ $11,843$ $8,022$ 306.28 $11,962$ $11,962$ $8,736$ 306.34 $12,080$ $9,457$ 306.40 $12,199$ $12,199$ $10,186$ 306.46 $12,318$ $12,318$ $10,921$ 306.52 $12,437$ $12,437$ $11,664$ 306.58 $12,556$ $12,556$ $12,414$ 306.64 $12,675$ $12,675$ $13,171$ 306.76 $12,912$ $12,912$ $14,706$ 306.82 $13,031$ $13,031$ $15,484$ 306.82 $13,031$ $13,031$ $15,484$ 306.88 $13,150$ $13,150$ $16,270$ 307.00 $13,388$ $13,388$ $17,862$ 307.06 $13,506$ $13,606$ $18,669$ 307.12 $13,625$ $13,625$ $19,483$ 307.14 $13,744$ $3,744$ $20,304$ 307.24 $13,863$ $13,863$ $21,132$ 307.60 $14,576$ $14,576$ $26,251$ 307.66 $14,695$ $27,129$ 307.72 $14,813$ $14,813$ $28,014$ 307.74 $14,932$ $14,932$ $28,906$ <t< td=""><td></td><td></td><td></td><td></td></t<> | | | | |
| 305.92 $11,254$ $11,254$ $4,558$ 305.98 $11,369$ $11,369$ $5,237$ 306.04 $11,486$ $11,486$ $5,922$ 306.10 $11,605$ $11,605$ $6,615$ 306.16 $11,724$ $11,724$ $7,315$ 306.22 $11,843$ $11,843$ $8,022$ 306.28 $11,962$ $11,962$ $8,736$ 306.34 $12,080$ $12,080$ $9,457$ 306.40 $12,199$ $12,199$ $10,186$ 306.52 $12,437$ $12,437$ $11,664$ 306.52 $12,437$ $12,675$ $13,171$ 306.64 $12,575$ $12,675$ $13,171$ 306.64 $12,675$ $12,675$ $13,171$ 306.76 $12,912$ $12,912$ $14,706$ 306.82 $13,031$ $15,484$ 306.82 $13,031$ $15,484$ 306.84 $13,269$ $13,269$ $17,062$ 307.00 $13,388$ $13,388$ $17,862$ 307.18 $13,744$ $13,744$ $20,304$ 307.24 $13,863$ $13,863$ $21,132$ 307.30 $13,982$ $13,982$ $21,967$ 307.42 $14,457$ $14,457$ $25,380$ 307.66 $14,695$ $14,695$ $27,129$ 307.76 $14,695$ $14,695$ $27,129$ 307.76 $14,932$ $14,932$ $28,906$ 307.78 $14,932$ $14,932$ $28,906$ 307.74 $14,813$ $14,932$ $49,322$ | | | | |
| 305.98 $11,369$ $11,369$ $5,237$ 306.04 $11,486$ $11,486$ $5,922$ 306.10 $11,605$ $11,605$ $6,615$ 306.16 $11,724$ $11,724$ $7,315$ 306.22 $11,843$ $11,843$ $8,022$ 306.28 $11,962$ $11,962$ $8,736$ 306.40 $12,199$ $12,199$ $10,186$ 306.40 $12,199$ $12,199$ $10,186$ 306.46 $12,318$ $12,318$ $10,921$ 306.52 $12,437$ $12,437$ $11,664$ 306.58 $12,556$ $12,556$ $12,414$ 306.64 $12,675$ $12,675$ $13,171$ 306.76 $12,912$ $12,9912$ $14,706$ 306.82 $13,031$ $13,031$ $15,484$ 306.88 $13,150$ $13,150$ $16,270$ 306.94 $13,269$ $13,269$ $17,662$ 307.06 $13,506$ $13,506$ $18,669$ 307.12 $13,625$ $13,625$ $19,483$ 307.18 $13,744$ $13,744$ $20,304$ 307.24 $13,863$ $21,132$ 307.30 $13,982$ $13,982$ $21,967$ 307.66 $14,695$ $14,695$ $27,129$ 307.48 $14,338$ $14,338$ $24,516$ 307.48 $14,932$ $14,932$ $28,906$ 307.48 $14,932$ $14,932$ $28,906$ 307.66 $14,695$ $14,695$ $27,129$ 307.72 $14,813$ $14,813$ <t< td=""><td></td><td></td><td></td><td></td></t<> | | | | |
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| 306.10 $11,605$ $11,605$ $6,615$ 306.16 $11,724$ $11,724$ $7,315$ 306.22 $11,843$ $11,843$ $8,022$ 306.28 $11,962$ $11,962$ $8,736$ 306.34 $12,080$ $12,080$ $9,457$ 306.40 $12,199$ $12,199$ $10,186$ 306.46 $12,318$ $12,318$ $10,921$ 306.52 $12,437$ $12,437$ $11,664$ 306.58 $12,556$ $12,556$ $12,414$ 306.64 $12,675$ $13,171$ 306.70 $12,793$ $12,793$ $13,935$ 306.76 $12,912$ $12,912$ $14,706$ 306.82 $13,031$ $13,031$ $15,484$ 306.88 $13,150$ $13,150$ $16,270$ 306.94 $13,269$ $13,269$ $17,062$ 307.00 $13,388$ $13,388$ $17,862$ 307.12 $13,625$ $13,625$ $19,483$ 307.12 $13,625$ $13,625$ $19,483$ 307.14 $13,744$ $13,744$ $23,569$ 307.24 $13,863$ $13,863$ $21,132$ 307.30 $13,982$ $13,982$ $21,967$ 307.48 $14,338$ $14,338$ $24,516$ 307.54 $14,457$ $14,457$ $25,380$ 307.66 $14,695$ $27,129$ 307.72 $14,813$ $14,813$ $28,906$ 307.90 $15,170$ $15,170$ $30,713$ 307.66 $14,695$ $14,695$ $27,129$ </td <td></td> <td></td> <td></td> <td></td> | | | | |
| 306.16 $11,724$ $11,724$ $7,315$ 306.22 $11,843$ $11,843$ $8,022$ 306.28 $11,962$ $11,962$ $8,736$ 306.34 $12,080$ $12,080$ $9,457$ 306.40 $12,199$ $12,199$ $10,186$ 306.46 $12,318$ $12,318$ $10,921$ 306.52 $12,437$ $12,437$ $11,664$ 306.52 $12,437$ $12,437$ $11,664$ 306.64 $12,675$ $12,675$ $13,171$ 306.70 $12,793$ $12,793$ $13,935$ 306.76 $12,912$ $12,912$ $14,706$ 306.82 $13,031$ $13,031$ $15,484$ 306.88 $13,150$ $13,150$ $16,270$ 306.94 $13,269$ $13,269$ $17,062$ 307.06 $13,506$ $13,506$ $18,669$ 307.12 $13,625$ $13,625$ $19,483$ 307.18 $13,744$ $13,744$ $20,304$ 307.24 $13,863$ $13,863$ $21,132$ 307.30 $13,982$ $13,982$ $21,967$ 307.42 $14,219$ $14,219$ $23,659$ 307.44 $14,576$ $14,576$ $26,251$ 307.66 $14,695$ $14,695$ $27,129$ 307.72 $14,813$ $14,4813$ $28,016$ 307.78 $14,932$ $14,932$ $28,906$ 307.78 $14,932$ $14,932$ $28,906$ 307.84 $15,535$ $15,535$ $33,476$ 308.08 $15,535$ | | | | |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | | |
| 306.28 $11,962$ $11,962$ $8,736$ 306.34 $12,080$ $12,080$ $9,457$ 306.40 $12,199$ $12,199$ $10,186$ 306.46 $12,318$ $12,318$ $10,921$ 306.52 $12,437$ $12,437$ $11,664$ 306.58 $12,556$ $12,556$ $12,414$ 306.64 $12,675$ $12,675$ $13,171$ 306.70 $12,793$ $12,793$ $13,935$ 306.76 $12,912$ $12,912$ $14,706$ 306.82 $13,031$ $13,031$ $15,484$ 306.88 $13,150$ $13,150$ $16,270$ 306.94 $13,269$ $13,269$ $17,062$ 307.00 $13,388$ $13,388$ $17,862$ 307.00 $13,506$ $13,506$ $18,669$ 307.12 $13,625$ $13,625$ $19,483$ 307.18 $13,744$ $13,744$ $20,304$ 307.24 $13,863$ $13,863$ $21,132$ 307.36 $14,100$ $14,100$ $22,810$ 307.42 $14,219$ $14,219$ $23,659$ 307.48 $14,338$ $14,338$ $24,516$ 307.66 $14,695$ $27,129$ 307.72 $14,813$ $14,813$ $28,014$ 307.78 $14,932$ $14,932$ $28,906$ 307.84 $15,051$ $15,535$ $33,476$ 308.02 $15,787$ $15,787$ $35,355$ 308.08 $15,535$ $15,535$ $33,476$ 308.14 $15,661$ $14,612$ <td></td> <td></td> <td></td> <td></td> | | | | |
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| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | | |
| 306.52 $12,437$ $12,437$ $11,664$ 306.58 $12,556$ $12,556$ $12,414$ 306.64 $12,675$ $12,675$ $13,171$ 306.70 $12,793$ $12,793$ $13,935$ 306.76 $12,912$ $12,912$ $14,706$ 306.82 $13,031$ $13,031$ $15,484$ 306.88 $13,150$ $13,150$ $16,270$ 306.94 $13,269$ $13,269$ $17,062$ 307.00 $13,388$ $13,388$ $17,862$ 307.06 $13,506$ $13,506$ $18,669$ 307.12 $13,625$ $13,625$ $19,483$ 307.18 $13,744$ $13,744$ $20,304$ 307.24 $13,863$ $13,863$ $21,132$ 307.36 $14,100$ $14,100$ $22,810$ 307.42 $14,219$ $14,219$ $23,659$ 307.48 $14,338$ $14,338$ $24,516$ 307.54 $14,457$ $14,457$ $25,380$ 307.60 $14,576$ $14,576$ $26,251$ 307.60 $14,576$ $14,576$ $26,251$ 307.60 $14,576$ $14,695$ $27,129$ 307.72 $14,813$ $14,932$ $28,906$ 307.90 $15,170$ $15,170$ $30,713$ 307.96 $15,289$ $15,289$ $31,626$ 308.02 $15,410$ $15,410$ $32,547$ 308.08 $15,535$ $15,535$ $33,476$ 308.14 $15,661$ $15,661$ $34,412$ 308.26 $15,912$ </td <td></td> <td>12,318</td> <td></td> <td></td> | | 12,318 | | |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 306.52 | | | |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 306.58 | 12,556 | 12,556 | 12,414 |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 306.64 | 12,675 | 12,675 | 13,171 |
| 306.82 $13,031$ $13,031$ $15,484$ 306.88 $13,150$ $13,150$ $16,270$ 306.94 $13,269$ $13,269$ $17,062$ 307.00 $13,388$ $13,388$ $17,862$ 307.06 $13,506$ $13,506$ $18,669$ 307.12 $13,625$ $13,625$ $19,483$ 307.18 $13,744$ $13,744$ $20,304$ 307.24 $13,863$ $21,132$ 307.30 $13,982$ $13,982$ $21,967$ 307.36 $14,100$ $14,100$ $22,810$ 307.42 $14,219$ $14,219$ $23,659$ 307.48 $14,338$ $14,338$ $24,516$ 307.54 $14,457$ $14,457$ $25,380$ 307.60 $14,576$ $14,576$ $26,251$ 307.66 $14,695$ $14,695$ $27,129$ 307.72 $14,813$ $14,813$ $28,906$ 307.96 $15,289$ $15,051$ $29,806$ 307.96 $15,289$ $15,289$ $31,626$ 308.02 $15,410$ $15,410$ $32,547$ 308.08 $15,535$ $15,535$ $33,476$ 308.14 $15,661$ $34,412$ 308.20 $15,787$ $15,787$ $35,355$ 308.26 $15,912$ $15,912$ $36,306$ 308.32 $16,038$ $16,038$ $37,264$ 308.44 $16,289$ $16,289$ $39,204$ 308.50 $16,415$ $16,415$ $40,185$ | 306.70 | 12,793 | 12,793 | 13,935 |
| 306.88 $13,150$ $13,150$ $16,270$ 306.94 $13,269$ $13,269$ $17,062$ 307.00 $13,388$ $13,388$ $17,862$ 307.06 $13,506$ $13,506$ $18,669$ 307.12 $13,625$ $13,625$ $19,483$ 307.18 $13,744$ $13,744$ $20,304$ 307.24 $13,863$ $21,132$ 307.30 $13,982$ $13,982$ $21,967$ 307.36 $14,100$ $14,100$ $22,810$ 307.42 $14,219$ $14,219$ $23,659$ 307.48 $14,338$ $14,338$ $24,516$ 307.54 $14,457$ $14,457$ $25,380$ 307.60 $14,576$ $14,576$ $26,251$ 307.66 $14,695$ $14,695$ $27,129$ 307.72 $14,813$ $14,813$ $28,906$ 307.96 $15,289$ $15,051$ $29,806$ 307.90 $15,170$ $15,170$ $30,713$ 307.96 $15,289$ $15,289$ $31,626$ 308.02 $15,410$ $15,410$ $32,547$ 308.08 $15,535$ $15,535$ $33,476$ 308.20 $15,787$ $15,787$ $35,355$ 308.26 $15,912$ $15,912$ $36,306$ 308.32 $16,038$ $16,038$ $37,264$ 308.34 $16,289$ $16,289$ $39,204$ 308.50 $16,415$ $16,415$ $40,185$ | 306.76 | | | |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | | |
| 308.0215,41015,41032,547308.0815,53515,53533,476308.1415,66115,66134,412308.2015,78715,78735,355308.2615,91215,91236,306308.3216,03816,03837,264308.3816,16416,16438,230308.4416,28916,28939,204308.5016,41516,41540,185 | | | | |
| 308.0815,53515,53533,476308.1415,66115,66134,412308.2015,78715,78735,355308.2615,91215,91236,306308.3216,03816,03837,264308.3816,16416,16438,230308.4416,28916,28939,204308.5016,41516,41540,185 | | | | |
| 308.1415,66115,66134,412308.2015,78715,78735,355308.2615,91215,91236,306308.3216,03816,03837,264308.3816,16416,16438,230308.4416,28916,28939,204308.5016,41516,41540,185 | | | | |
| 308.2015,78715,78735,355308.2615,91215,91236,306308.3216,03816,03837,264308.3816,16416,16438,230308.4416,28916,28939,204308.5016,41516,41540,185 | | | | |
| 308.2615,91215,91236,306308.3216,03816,03837,264308.3816,16416,16438,230308.4416,28916,28939,204308.5016,41516,41540,185 | | | | |
| 308.3216,03816,03837,264308.3816,16416,16438,230308.4416,28916,28939,204308.5016,41516,41540,185 | | | | 36,306 |
| 308.3816,16416,16438,230308.4416,28916,28939,204308.5016,41516,41540,185 | | | | |
| 308.50 16,415 16,415 40,185 | 308.38 | 16,164 | 16,164 | |
| | 308.44 | | 16,289 | 39,204 |
| 308.56 16,540 16,540 41,174 | 308.50 | | | |
| | 308.56 | 16,540 | 16,540 | 41,174 |

Pre-Post Development REV 1-26-24NRCC 24Prepared by Guerriere & Halnon, Inc.HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD Software Solutions LLC

Stage-Area-Storage for Pond 1P: Infiltration Basin #1 (continued)

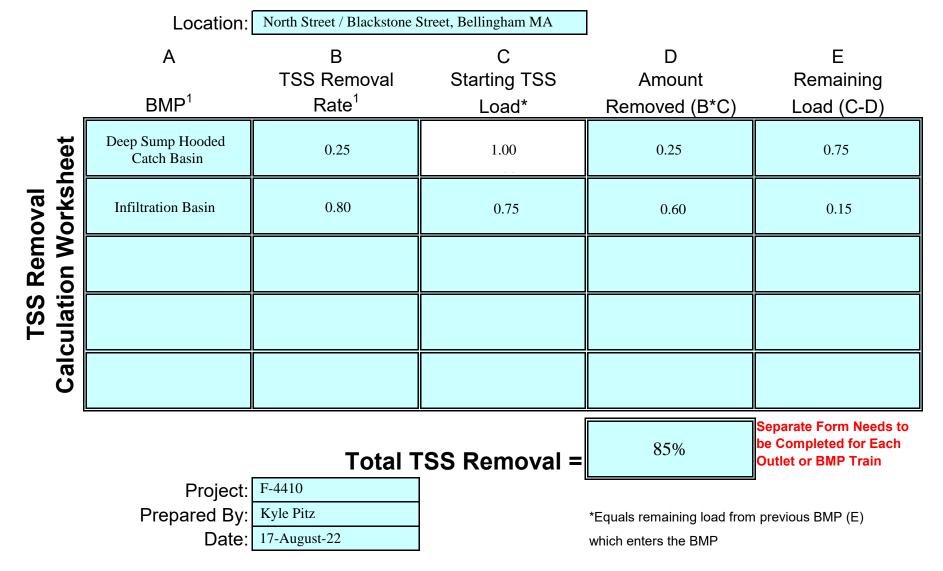
| Elevation | Surface | Horizontal | Storage |
|-----------|---------|------------|--------------|
| (feet) | (sq-ft) | (sq-ft) | (cubic-feet) |
| 308.62 | 16,666 | 16,666 | 42,170 |
| 308.68 | 16,792 | 16,792 | 43,174 |
| 308.74 | 16,917 | 16,917 | 44,185 |
| 308.80 | 17,043 | 17,043 | 45,204 |
| 308.86 | 17,168 | 17,168 | 46,230 |
| 308.92 | 17,294 | 17,294 | 47,264 |
| 308.98 | 17,420 | 17,420 | 48,305 |
| 309.04 | 17,545 | 17,545 | 49,354 |
| 309.10 | 17,671 | 17,671 | 50,411 |
| 309.16 | 17,796 | 17,796 | 51,475 |
| 309.22 | 17,922 | 17,922 | 52,546 |
| 309.28 | 18,048 | 18,048 | 53,626 |
| 309.34 | 18,173 | 18,173 | 54,712 |
| 309.40 | 18,299 | 18,299 | 55,806 |
| 309.46 | 18,425 | 18,425 | 56,908 |
| 309.52 | 18,550 | 18,550 | 58,017 |
| 309.58 | 18,676 | 18,676 | 59,134 |
| 309.64 | 18,801 | 18,801 | 60,258 |
| 309.70 | 18,927 | 18,927 | 61,390 |
| 309.76 | 19,053 | 19,053 | 62,530 |
| 309.82 | 19,178 | 19,178 | 63,677 |
| 309.88 | 19,304 | 19,304 | 64,831 |
| 309.94 | 19,429 | 19,429 | 65,993 |
| 310.00 | 19,555 | 19,555 | 67,163 |
| 310.06 | 19,685 | 19,685 | 68,340 |
| 310.12 | 19,815 | 19,815 | 69,525 |
| 310.18 | 19,945 | 19,945 | 70,717 |
| 310.24 | 20,074 | 20,074 | 71,918 |
| 310.30 | 20,204 | 20,204 | 73,126 |
| 310.36 | 20,334 | 20,334 | 74,343 |
| 310.42 | 20,464 | 20,464 | 75,566 |
| 310.48 | 20,594 | 20,594 | 76,798 |
| 310.54 | 20,637 | 20,637 | 78,036 |
| 310.60 | 20,637 | 20,637 | 79,274 |
| 310.66 | 20,637 | 20,637 | 80,512 |
| 310.72 | 20,637 | 20,637 | 81,751 |
| 310.78 | 20,637 | 20,637 | 82,989 |
| 310.84 | 20,637 | 20,637 | 84,227 |
| 310.90 | 20,637 | 20,637 | 85,465 |
| 310.96 | 20,637 | 20,637 | 86,704 |

<u>TSS Removal Worksheet</u> Appendix 6

INSTRUCTIONS:

1. Sheet is nonautomated. Print sheet and complete using hand calculations. Column A and B: See MassDEP Structural BMP Table

- 2. The calculations must be completed using the Column Headings specified in Chart and Not the Excel Column Headings
- 3. To complete Chart Column D, multiple Column B value within Row x Column C value within Row
- 4. To complete Chart Column E value, subtract Column D value within Row from Column C within Row
- 5. Total TSS Removal = Sum All Values in Column D



INSTRUCTIONS:

1. Sheet is nonautomated. Print sheet and complete using hand calculations. Column A and B: See MassDEP Structural BMP Table

- 2. The calculations must be completed using the Column Headings specified in Chart and Not the Excel Column Headings
- 3. To complete Chart Column D, multiple Column B value within Row x Column C value within Row

-

- 4. To complete Chart Column E value, subtract Column D value within Row from Column C within Row
- 5. Total TSS Removal = Sum All Values in Column D

| | Location: North Street / Blackstone Street, Bellingham MA | | | | |
|-----------------------|---|----------------------------------|-------------------------|--|--|
| | А | В | С | D | E |
| | BMP ¹ | TSS Removal Rate ¹ | Starting TSS Load* | Amount Removed (B*C) | Remaining Load (C-D) |
| neet | Deep Sump Hooded Catch Basin | 0.25 | 1.00 | 0.25 | 0.75 |
| moval Worksheet | Sediment Forebay | 0.25 | 0.75 | 0.19 | 0.56 |
| D | | | | | |
| TSS Re Calculation | | | | | |
| Calc | | | | | |
| Ľ | | | atment 'SS Removal = | 44% | Separate Form Needs to be Completed for Each Outlet or BMP Train |
| | Project: Prepared By: Date: | | | *Equals remaining load from which enters the BMP | previous BMP (E) |

Long Term Operation and Maintenance Plan Appendix 7 The following shall serve as the (O&M) Plan required by Standard 9, as well as the Long-Term Pollution Prevention Plan required by Standard 4.

A. <u>Names of Persons or Entity Responsible for Plan Compliance</u> Applicant: Raven Homes, Inc. 22 Buckhill Road Northborough, MA 01532 PH: 508-393-4511

B. <u>Stormwater Management System Owner</u> Owner: Raven Homes, Inc.

Raven Homes, Inc. 22 Buckhill Road Northborough, MA 01532 PH: 508-393-4511

- C. <u>Good housekeeping practices</u>
 - 1. Maintain site, landscaping and vegetation.
 - 2. Sweep and pick up litter on pavements and grounds.
 - 3. Deliveries shall be monitored by owners or representative to ensure that if any spillage occurs, it shall be contained and cleaned up immediately.
 - 4. Maintain pavement and curbing in good repair.
- D. Requirements for routine inspections and maintenance of stormwater BMPs
 - 1. Plans: The stormwater Operation and Maintenance Plan shall consist of all Plans, documents and all local state and federal approvals as required for the subject property.
 - 2. Record Keeping:
 - a. Maintain a log of all operation and maintenance activities for at least three years following construction, including inspections, repairs, replacement and disposal (for disposal, the log shall indicate the type of material and the disposal location).
 - b. Make this log available to MassDEP and the Conservation Commission upon request; and
 - c. Allow MassDEP and the Conservation Commission to inspect each BMP to determine whether the responsible party is implementing the Operation and Maintenance Plan.
 - 3. Descriptions and Designs: The Best Management Practices (BMP) incorporated into the design include the following.
 - a. Street Sweeping Stipulated within the Construction Period Pollution Prevention Plan, the Long-Term Pollution Prevention Plan, and the Operation and Maintenance Plan. As the amount of TSS removal is discretionary, no credit was taken within the calculations for this BMP.
 - b. Deep sump catch basins with hoods installed to promote TSS Removal of solids and control floatable pollutants. This BMP has a design rate of 25% TSS Removal.
 - c. Infiltration basin and sediment forebay provided to promote the required 80% TSS Removal. Refer to TSS Removal Worksheet in Standard 4 for treatment train.
 - d. Safety Fencing: Provide 6-FT high chain link fence with lockable gates around detention basin for public safety.
 - e. Spill Containment Kit to contain and clean-up spills that could occur on site.

- 4. BMP Maintenance: After construction it is the responsibility of the owner to perform maintenance. The cleaning of the components of the stormwater management system shall generally be as follows:
 - a. Roadway: The owner shall keep the roadway swept with a mechanical sweeper or hand swept semi-annually at a minimum.
 - b. Catch Basins: Shall be cleaned by excavating, pumping or vacuuming four times per year and at the end of foliage and snow removal seasons. The sediment shall be disposed of off-site by the Owner. Inspect quarterly, remove silt when ¹/₄ full.
 - c. Infiltration Basin: Preventative maintenance shall be performed at least twice per year. Inspection shall be performed after every major storm for the first three months and twice a year thereafter and when there are discharges through the high outlet orifice. Mowing of the buffer area, and bottom of basin; removal of trash and debris; removal of grass clippings and organic matter to be performed at least twice per year. Pretreatment devices shall be inspected every other month and a least twice a year and after every major storm event.
- 5. Access Provisions: All of the components of the storm water system shall be accessible by the Owner
- E. <u>Spill prevention and response plans</u>
 - 1. Inventory materials to be present on-site during construction.
 - 2. Train employees and subcontractors in prevention and clean up procedures.
 - 3. All materials stored on site will be stored in their appropriate containers under a roof.
 - 4. Follow manufacturers recommendation for disposal of used containers.
 - 5. Store only enough product on site to do the job.
 - 6. On site equipment, fueling and maintenance measures:
 - a. Inspect on-site vehicles and equipment daily for leaks.
 - b. Conduct all vehicle and equipment maintenance and refueling in one location, away from storm drains.
 - c. Perform major repairs and maintenance off site.
 - d. Use drip pans, drip cloths or absorbent pads when replacing spent fuels.
 - e. Collect spent fuels and remove from site.
 - 7. Clean up spills.
 - a. Never hose down "dirty" pavement or impermeable surfaces where fluids have spilled. Use dry clean up methods (sawdust, cat litter and/or rags and absorbent pads).
 - b. Sweep up dry materials immediately. Never wash them away or bury them.
 - c. Clean up spills on dirt areas by digging up and properly disposing of contaminated soil.
 - d. Report significant spills to the Fire Department, Conservation Commission and Board of Health.
- F. <u>Provisions for maintenance of lawns, gardens, and other landscaped areas</u> Use only organic fertilizer. Dispose of clippings outside of the 100-foot buffer zone to the adjacent wetland.
- G. <u>Requirements for storage and use of herbicides, and pesticides</u> The application of herbicides or pesticides will be done by professional certified contractor.
- H. <u>Provisions for operation and management of septic system</u> Site to be serviced by private on-site sewer.

I. <u>Requirements for handling of pet waste</u>

Pet waste should never be dumped or washed into the local storm drain system. Waste shall be picked up immediately and placed in bags and properly disposed of in the garbage to be collected and taken to a landfill.

J. <u>Provisions for washing of vehicles</u>

Washing of vehicles shall be done in an area as to eliminate wash water from being directly discharged to the local storm drain system. Vehicles should be washed in areas where wash water can be held prior to discharging to the sanitary sewer system or in areas where infiltration precludes runoff to storm drains. Avoid using detergents whenever possible.

- K. Provisions for solid waste management
 - 1. <u>Waste Management Plan</u>
 - a. Recycle materials whenever possible (paper, plaster cardboard, metal cans). Separate containers for material are recommended.
 - b. Do not bury waste and debris on site.
 - c. Certified haulers will be hired to remove the dumpster container waste as needed. Recycling products will also be removed off site weekly.
- L. <u>Snow disposal and plowing plans relative to Wetland Resource Areas</u> Snow storage is adequate around the site for large storm events. Storage of snow shall not be placed directly near areas adjacent to the proposed infiltration basin.
- M. <u>Winter Road Salt and/or Sand Use and Storage restrictions</u> No sand, salt, or chemicals for de-icing will be stored outside.
- N. Street sweeping schedules

Sweeping, the act of cleaning pavement can be done by mechanical sweepers, vacuum sweeper or hand sweeper. The quantity of sand is a direct correlation with the treatment of ice and snow and the types of chemicals and spreaders that are being used on site to manage snow. If a liquid de-icer such as calcium chloride is used as a pretreatment to new events the amount of sand is minimized. Sweeping for this site should be done semi-annually at a minimum. Collecting the particulate before it enters the catch basins is cheaper and more environmentally friendly than in a catch basin mixing with oils and greases in the surface water runoff in catch basins.

- O. <u>Provisions for prevention of illicit discharges to the stormwater management system</u> The discharge into the stormwater system is not being violated, see attachment for illicit discharges compliance.
- P. <u>Training the staff or personnel involved with implementing Long-Term Pollution Prevention</u> <u>Plan</u>

The owner shall develop policies and procedures for containing the illicit spilling of oils, soda, beer, paper and litter. These wastes provide a degrading of the water quality. The placement of signs and trash barrels with lids around the site would contribute to a clean water quality site condition.

Q. List of Emergency contacts for implementing Long-Term Pollution Prevention Plan:

Raven Homes, Inc. 22 Buckhill Road Northborough, MA 01532 PH: 508-393-4511

This shall be the contact until such time as the project is sold.

R. Estimated BMP Maintenance Costs

The following prices are estimates of the costs associated with maintenance of the proposed site BMPs. Costs provided are only estimates and may not reflect actual costs to perform the work. Actual costs may vary depending on company/personnel performing the work. Actual costs may increase over time.

<u>BMP</u>

Pavement sweeping Catch basin cleaning Infiltration Basin Spill Containment Kit Estimated Maintenance Cost \$ 400 per year \$ 200 per catch basin per cleaning \$ 200 per cleaning \$ 750 purchase price **Construction Period Pollution Prevention Plan** Appendix 8 Construction Period Pollution Prevention Plan and Erosion and Sedimentation Control. EPA NPDES – Storm Water Pollution Prevention Plan (SWPPP)

A. <u>Names of Persons or Entity Responsible for Plan Compliance</u> Applicant: Raven Homes, Inc. 22 Buckhill Road Northborough, MA 01532

PH: 508-393-4511

B. <u>Construction Period Pollution Prevention Measures</u>

- 1. Inventory materials to be present on-site during construction.
- 2. Train employees and subcontractors in prevention and clean up procedures.
- 3. All materials stored on site will be stored in their appropriate containers and if possible, under a roof or covered.
- 4. Follow manufacturer's recommendation for disposal of used containers.
- 5. Store only enough product on site to do the job.
- 6. On site equipment, fueling and maintenance measures:
 - a. Inspect on-site vehicles and equipment daily for leaks.
 - b. Conduct all vehicle and equipment maintenance and refueling in front of building, away from storm drains.
 - c. Perform major repairs and maintenance off site.
 - d. Use drip pans, drip cloths or absorbent pads when replacing spent fuels.
 - e. Collect spent fuels and remove from site, per Local and State regulations.
 - f. Maintain a clean construction entrance where truck traffic is frequent to reduce soil compaction constant sweeping is required and limit tracking of sediment into streets, sweeping street when silt is observed on street.
- 7. Stockpile materials and maintain Erosion Control around the materials where it can easily be accessed. Maintain easy access to clean up materials to include brooms, mops, rags gloves, goggles, sand, sawdust, plastic and metal trash containers.
- 8. Clean up spills.
 - a. Never hose down "dirty" pavement or impermeable surfaces where fluids have spilled. Use dry clean up methods (sawdust, cat litter and/or rags/absorbent pads).
 - b. Sweep up dry materials immediately. Never wash them away or bury them.
 - c. Clean up spills on dirt areas by digging up and properly disposing of contaminated soil in a certified container and notify a certified hauler for removal.
 - d. Report significant spills to the Fire Department.
- 9. It is the responsibility of the site superintendent or employees designated by the Applicant to inspect erosion control and repair as needed, also to inspect all on site vehicles for leaks and check all containers on site that may contain hazardous materials daily.
- C. <u>Erosion and Sedimentation Control Plan.</u> Erosion Control Plan prepared by Guerriere & Halnon, Inc. Dated 12/30/22 revised 02/13/2024
- D. <u>Site Development Plans</u>. See Site Plan prepared by Guerriere & Halnon, Inc. Dated 12/30/22 and revised through 02/13/2024
- E. <u>Construction Plans</u> See Site Plan prepared by Guerriere & Halnon, Inc. Dated 12/30/22 and revised through 02/13/2024

- 1. Construction
 - a. Record Order of Conditions The site superintendent shall be aware of all the Conditions contained within the Order including inspection schedules.
 - b. Install DEP File # Sign.
 - c. Prior to any work on the site including tree/brush clearing, the approved limit of clearing as well as the location of the proposed erosion control devices (such as silt fence/mulch sock, etc.) must be staked on the ground under the direction of a Massachusetts registered Professional Land Surveyor.
 - d. Install silt fence/mulch sock at locations shown on Erosion Control Plan
 - e. Strip off top and subsoil. Stockpile material to be reused away from the wetland, remove excess material from the site. Install and maintain erosion control barrier around stockpile.
 - f. Rough grade site, maintaining a temporary low area/sediment trap away from the wetland.
 - g. Construct drainage outfalls and stilling basin. Stabilize side slopes with loam, seed and mulch.
 - h. Install underground utilities; protect all open drainage structures with erosion/siltation control devices.
 - i. Install binder course of bituminous asphalt.
 - j. Install wearing course of asphalt, and striping (where required).
 - k. Maintain all erosion control devices until site is stabilized and a Certificate of Compliance is issued by the Conservation Commission.
 - 1. The Contractor shall be responsible to schedule any required inspections of his/her work.
- F. Construction Waste Management Plan
 - a. Dumpster for trash and bulk waste collection shall be provided separately for construction.
 - b. Recycle materials whenever possible (paper, plaster cardboard, metal cans). Separate containers for material are recommended.
 - c. Segregate and provide containers for disposal options for waste.
 - d. Do not bury waste and debris on site.
 - e. Certified haulers will be hired to remove the dumpster container waste as needed. Recycling products will also be removed off site weekly.
 - f. The sewer system is only for disposal of human waste, and substances permitted for disposal in the site sewer permit with the Town B.O.H.

G. Operation and Maintenance of Erosion and Sedimentation Controls

- The operation and maintenance of sedimentation control shall be the responsibility of the contractor. The inspection and maintenance of the stormwater component shall be performed as noted below. The contractor shall have erosion control in place at all times. The contractor, based on future weather reports, shall prepare and inspect all erosion control devices; cleaning, repairing and upgrading is a priority so that the devices perform as per design. Inspect the site during rain events. Do not stay away from the site. At a minimum there should be inspection to assure the devices are not clogged or plugged, or that devices have not been destroyed or damaged during the rain event. After a storm event inspection is required to clean and repair any damage components. Immediate repair is required.
- H. Inspection and Maintenance Schedules
 - 1. Inspection must be conducted at least once every 7 days and within 24 hours of the end of a storm event 0.5 inches or greater.

- 2. Inspection frequency can be reduced to once a month if:
 - a. The site is temporarily stabilized.
 - b. Runoff is unlikely due to winter conditions when site is covered with snow or ice.
- 3. Inspections must be conducted by qualified personnel, "qualified personnel" means a person knowledgeable in the principles and practice of erosion and sediment controls and who possess the skills to assess the conditions and take measures to maintain and ensure proper operation, also to conclude if the erosion control methods selected are effective.
- 4. For each inspection, the inspection report must include: (See attached inspection and maintenance log)
 - a. The inspection date.
 - b. Names, titles of personnel making the inspection.
 - c. Weather information for the period since the last inspection.
 - d. Weather information at the time of the inspection.
 - e. Locations of discharges of sediment from the site, if any.
 - f. Locations of BMP's that need to be maintained.
 - g. Locations where additional BMP's may be required.
 - h. Corrective action required or any changes to the SWPPP that may be necessary.
- 5. The owner, or their representative, such as the contractor, shall inspect the following inplace work.

| Inspection Schedule: | |
|--------------------------------------|--------|
| Erosion Control | Weekly |
| Catch Basins | Weekly |
| Temporary Sedimentation Traps/Basins | Weekly |
| Street Sweeping | Weekly |

Please Note: Special inspections shall also be made after a significant rainfall event.

| Maintenance Schedule | |
|---------------------------------|----------------------------------|
| Erosion Control Devices Failure | Immediately |
| Catch Basins | Sump 1/4 full of sediment |
| Street Sweeping | 14 days minimum and prior to any |
| | significant rain event. |

Please Note: Special maintenance shall also be made after a significant rainfall event.

I. <u>Inspection and Maintenance Log Form</u>. (Log Form Follows)

<u>Illicit Discharge Statement</u> Appendix 9

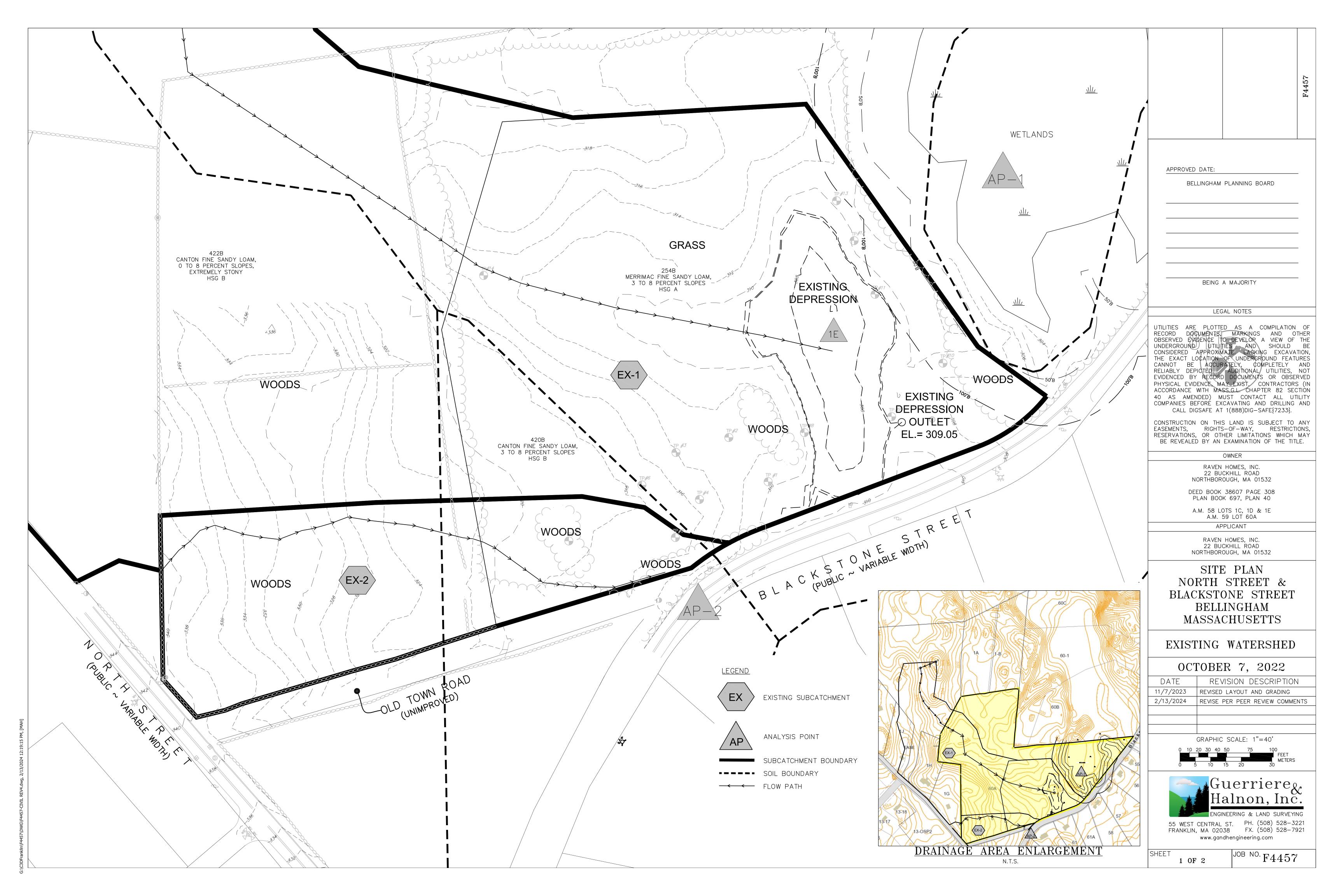
Illicit Discharge Compliance Statement

It is the intent of the Applicant, Raven Homes, Inc, 22 Buckhill Road, Northborough, MA 01532, (508)393-4511, to control illicit disposal into the storm drainage system. There will be no connection to the storm water system to inadvertently direct other types of liquids, chemicals or solids into the storm drainage system. The Applicant will also promote a clean Green Environment by mitigating spills onto pavements, oils, chemicals, pet waste, debris and litter.

Respectfully Acknowledged,

1000 Rayen Homes, Inc.

Drainage Area Plans Appendix 10





\C3DFranklin\F4457\DWG\F4457-CIVIL REV4.dwg, 2/13/2024 12:19:18 PM, [

SUPPLEMENTAL ATTACHMENTS Appendix 11

Pre-Post Development for 5 building layoutNRCC 2Prepared by {enter your company name here}HydroCAD® 10.00-21s/n 10299 © 2018 HydroCAD Software Solutions LLC

Hydrograph for Pond 1P: Infiltration Basin #1

| Time | Inflow | Storage | Elevation | Outflow | Discarded | Primary | Secondary |
|---------|--------|--------------|-----------|---------|-----------|---------|-----------|
| (hours) | (cfs) | (cubic-feet) | (feet) | (cfs) | (cfs) | (cfs) | (cfs) |
| 0.00 | 0.00 | 0 | 305.50 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2.50 | 0.00 | 0 | 305.50 | 0.00 | 0.00 | 0.00 | 0.00 |
| 5.00 | 0.00 | 0 | 305.50 | 0.00 | 0.00 | 0.00 | 0.00 |
| 7.50 | 0.07 | 4 | 305.50 | 0.07 | 0.07 | 0.00 | 0.00 |
| 10.00 | 0.44 | 23 | 305.50 | 0.44 | 0.44 | 0.00 | 0.00 |
| 12.50 | 21.99 | 33,606 | 308.09 | 8.18 | 5.17 | 3.01 | 0.00 |
| 15.00 | 4.01 | 27,902 | 307.71 | 6.60 | 4.67 | 1.93 | 0.00 |
| 17.50 | 2.34 | 15,133 | 306.79 | 3.50 | 3.50 | 0.00 | 0.00 |
| 20.00 | 1.71 | 5,853 | 306.03 | 2.59 | 2.59 | 0.00 | 0.00 |
| 22.50 | 1.43 | 104 | 305.51 | 1.99 | 1.99 | 0.00 | 0.00 |
| 25.00 | 0.06 | 7 | 305.50 | 0.13 | 0.13 | 0.00 | 0.00 |
| 27.50 | 0.00 | 0 | 305.50 | 0.00 | 0.00 | 0.00 | 0.00 |
| 30.00 | 0.00 | 0 | 305.50 | 0.00 | 0.00 | 0.00 | 0.00 |
| 32.50 | 0.00 | 0 | 305.50 | 0.00 | 0.00 | 0.00 | 0.00 |
| 35.00 | 0.00 | 0 | 305.50 | 0.00 | 0.00 | 0.00 | 0.00 |
| 37.50 | 0.00 | 0 | 305.50 | 0.00 | 0.00 | 0.00 | 0.00 |
| 40.00 | 0.00 | 0 | 305.50 | 0.00 | 0.00 | 0.00 | 0.00 |
| 42.50 | 0.00 | 0 | 305.50 | 0.00 | 0.00 | 0.00 | 0.00 |
| 45.00 | 0.00 | 0 | 305.50 | 0.00 | 0.00 | 0.00 | 0.00 |
| 47.50 | 0.00 | 0 | 305.50 | 0.00 | 0.00 | 0.00 | 0.00 |
| 50.00 | 0.00 | 0 | 305.50 | 0.00 | 0.00 | 0.00 | 0.00 |
| 52.50 | 0.00 | 0 | 305.50 | 0.00 | 0.00 | 0.00 | 0.00 |
| 55.00 | 0.00 | 0 | 305.50 | 0.00 | 0.00 | 0.00 | 0.00 |
| 57.50 | 0.00 | 0 | 305.50 | 0.00 | 0.00 | 0.00 | 0.00 |
| 60.00 | 0.00 | 0 | 305.50 | 0.00 | 0.00 | 0.00 | 0.00 |
| 62.50 | 0.00 | 0 | 305.50 | 0.00 | 0.00 | 0.00 | 0.00 |
| 65.00 | 0.00 | 0 | 305.50 | 0.00 | 0.00 | 0.00 | 0.00 |
| 67.50 | 0.00 | 0 | 305.50 | 0.00 | 0.00 | 0.00 | 0.00 |
| 70.00 | 0.00 | 0 | 305.50 | 0.00 | 0.00 | 0.00 | 0.00 |

Land Use Coefficients "C"

| Pave | 0.90 |
|---------|------|
| Gravel | 0.80 |
| Wetland | 0.72 |
| Grass | 0.30 |
| Woods | 0.25 |
| Roof | 0.90 |

| Drainage | Land Use Area | | | | | | | Weighted |
|----------|---------------|---------|---------|----------|---------|---------|---------|----------|
| Area | Impervious | Gravel | Wetland | Pervious | Woods | Roof | Total | "C" |
| | (acres) | (acres) | (acres) | (acres) | (acres) | (acres) | (acres) | |
| DA-1A | 0.346 | | | 0.198 | | 0.186 | 0.731 | 0.74 |
| DA-1B | 0.357 | | | 0.108 | | 0.130 | 0.595 | 0.79 |
| DA-3A | 0.094 | | | 0.093 | | 0.000 | 0.187 | 0.60 |
| DA-3B | 0.076 | | | 0.041 | | 0.000 | 0.118 | 0.69 |
| DA-5 | | | | | 14.336 | | 15.372 | 0.23 |
| DA-6 | | | | 0.351 | 0.000 | | 0.351 | 0.30 |
| SUBTOTAL | 0.874 | 0.000 | 0.000 | 0.791 | 14.336 | 0.316 | 17.353 | |
| OVERALL | | | | | | | | |
| TOTALS | 0.874 | | | 0.791 | 14.336 | 0.316 | 16.317 | |

| Guerriere & | Halnon, Inc. | | | | | | | | | | Project | | | Ν | orth Stre | eet & Blacks | tone Street, | Bellingham M | ΛA | | | | | |
|-------------|--------------|--------------------------------------|--------|-------------------|------------------------------|----------------------|------------|---------|------------------------|--------------------------|------------------------------|---------------------------|--------------------|------------------|-----------|--------------|--------------|--------------|-----------|-----|-----|------------|---------|--|
| 55 West Ce | ntral Steet | | | | | | | | | | Job No. | | | 4457 | | | | | | | | | | |
| Franklin, M | A 01757-023 | 4 | | | | | | | | | | | | | - | | | | | | | | | |
| | | DESIGN COMPUTATIONS FOR STORM DRAINS | | | | | | | | | | I | Prepared By | KKP | Date | 10/ | 12/2022 | Revised | 11-7-23 | MAH | | | | |
| | | DESIGN COMPUTATIONS FOR STORM DRAINS | | | | | | | | | | | Checked By | | Date | | | Revised | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | Invert E | levation | Rim | Elev | | | | | |
| Drainage | | | | f ntrat () | ty II | al Flow (Q) | ter | | ness cient | II. | ty. | L7 | of *() | .5 | all | | | | | | | | | |
| Area | | | Sum of | ne of ncent | Rainfall Intensity (I) | | e | Slope | tough Doeffic n) | Design Flow Ft (Q) | Velocity Flow Full (V) | Actual Velocity (V) | Length Pipe (L) | l'ime ii dipe | otal F. | | | | | | | Destinati | on | |
| | Upper | Lower | CA's | Tin Coi ion | Rai Inte (I) | Actu Peak Rate | Pip Dia | Slo | E C & | De: Flo (Q) | Vel Flo (V) | Act Vel (V) | Ler Pip | Tin pip | Tot | Elev. | Elev. | Elev. | Elev. | | | | | |
| | Structure | Structure | (sf) | (min) | (in/hr) | (cfs) | (in) | (ft/ft) | | (cfs) | (fps) | (fps) | (ft) | (min) | (ft) | Upper End | Lower End | Upper End | Lower End | | | | | |
| DA-1 | CB-1A | DMH-1 | 0.54 | 6.00 | 5.80 | 3.12 | 12 | 0.013 | 0.011 | 4.89 | 6.22 | 3.98 | 24.5 | 0.07 | 0.33 | 309.60 | 309.27 | 313.84 | 313.68 | | | | | |
| | CB-1B | DMH-1 | 0.47 | 6.00 | 5.80 | 2.73 | 12 | 0.018 | 0.011 | 5.61 | 7.14 | 3.47 | 18.6 | 0.04 | 0.33 | 309.60 | 309.27 | 313.73 | 313.68 | | | | | |
| | DMH-1 | HW #1 | 1.01 | 6.07 | 5.80 | 5.85 | 12 | 0.024 | 0.011 | 6.51 | 8.29 | 7.45 | 73.9 | 0.15 | 1.77 | 308.77 | 307.00 | 313.68 | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | |
| DA-3 | CB-2A | DMH-2 | 0.11 | 6.00 | 5.80 | 0.65 | 12 | 0.005 | 0.011 | 2.97 | 3.78 | 0.83 | 14.1 | 0.06 | 0.07 | 307.67 | 307.60 | 310.47 | 310.86 | | | | | |
| | CB-2B | DMH-2 | 0.08 | 6.00 | 5.80 | 0.47 | 12 | 0.007 | 0.011 | 3.48 | 4.43 | 0.60 | 10.3 | 0.04 | 0.07 | 307.67 | 307.60 | 310.47 | 310.86 | | | | | |
| | DMH-2 | HW #2 | 0.19 | 6.06 | 5.80 | 1.12 | 18 | 0.005 | 0.011 | 9.01 | 5.10 | 0.64 | 94.8 | 0.31 | 0.50 | 307.50 | 307.00 | 310.86 | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | IN | FILTRATION | | |
| | OCS | HW #2 | | | | 1.12 | 24 | 0.005 | 0.013 | 15.96 | 5.08 | 0.36 | 96.5 | 0.32 | 0.48 | 306.00 | 305.52 | | | | IIN | | N DAGIN | |

CONSTRUCTION PHASE INSPECTION FORMS

| North Street and Blackston Bellingham MA | e Street |
|--|-------------------|
| | |
| Date | Prev. Insp. Date: |
| Inspector: | Title: |
| Weather: | |
| | |
| Erosion Control - Inspect Weekly | |
| Comments: | |
| | |
| Corrective measures taken and date | |
| | |
| On Site Pavement Sweeping - Inspect Weekly | |
| Comments: | |
| | |
| Corrective measures taken and date | |
| | |
| Catch Basins - Inspect Weekly | |
| Comments: | |
| Corrective measures taken and date | |
| Corrective measures taken and date | |
| Stormceptor - Inspect Weekly | |
| Comments: | |
| | |
| Corrective measures taken and date | |
| | |
| Temporary Sediment Traps/Basins - Inspect Weekly | |
| Comments: | |
| | |
| Corrective measures taken and date | |

CONSTRUCTION PHASE INSPECTION FORMS

North Street and Blackstone Street

Bellingham MA

Notify Conservation Commission RE Issues Effecting Resource Areas

| Comments: |
|-----------|
|-----------|

Corrective measures taken and date

Silt on Public Streets - Inspect Weekly

Comments:

Corrective measures taken and date

Stock Pile Materials - Ring with Haybales - Inspect Weekly

Comments:

Corrective measures taken and date

Any Fuel or Chemical Spill - Inspect Daily

Comments:

Corrective measures taken and date

Post Construction Inspection Report North Street/Blackstone Street Bellingham, Massachusetts

| INSPECTION DATE: | | | | 1 | | | | |
|--|------|---------|--------|-------------------------|------|-----------|--|--|
| Person Inspecting | | Weather | | Other Personnel Present | | | | |
| | | Clear | | | | | | |
| ltem | N/A* | sat.** | NMR*** | CAM** | MCA* | Comments: | | |
| Pavement Swept | | | | | | | | |
| Catch Basins | | | | | | | | |
| CB #1A | | | | | | | | |
| CB #1B | | | | | | | | |
| CB #2A | | | | | | | | |
| CB #2B | | | | | | | | |
| Infiltration Basin #1 | | | | | | | | |
| | | | | | | | | |
| Sediment Forebay Infiltration Basin | | | | | | | | |
| | | | | | | | | |
| Inlet Basin #2 | | | | | | | | |
| Infiltration Basin | | | | | | | | |
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| | | | | | | | | |
| | | | | | | | | |
| NMR* normal maintenance | | | | | | | | |
| N/A* not applicable at the ti | | ection | | | | | | |
| CAM* corrective action - m | | | | | | | | |
| SAT* satisfactory condition | | ant | | | | | | |
| MCA* Major corrective action | on | | | | | | | |