Stormwater Report North Street & Blackstone Street Bellingham, MA



Date: December 30, 2022 November 7, 2023 February 13, 2024

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G&H Project F4457



# Massachusetts Department of Environmental Protection Bureau of Resource Protection - Wetlands Program Checklist for Stormwater Report

# A. Introduction

Important: When filling out forms on the computer, use only the tab key to move your cursor - do not use the return key.



A Stormwater Report must be submitted with the Notice of Intent permit application to document compliance with the Stormwater Management Standards. The following checklist is NOT a substitute for the Stormwater Report (which should provide more substantive and detailed information) but is offered here as a tool to help the applicant organize their Stormwater Management documentation for their Report and for the reviewer to assess this information in a consistent format. As noted in the Checklist, the Stormwater Report must contain the engineering computations and supporting information set forth in Volume 3 of the Massachusetts Stormwater Handbook. The Stormwater Report must be prepared and certified by a Registered Professional Engineer (RPE) licensed in the Commonwealth.

The Stormwater Report must include:

- The Stormwater Checklist completed and stamped by a Registered Professional Engineer (see page 2) that certifies that the Stormwater Report contains all required submittals.<sup>1</sup> This Checklist is to be used as the cover for the completed Stormwater Report.
- Applicant/Project Name
- Project Address
- Name of Firm and Registered Professional Engineer that prepared the Report
- Long-Term Pollution Prevention Plan required by Standards 4-6
- Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan required by Standard 8<sup>2</sup>
- Operation and Maintenance Plan required by Standard 9

In addition to all plans and supporting information, the Stormwater Report must include a brief narrative describing stormwater management practices, including environmentally sensitive site design and LID techniques, along with a diagram depicting runoff through the proposed BMP treatment train. Plans are required to show existing and proposed conditions, identify all wetland resource areas, NRCS soil types, critical areas, Land Uses with Higher Potential Pollutant Loads (LUHPPL), and any areas on the site where infiltration rate is greater than 2.4 inches per hour. The Plans shall identify the drainage areas for both existing and proposed conditions at a scale that enables verification of supporting calculations.

As noted in the Checklist, the Stormwater Management Report shall document compliance with each of the Stormwater Management Standards as provided in the Massachusetts Stormwater Handbook. The soils evaluation and calculations shall be done using the methodologies set forth in Volume 3 of the Massachusetts Stormwater Handbook.

To ensure that the Stormwater Report is complete, applicants are required to fill in the Stormwater Report Checklist by checking the box to indicate that the specified information has been included in the Stormwater Report. If any of the information specified in the checklist has not been submitted, the applicant must provide an explanation. The completed Stormwater Report Checklist and Certification must be submitted with the Stormwater Report.

<sup>&</sup>lt;sup>1</sup> The Stormwater Report may also include the Illicit Discharge Compliance Statement required by Standard 10. If not included in the Stormwater Report, the Illicit Discharge Compliance Statement must be submitted prior to the discharge of stormwater runoff to the post-construction best management practices.

<sup>&</sup>lt;sup>2</sup> For some complex projects, it may not be possible to include the Construction Period Erosion and Sedimentation Control Plan in the Stormwater Report. In that event, the issuing authority has the discretion to issue an Order of Conditions that approves the project and includes a condition requiring the proponent to submit the Construction Period Erosion and Sedimentation Control Plan before commencing any land disturbance activity on the site.



# B. Stormwater Checklist and Certification

The following checklist is intended to serve as a guide for applicants as to the elements that ordinarily need to be addressed in a complete Stormwater Report. The checklist is also intended to provide conservation commissions and other reviewing authorities with a summary of the components necessary for a comprehensive Stormwater Report that addresses the ten Stormwater Standards.

Note: Because stormwater requirements vary from project to project, it is possible that a complete Stormwater Report may not include information on some of the subjects specified in the Checklist. If it is determined that a specific item does not apply to the project under review, please note that the item is not applicable (N.A.) and provide the reasons for that determination.

A complete checklist must include the Certification set forth below signed by the Registered Professional Engineer who prepared the Stormwater Report.

## **Registered Professional Engineer's Certification**

I have reviewed the Stormwater Report, including the soil evaluation, computations, Long-term Pollution Prevention Plan, the Construction Period Erosion and Sedimentation Control Plan (if included), the Longterm Post-Construction Operation and Maintenance Plan, the Illicit Discharge Compliance Statement (if included) and the plans showing the stormwater management system, and have determined that they have been prepared in accordance with the requirements of the Stormwater Management Standards as further elaborated by the Massachusetts Stormwater Handbook. I have also determined that the information presented in the Stormwater Checklist is accurate and that the information presented in the Stormwater Report accurately reflects conditions at the site as of the date of this permit application.

Registered Professional Engineer Block and Signature



2/13/2024 ma

Signature and Date

## Checklist

Project Type: Is the application for new development, redevelopment, or a mix of new and redevelopment?

New development

Redevelopment

Mix of New Development and Redevelopment



**LID Measures:** Stormwater Standards require LID measures to be considered. Document what environmentally sensitive design and LID Techniques were considered during the planning and design of the project:

No disturbance to any Wetland Resource A	reas
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- Site Design Practices (e.g. clustered development, reduced frontage setbacks)
- Reduced Impervious Area (Redevelopment Only)
- Minimizing disturbance to existing trees and shrubs
- LID Site Design Credit Requested:
  - Credit 1
  - Credit 2
  - Credit 3
- Use of "country drainage" versus curb and gutter conveyance and pipe
- Bioretention Cells (includes Rain Gardens)
- Constructed Stormwater Wetlands (includes Gravel Wetlands designs)
- Treebox Filter
- Water Quality Swale
- Grass Channel
- Green Roof
- Other (describe):

### **Standard 1: No New Untreated Discharges**

- No new untreated discharges
- Outlets have been designed so there is no erosion or scour to wetlands and waters of the Commonwealth
- Supporting calculations specified in Volume 3 of the Massachusetts Stormwater Handbook included.



### Standard 2: Peak Rate Attenuation

- Standard 2 waiver requested because the project is located in land subject to coastal storm flowage and stormwater discharge is to a wetland subject to coastal flooding.
- Evaluation provided to determine whether off-site flooding increases during the 100-year 24-hour storm.

Calculations provided to show that post-development peak discharge rates do not exceed predevelopment rates for the 2-year and 10-year 24-hour storms. If evaluation shows that off-site flooding increases during the 100-year 24-hour storm, calculations are also provided to show that post-development peak discharge rates do not exceed pre-development rates for the 100-year 24hour storm.

### Standard 3: Recharge

Soil Analysis provided.

- Required Recharge Volume calculation provided.
- Required Recharge volume reduced through use of the LID site Design Credits.
- Sizing the infiltration, BMPs is based on the following method: Check the method used.

$\bowtie$	Static
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Dynamic Field<sup>1</sup>

 $\boxtimes$  Runoff from all impervious areas at the site discharging to the infiltration BMP.

Simple Dynamic

- Runoff from all impervious areas at the site is *not* discharging to the infiltration BMP and calculations are provided showing that the drainage area contributing runoff to the infiltration BMPs is sufficient to generate the required recharge volume.
- Recharge BMPs have been sized to infiltrate the Required Recharge Volume.
- Recharge BMPs have been sized to infiltrate the Required Recharge Volume *only* to the maximum extent practicable for the following reason:
  - Site is comprised solely of C and D soils and/or bedrock at the land surface
  - M.G.L. c. 21E sites pursuant to 310 CMR 40.0000
  - Solid Waste Landfill pursuant to 310 CMR 19.000
  - Project is otherwise subject to Stormwater Management Standards only to the maximum extent practicable.
- $\boxtimes$  Calculations showing that the infiltration BMPs will drain in 72 hours are provided.
- Property includes a M.G.L. c. 21E site or a solid waste landfill and a mounding analysis is included.

<sup>&</sup>lt;sup>1</sup> 80% TSS removal is required prior to discharge to infiltration BMP if Dynamic Field method is used.



### Standard 3: Recharge (continued)

- The infiltration BMP is used to attenuate peak flows during storms greater than or equal to the 10year 24-hour storm and separation to seasonal high groundwater is less than 4 feet and a mounding analysis is provided.
- Documentation is provided showing that infiltration BMPs do not adversely impact nearby wetland resource areas.

### **Standard 4: Water Quality**

The Long-Term Pollution Prevention Plan typically includes the following:

- Good housekeeping practices;
- Provisions for storing materials and waste products inside or under cover;
- Vehicle washing controls;
- Requirements for routine inspections and maintenance of stormwater BMPs;
- Spill prevention and response plans;
- Provisions for maintenance of lawns, gardens, and other landscaped areas;
- Requirements for storage and use of fertilizers, herbicides, and pesticides;
- Pet waste management provisions;
- Provisions for operation and management of septic systems;
- Provisions for solid waste management;
- Snow disposal and plowing plans relative to Wetland Resource Areas;
- Winter Road Salt and/or Sand Use and Storage restrictions;
- Street sweeping schedules;
- Provisions for prevention of illicit discharges to the stormwater management system;
- Documentation that Stormwater BMPs are designed to provide for shutdown and containment in the event of a spill or discharges to or near critical areas or from LUHPPL;
- Training for staff or personnel involved with implementing Long-Term Pollution Prevention Plan;
- List of Emergency contacts for implementing Long-Term Pollution Prevention Plan.
- A Long-Term Pollution Prevention Plan is attached to Stormwater Report and is included as an attachment to the Wetlands Notice of Intent.
- Treatment BMPs subject to the 44% TSS removal pretreatment requirement and the one inch rule for calculating the water quality volume are included, and discharge:
  - is within the Zone II or Interim Wellhead Protection Area
  - is near or to other critical areas
  - is within soils with a rapid infiltration rate (greater than 2.4 inches per hour)
  - involves runoff from land uses with higher potential pollutant loads.
- The Required Water Quality Volume is reduced through use of the LID site Design Credits.
- Calculations documenting that the treatment train meets the 80% TSS removal requirement and, if applicable, the 44% TSS removal pretreatment requirement, are provided.



Checklist (continued)
Standard 4: Water Quality (continued)
$\boxtimes$ The BMP is sized (and calculations provided) based on:
☐ The ½" or 1" Water Quality Volume or
The equivalent flow rate associated with the Water Quality Volume and documentation is provided showing that the BMP treats the required water quality volume.
☐ The applicant proposes to use proprietary BMPs, and documentation supporting use of proprietary BMP and proposed TSS removal rate is provided. This documentation may be in the form of the propriety BMP checklist found in Volume 2, Chapter 4 of the Massachusetts Stormwater Handbook and submitting copies of the TARP Report, STEP Report, and/or other third party studies verifying performance of the proprietary BMPs.
A TMDL exists that indicates a need to reduce pollutants other than TSS and documentation showing that the BMPs selected are consistent with the TMDL is provided.
Standard 5: Land Uses With Higher Potential Pollutant Loads (LUHPPLs)
<ul> <li>The NPDES Multi-Sector General Permit covers the land use and the Stormwater Pollution Prevention Plan (SWPPP) has been included with the Stormwater Report.</li> <li>The NPDES Multi-Sector General Permit covers the land use and the SWPPP will be submitted <i>prior to</i> the discharge of stormwater to the post-construction stormwater BMPs.</li> </ul>
☐ The NPDES Multi-Sector General Permit does <i>not</i> cover the land use.
LUHPPLs are located at the site and industry specific source control and pollution prevention measures have been proposed to reduce or eliminate the exposure of LUHPPLs to rain, snow, snow melt and runoff, and been included in the long term Pollution Prevention Plan.
All exposure has been eliminated.
All exposure has <i>not</i> been eliminated and all BMPs selected are on MassDEP LUHPPL list.
The LUHPPL has the potential to generate runoff with moderate to higher concentrations of oil and grease (e.g. all parking lots with >1000 vehicle trips per day) and the treatment train includes an oil

### **Standard 6: Critical Areas**

- The discharge is near or to a critical area and the treatment train includes only BMPs that MassDEP has approved for stormwater discharges to or near that particular class of critical area.
- Critical areas and BMPs are identified in the Stormwater Report.

grit separator, a filtering bioretention area, a sand filter or equivalent.



# Standard 7: Redevelopments and Other Projects Subject to the Standards only to the maximum extent practicable

The project is subject to the Stormwater Management Standards only to the maximum Extent Practicable as a:

Limited Project	ct
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- Small Residential Projects: 5-9 single family houses or 5-9 units in a multi-family development provided there is no discharge that may potentially affect a critical area.
- Small Residential Projects: 2-4 single family houses or 2-4 units in a multi-family development with a discharge to a critical area
- Marina and/or boatyard provided the hull painting, service and maintenance areas are protected from exposure to rain, snow, snow melt and runoff
- Bike Path and/or Foot Path
- Redevelopment Project
- Redevelopment portion of mix of new and redevelopment.
- Certain standards are not fully met (Standard No. 1, 8, 9, and 10 must always be fully met) and an explanation of why these standards are not met is contained in the Stormwater Report.

☐ The project involves redevelopment and a description of all measures that have been taken to improve existing conditions is provided in the Stormwater Report. The redevelopment checklist found in Volume 2 Chapter 3 of the Massachusetts Stormwater Handbook may be used to document that the proposed stormwater management system (a) complies with Standards 2, 3 and the pretreatment and structural BMP requirements of Standards 4-6 to the maximum extent practicable and (b) improves existing conditions.

### Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control

A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan must include the following information:

- Narrative;
- Construction Period Operation and Maintenance Plan;
- Names of Persons or Entity Responsible for Plan Compliance;
- Construction Period Pollution Prevention Measures;
- Erosion and Sedimentation Control Plan Drawings;
- Detail drawings and specifications for erosion control BMPs, including sizing calculations;
- Vegetation Planning;
- Site Development Plan;
- Construction Sequencing Plan;
- Sequencing of Erosion and Sedimentation Controls;
- Operation and Maintenance of Erosion and Sedimentation Controls;
- Inspection Schedule;
- Maintenance Schedule;
- Inspection and Maintenance Log Form.

A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan containing the information set forth above has been included in the Stormwater Report.



# Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control (continued)

- ☐ The project is highly complex and information is included in the Stormwater Report that explains why it is not possible to submit the Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan with the application. A Construction Period Pollution Prevention and Erosion and Sedimentation Control has *not* been included in the Stormwater Report but will be submitted *before* land disturbance begins.
- The project is *not* covered by a NPDES Construction General Permit.
- The project is covered by a NPDES Construction General Permit and a copy of the SWPPP is in the Stormwater Report.
- The project is covered by a NPDES Construction General Permit but no SWPPP been submitted. The SWPPP will be submitted BEFORE land disturbance begins.

### **Standard 9: Operation and Maintenance Plan**

- The Post Construction Operation and Maintenance Plan is included in the Stormwater Report and includes the following information:
  - Name of the stormwater management system owners;
  - Party responsible for operation and maintenance;
  - Schedule for implementation of routine and non-routine maintenance tasks;
  - Plan showing the location of all stormwater BMPs maintenance access areas;
  - Description and delineation of public safety features;
  - Estimated operation and maintenance budget; and
  - Operation and Maintenance Log Form.
- The responsible party is *not* the owner of the parcel where the BMP is located and the Stormwater Report includes the following submissions:
  - A copy of the legal instrument (deed, homeowner's association, utility trust or other legal entity) that establishes the terms of and legal responsibility for the operation and maintenance of the project site stormwater BMPs;
  - A plan and easement deed that allows site access for the legal entity to operate and maintain BMP functions.

### Standard 10: Prohibition of Illicit Discharges

- The Long-Term Pollution Prevention Plan includes measures to prevent illicit discharges;
- An Illicit Discharge Compliance Statement is attached;
- NO Illicit Discharge Compliance Statement is attached but will be submitted *prior to* the discharge of any stormwater to post-construction BMPs.

## **Project Description**

The project locus is a  $20.8\pm$  acre site located adjacent to North Street, and Blackstone Street. It is in the Agricultural District Zone. The project area contains approximately  $5.4\pm$  acres of land which will be fully developed, and the remaining lot area consists of approximately  $15.5\pm$  acres which will be designated as conservation land which will remain undeveloped. Run-off from this property generally flows from west to east ultimately captured within Bordering Vegetative Wetland (BVW) located in the easterly portion of the property. See Appendix 1/Locus Map.

Soils on site are in three categories – a Canton fine sandy loam 422B, 0 to 8% slopes, extremely stony, Hydrologic Group B, Canton fine sandy loam 420B, 3 to 8% slopes, Hydrologic Group B, and Merrimac fine sandy loam 254B, 3 to 8% slopes, Hydrologic Group A based on the web soil survey and site observations - See Appendix 2 / NRCS Soil Report.

The project proponent intends to construct a  $366\pm$  foot long roadway with bituminous concrete curbing and asphalt sidewalk. The proposed road will be 22' wide paved surface with access to Blackstone Street and will serve five 3-unit Townhouses. Each unit will have public water service and all units will be connected to a shared septic system for sewer. Storm water run-off will be collected by catch basin to manhole drainage system. A majority of run-off captured within the development will be sent to an infiltration basin, while the remaining runoff, will be conveyed through a series of drainage pipes and swales. Ultimately all the runoff generated from this development will be discharged to the existing wetlands located on the property to the east.

Pre-development drainage runoff from the site was analyzed as two watersheds - See Appendix 10 / Drainage Area Plans.

- EX-1 This watershed drainage area includes approximately 19.4± acres of both onsite and offsite areas. Runoff from this watershed flows easterly to an existing depression, which discharges overland when full to the bordering vegetative wetlands located on the east side of the property and is identified at the point of analysis (AP-1).
- EX-2 This watershed drainage area includes approximately 2.0± acres of contributing area. Runoff from this watershed flows overland southeasterly to Blackstone Street, which is identified at the point of analysis (AP-2).

The Post-Development Drainage Analysis regards the area as four watersheds – See Appendix 10 / Drainage Area Plans.

• PR-1 watershed consists of a proposed paved roadway, sidewalks, driveways, roofs, infiltration basin, and lawn areas of the proposed development which will be collected by the proposed drainage system. The entirety of the proposed drainage system is collected by street catch basins and conveyed by drainage pipes and

manholes to the proposed infiltration basin located in the eastern side of the project area, ultimately discharging to the wetlands located to the east within the proposed conservation area and is identified as point of analysis (AP-1).

- PR-2 watershed includes primarily the undeveloped portion of the property located along the north and west property lines, as well as a portion of the westerly lawn area. Topography and runoff patterns remain generally unchanged from the predevelopment conditions. Runoff generated in this sub catchment flows via surface flow to inlet basin #2 and is captured and conveyed via pipe to the proposed infiltration basin for infiltration and detention prior to discharging to the wetlands located to the east within the conservation easement and is identified as point of analysis (AP-1).
- PR-3 watershed includes primarily the undeveloped portion of the property which currently flows to Blackstone Street, as well as a portion of the southwesterly lawn area. Topography and runoff patterns remain generally unchanged from the predevelopment conditions. Runoff generated in this sub catchment flows via surface flow southeasterly to Blackstone Street, identified as point of analysis (AP-2).
- PR-4 watershed consists of that portion of the proposed lawn area not captured by the proposed drainage system, which flows easterly overland via swale, discharging to the wetlands identified as point of analysis (AP-1)

Post development stormwater runoff will be treated and attenuated by a standard catch basin to manhole collection system. The site has soils that are considered to have low stormwater runoff potential as identified in the NRCS Web Soil Survey information provided in Appendix 2. The site is designed to be in conformance with the Massachusetts Stormwater Management Guidelines, Massachusetts Wetlands Protection Act and the Town of Bellingham local bylaws and regulations for stormwater management and compliance.

### **Stormwater Design Parameter:**

The stormwater management system was designed to control the post-development rate of peak rainfall runoff from the site by keeping it below the post-development peak rate of rainfall runoff as stated as the objective in the Massachusetts Stormwater Handbook. The calculations were performed using the HydroCAD hydraulic program, developed by applied Microcomputer System. The HydroCAD software is based upon the Soil Conservation Service, "Technical Release 55 – Urban Hydrology for Small Watersheds" and is generally accepted industry methodology.

The analysis was performed for the 2-year, 10-year, and 100-year 24-hour storm events.

The following data was required for input:

• Watershed Area: Areas of each watershed were calculated and expressed in square feet for these calculations.

- SCS Curve Number (Cn): Based on the cover type and hydrologic soil group, a weighted curve number (CN) was determined for each of the existing watersheds utilizing Table 2-2a- *Runoff Curve Numbers For Urban Areas* and *Worksheet 2, Runoff Curve Number and Runoff* from the Soil Conservation Service Technical Release 55 Urban Hydrology for Small Watersheds.
- Time of Concentration, Tc (Minutes): The time of concentration for each watershed was determined by finding the time necessary for runoff to travel from the hydraulically most distant point in the watershed to the point of analysis. This was calculated by using a minimum time of 6 minutes for runoff to reach the most distant catch basin.
- SCS 24-Hour Storm Type: For the greater New England region, a Type III storm rainfall distribution is recommended for drainage calculations and was used for this project.
- Rainfall Precipitation: Rainfall precipitations used the Cornell Extreme Precipitations rainfall estimates for Norfolk County for the 2, 10, 25, and 100 year storm events and are as follows:

2-year storm event: 3.26 inches10-year storm event: 4.88 inches25 year storm event: 6.15 inches100-year storm event: 8.74 inches

An on-site conventional storm drainage collection system is designed based on the "Rational Method" using Manning's equation to carry a minimum 25-year storm event and underground culverts to carry a minimum 50-year storm event through the site (See Pipe Sizing Attachments). The proposed drainage pipes will be Reinforced Concrete Pipe (RCP), unless otherwise noted on the plans.

## Compliance with the 10 Stormwater Standards

### Standard 1: No new untreated Discharges

All Paved area runoff from the proposed development will flow across the pavement areas, accumulate into hooded catch basins, connect with drain pipe to a sediment forebay, which discharges to the infiltration basin. No new untreated stormwater discharges are proposed.

### Standard 2: Peak Rate Attenuation

To meet Standard 2, the post-development peak discharge rate must be equal to or less than pre-development rates to prevent storm damage and downstream and offsite flooding from the 2-year and the 10-year 24-hour storm events. In addition, the Bellingham Wetlands Bylaws require that runoff volumes not exceed pre-development conditions for up to the 25year storm. Additionally, surface basins are to be sized assuming frozen conditions within the basin, with no infiltration during a 25-year storm event. Peak discharge rates were calculated and evaluated at Blackstone Street and the existing wetlands. The point of evaluation is shown on the accompanying watershed plans.

In summary of the attached drainage analysis (HydroCAD), the peak discharge rates (cfs) and Volumes (af) at the point of evaluation are as follows;

	2-yr Storm	10-yr Storm	25-yr Storm	25-yr Storm	100-yr Storm
				Frozen Cond.	
Flow to Analysis Point (AP-1)					
Pre-Development	0.0 cfs	0.0 cfs	1.65 cfs	4.38 cfs	19.70 cfs
Post-Development	0.0 cfs	0.0 cfs	1.30 cfs	4.34 cfs	15.87 cfs
Flow to Analysis Point (AP-2)					
Pre-Development	0.21 cfs	1.43 cfs	2.74 cfs	N/A	5.94 cfs
Post-Development	0.21 cfs	1.42 cfs	2.73 cfs	N/A	5.90 cfs

### Table 1A: Peak Rate Attenuation Summary

### Table 1B: Runoff Volume

	2-yr Storm	10-yr Storm	25-yr Storm	25-yr Storm	100-yr Storm
Flow to Analysis Point (AP-1)				Frozen Cond.	
Pre-Development	0.000 af	0.00 af	0.15 af	1.39 af	1.93 af
Post-Development	0.000 af	0.00 af	0.12 af	2.11 af	1.34 af
Flow to Analysis Point (AP-2)					
Pre-Development	0.05 af	0.16 af	0.28 af	N/A	0.56 af
Post-Development	0.05 af	0.16 af	0.28 af	N/A	0.56 af

In addition to peak rate attenuation and volume reduction, an on-site storm drain collection system was designed based on the "Rational Method" using Manning's equation to carry a minimum 25-year storm event through the site. The proposed drainage pipes will be Class V reinforced concrete pipe (RCP). On-site storm drainage calculations are included in Appendix 11 / Supplemental Attachments.

### Standard 3: Recharge

### Soil Evaluation

Soil evaluation is broken down into two stages. Stage 1 identifies the underlying soils just beneath the surface that contribute to how much runoff is generated as stormwater falls and moves across the surface. Stage 2 evaluates the soils in direct contact with the proposed infiltration BMPs. Appendix 2 includes the NRCS Soil Survey used for Stage 1 while Appendix 3 includes the on-site soil textural analysis in the specific locations that infiltration

is proposed. The information from the NRCS Soil Survey is on the Pre and Post Development drainage plans in Appendix 10.

### Recharge Volume

The required recharge volume is determined by calculating the proposed impervious area over the corresponding soil identified in the NRCS Soil Survey. As previously stated, the NRCS Soil Survey lists the site as Canton Fine Sandy Loam, 0 to 8 percent slopes, HSG B, Canton Fine Sandy Loam, 3 to 8 percent slopes, HSG B, and Merrimac Fine Sandy Loam, 3 to 8 percent slopes, HSG B, and Merrimac Fine Sandy Loam, 3 to 8 percent slopes, the site consists of an existing undeveloped residential lot, the project is considered a new development project, as noted in Standard 7, therefore the recharge volume was calculated for the total impervious area.

	Recharge	Impervious	Volume
Hydrologic Group	(in/sqft)	(sqft)	(cf)
A - sand	0.60	57,369	2,868 cf
<b>B</b> - loam	0.35	0	0
<b>C</b> - silty loam	0.25	None	0
<b>D</b> - clay	0.10	None	0
Required Recharge Volume Total			2,868 cf

**Table 2: Required Recharge Volume Calculation** 

### Stormwater Basin Sizing

There are three ways of determining the recharge volume provided by a storm water basin (Static, Simple Dynamic and Dynamic Field). The Static Method, used here, includes the volume of water that can be stored beneath the lowest outlet of the basin. This, the most conservative method of determining the recharge volume, does not account for any infiltration that takes place while the basin is filling with water and is less dependent on maintenance of the basin since the only way for the water below the lowest invert can leave the basin is though infiltration. The following table summarizes the recharge volume provided by the infiltration basin. Detailed volume calculations for the basins are included in Appendix 5 / Stage-Area-Storage Calculations.

### Table 3: Basin Recharge Volume

	Recharge Volume
Basin 1	17,862 cf
Total	17,862 cf

### 72-hour Drawdown

When using the conservative Static Method to determine infiltration volume provided, the Rawls Rate is used to represent the infiltration rate in place of a hydraulic conductivity rate. The specific rate chosen is based on the textural analysis of the in-situ soil performed by a competent soil professional.

A Massachusetts Certified Soil Evaluator performed an evaluation of the soil at the proposed infiltration BMP. The soil textural analysis for the infiltration BMP is listed below with the associated Rawls Rate used in the calculations. Where textural analysis varied within any single BMP, the most restrictive textural evaluation and Rawls Rate were used. Soil logs of the in-situ soil evaluation are included in Appendix 3 / Field Soils Evaluation.

### Table 4: Rawls Rate

	Most Restrictive Soil Texture	Rawls Rate (in/hour)
Basin 1	Sand	8.27 in/hr

Drawdown time for the infiltration basin is determined by applying the Rawls Rate across the bottom area of the infiltration basin. The volume required for drawdown includes the entire volume below in the lowest outlet in the infiltration basin. The following table summarizes the drawdown time for the basin to show it will drawdown within the 72-hour maximum.

### Table 5: Basin Drawdown

	Storage Volume	<b>Bottom Area</b>	Time for Drawdown
Basin 1	17,862 cf	10,452 sf	3 hours

In addition, the HydroCAD model demonstrates that the proposed basin will fully dewater at the 26 hour mark during/after the 100-year design storm.

### Standard 4: Water Quality

### Water Quality Volume

The required water quality volume is determined through a calculation of the proposed impervious pavement throughout the site and a determination of whether the site is in a critical area, or the proposed use is considered to produce a high pollutant load. As noted in Standards 5 and 6, the land use does not qualify as a use with high pollutant load and no critical area was identified for this site. However, the required water quality volume is based on 1.0" as the soil recharge rate is 8.27 in/hr, meeting the threshold rate of 2.4 in/hr or greater, therefore, the water quality volume is calculated at 1.0" over the area of new proposed impervious pavement.

The area of impervious materials within the proposed site is calculated from the information entered HydroCAD and can be found in Appendix 4. One inch across 38,071 square feet of impervious pavement requires a water quality volume of 3,172.6 cubic feet. Detailed calculations for the infiltration basin are included in Appendix 5 / Stage-Area-Storage Calculations.

### Removal of Total Suspended Solids

The water quality volume, as calculated in the previous section, is treated through "Treatment Trains" to provide a minimum of 80 percent TSS removal including 44 percent TSS removal for pretreatment prior to discharging to the infiltration BMP. The TSS Removal Worksheets are included in Appendix 6 for the proposed treatment train. The infiltration basin in conjunction with deep sump hooded catch basins and sediment forebay complete the treatment trains at a minimum of 80 percent and 44 percent TSS removal.

### Forebay Sizing

All the stormwater from the impervious pavement is collected and discharged to the proposed sediment forebay which is sized to treat 0.1" of runoff from the 38,071-sf impervious area contributing to the basin. Detailed calculations for the sediment forebay are included in Appendix 5 / Stage-Area-Storage Calculations.

### $0.1^{"}/12^{"}$ per foot x 38,071 sf = 317.3 cf of storage required

### Table 6: Sediment Forebay Sizing

	Impervious Area being Discharged	Required Volume	Provided Volume
Forebay 1 @ Inv.=307.0	38,071 cf	317.3 c.f.	1,425c.f.

### Standard 5: Land Uses with Higher Potential Pollutant Loads

The proposed project is not a use that would qualify as a LUHPPL.

### Standard 6: Critical Areas

The proposed project is not within, nor does it discharge stormwater to an identified Critical Area. However, the site does contain soils with rapid infiltration rates (>2.41 in/hr), and must meet the 1" WQV requirement of Standard 4.

### Standard 7: Redevelopment Project

This project is not a redevelopment project.

### Standard 8: Construction Period Controls

A Construction Period Pollution Control Plan is included in Appendix 8 will be followed to prevent discharge of erosion to abutting properties.

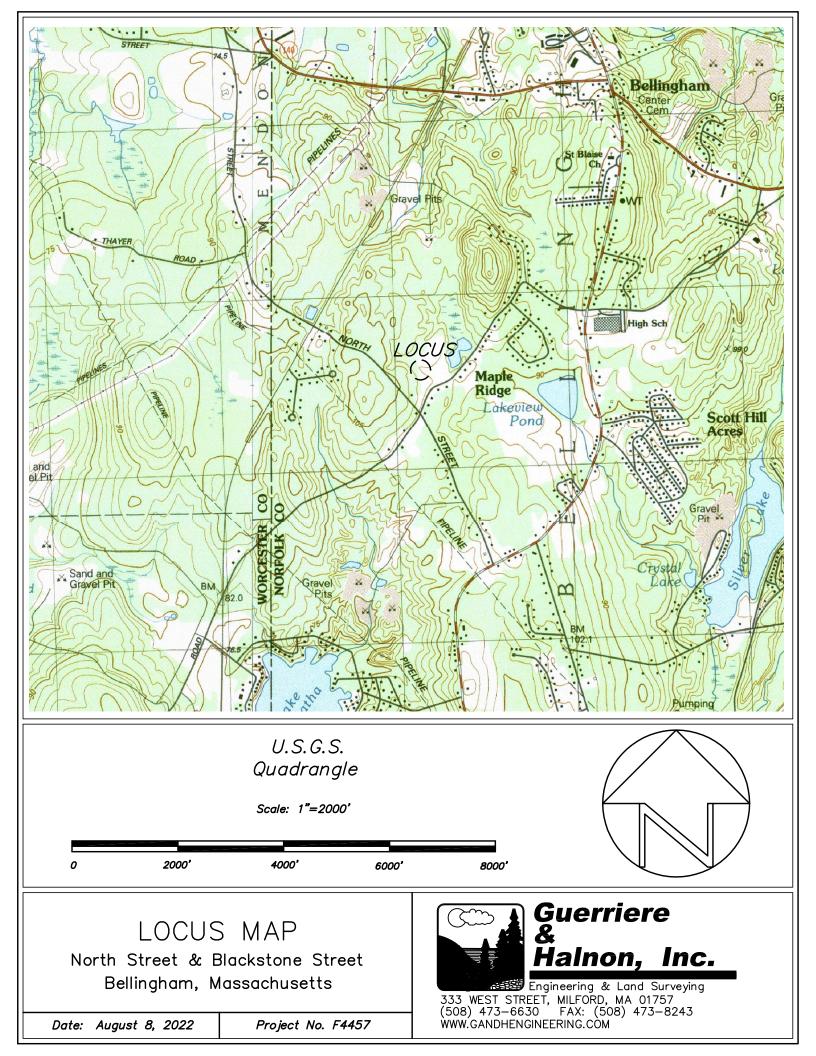
### Standard 9: Operation and Maintenance Plan

The Operation and Maintenance Plan included in Appendix 7 address the responsibilities of maintaining the stormwater BMPs.

### Standard 10: Illicit Discharges to Drainage System

It is the intent of the developer to follow the Construction Period Pollution Prevention Control Plan and the Order of Conditions to mitigate the affects of the proposed project on the adjacent environment. Following completion of construction, the Operation and Maintenance Plan will be provided to the property manager who will continue, the maintenance of the project. The Illicit Discharge Statement is included in Appendix 9.

# <u>Locus Map</u> Appendix 1



# NRCS Soils Report Appendix 2



United States Department of Agriculture

NRCS

Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

# Custom Soil Resource Report for Norfolk and Suffolk Counties, Massachusetts

North Street & Blackstone Street



# Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/? cid=nrcs142p2\_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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# **How Soil Surveys Are Made**

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

# Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



	MAP L	EGEND	1	MAP INFORMATION	
Area of Int	erest (AOI) Area of Interest (AOI)	8	Spoil Area Stony Spot	The soil surveys that comprise your AOI were mapped at 1:25,000.	
Soils	Soil Map Unit Polygons Soil Map Unit Lines	00 V	Very Stony Spot Wet Spot	Warning: Soil Map may not be valid at this scale. Enlargement of maps beyond the scale of mapping can cause	
Special F	Soil Map Unit Points Point Features	∆ ≁= Water Fe	Other Special Line Features	misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed	
9 2	Blowout Borrow Pit	Transport	Streams and Canals	scale. Please rely on the bar scale on each map sheet for map	
☆ ※	Clay Spot Closed Depression Gravel Pit	<b>∷</b>	Rails Interstate Highways	measurements. Source of Map: Natural Resources Conservation Service	
™ ∴ ©	Gravelly Spot Landfill	~ ~	US Routes Major Roads Local Roads	Web Soil Survey URL: Coordinate System: Web Mercator (EPSG:3857) Maps from the Web Soil Survey are based on the Web Mercator	
٨.	Lava Flow Marsh or swamp	Backgrou		projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.	
* 0 0	Mine or Quarry Miscellaneous Water Perennial Water			This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.	
~ +	Rock Outcrop Saline Spot			Soil Survey Area: Norfolk and Suffolk Counties, Massachusetts Survey Area Data: Version 17, Sep 3, 2021	
:: =	Sandy Spot Severely Eroded Spot Sinkhole			Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.	
ବ ୬ ୭	Slide or Slip Sodic Spot			Date(s) aerial images were photographed: May 24, 2020—Jul 18, 2020	
<i>120</i>				The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.	

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI		
53	Freetown muck, ponded, 0 to 1 percent slopes	2.0	9.5%		
254B	Merrimac fine sandy loam, 3 to 8 percent slopes	12.8	61.3%		
420B	Canton fine sandy loam, 3 to 8 percent slopes	1.3	6.1%		
422B	Canton fine sandy loam, 0 to 8 percent slopes, extremely stony	4.8	23.1%		
Totals for Area of Interest		20.8	100.0%		

# Map Unit Legend

# **Map Unit Descriptions**

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

## Norfolk and Suffolk Counties, Massachusetts

### 53—Freetown muck, ponded, 0 to 1 percent slopes

### **Map Unit Setting**

National map unit symbol: 2t2qc Elevation: 0 to 1,140 feet Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 140 to 240 days Farmland classification: Not prime farmland

### **Map Unit Composition**

*Freetown, ponded, and similar soils:* 85 percent *Minor components:* 15 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

### **Description of Freetown, Ponded**

### Setting

Landform: Kettles, marshes, depressions, depressions, bogs, swamps Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Tread, dip Down-slope shape: Concave Across-slope shape: Concave Parent material: Highly decomposed organic material

### **Typical profile**

*Oe - 0 to 2 inches:* mucky peat *Oa - 2 to 79 inches:* muck

### **Properties and qualities**

Slope: 0 to 1 percent
Surface area covered with cobbles, stones or boulders: 0.0 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Very poorly drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high (0.14 to 14.17 in/hr)
Depth to water table: About 0 to 6 inches
Frequency of flooding: Rare
Frequency of ponding: Frequent
Available water supply, 0 to 60 inches: Very high (about 19.2 inches)

### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 5w Hydrologic Soil Group: B/D Ecological site: F144AY043MA - Acidic Organic Wetlands Hydric soil rating: Yes

### **Minor Components**

### Whitman, ponded

Percent of map unit: 5 percent Landform: Depressions on ground moraines Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Base slope Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

### Scarboro

Percent of map unit: 5 percent Landform: Drainageways, depressions Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Base slope, tread, dip Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

### Swansea, ponded

Percent of map unit: 5 percent Landform: Bogs, swamps, marshes, depressions, depressions, kettles Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Tread, dip Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

### 254B—Merrimac fine sandy loam, 3 to 8 percent slopes

### Map Unit Setting

National map unit symbol: 2tyqs Elevation: 0 to 1,290 feet Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 140 to 240 days Farmland classification: All areas are prime farmland

### **Map Unit Composition**

*Merrimac and similar soils:* 85 percent *Minor components:* 15 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

### **Description of Merrimac**

### Setting

Landform: Outwash plains, outwash terraces, moraines, eskers, kames Landform position (two-dimensional): Summit, shoulder, backslope, footslope Landform position (three-dimensional): Crest, side slope, riser, tread Down-slope shape: Convex Across-slope shape: Convex

*Parent material:* Loamy glaciofluvial deposits derived from granite, schist, and gneiss over sandy and gravelly glaciofluvial deposits derived from granite, schist, and gneiss

### **Typical profile**

*Ap - 0 to 10 inches:* fine sandy loam *Bw1 - 10 to 22 inches:* fine sandy loam *Bw2 - 22 to 26 inches:* stratified gravel to gravelly loamy sand *2C - 26 to 65 inches:* stratified gravel to very gravelly sand

### **Properties and qualities**

Slope: 3 to 8 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Somewhat excessively drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very high (1.42 to 99.90 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 2 percent
Maximum salinity: Nonsaline (0.0 to 1.4 mmhos/cm)
Sodium adsorption ratio, maximum: 1.0
Available water supply, 0 to 60 inches: Low (about 4.6 inches)

### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2s Hydrologic Soil Group: A Ecological site: F145XY008MA - Dry Outwash Hydric soil rating: No

### **Minor Components**

### Hinckley

Percent of map unit: 5 percent Landform: Deltas, kames, eskers, outwash plains Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Head slope, nose slope, crest, side slope, rise Down-slope shape: Convex Across-slope shape: Convex, linear Hydric soil rating: No

### Sudbury

Percent of map unit: 5 percent Landform: Deltas, terraces, outwash plains Landform position (two-dimensional): Footslope Landform position (three-dimensional): Tread, dip Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

### Windsor

Percent of map unit: 3 percent Landform: Outwash terraces, dunes, deltas, outwash plains Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Tread, riser Down-slope shape: Linear, convex Across-slope shape: Linear, convex Hydric soil rating: No

### Agawam

Percent of map unit: 2 percent Landform: Outwash plains, outwash terraces, moraines, stream terraces, eskers, kames Landform position (three-dimensional): Rise Down-slope shape: Convex Across-slope shape: Convex

Hydric soil rating: No

### 420B—Canton fine sandy loam, 3 to 8 percent slopes

### **Map Unit Setting**

National map unit symbol: 2w81b Elevation: 0 to 1,180 feet Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 140 to 240 days Farmland classification: All areas are prime farmland

### **Map Unit Composition**

*Canton and similar soils:* 80 percent *Minor components:* 20 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

### **Description of Canton**

### Setting

Landform: Hills, moraines, ridges Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Nose slope, side slope, crest Down-slope shape: Convex, linear Across-slope shape: Convex Parent material: Coarse-loamy over sandy melt-out till derived from gneiss, granite, and/or schist

### **Typical profile**

Ap - 0 to 7 inches: fine sandy loam Bw1 - 7 to 15 inches: fine sandy loam Bw2 - 15 to 26 inches: gravelly fine sandy loam 2C - 26 to 65 inches: gravelly loamy sand

### **Properties and qualities**

Slope: 3 to 8 percent
Depth to restrictive feature: 19 to 39 inches to strongly contrasting textural stratification
Drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high (0.14 to 14.17 in/hr)

Depth to water table: More than 80 inches Frequency of flooding: None Frequency of ponding: None Available water supply, 0 to 60 inches: Very low (about 2.7 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2s Hydrologic Soil Group: B Ecological site: F144AY034CT - Well Drained Till Uplands Hydric soil rating: No

#### **Minor Components**

#### Scituate

Percent of map unit: 10 percent Landform: Hills, drumlins, ground moraines Landform position (two-dimensional): Summit, backslope, footslope Landform position (three-dimensional): Side slope, crest Down-slope shape: Convex, linear Across-slope shape: Convex Hydric soil rating: No

#### Montauk

Percent of map unit: 5 percent Landform: Moraines, ground moraines, hills, drumlins Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Side slope, crest Down-slope shape: Convex, linear Across-slope shape: Convex Hydric soil rating: No

#### Charlton

Percent of map unit: 4 percent Landform: Ridges, ground moraines, hills Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Side slope, crest Down-slope shape: Convex, linear Across-slope shape: Convex Hydric soil rating: No

#### Swansea

Percent of map unit: 1 percent Landform: Marshes, depressions, bogs, swamps, kettles Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

#### 422B—Canton fine sandy loam, 0 to 8 percent slopes, extremely stony

#### **Map Unit Setting**

National map unit symbol: 2w818 Elevation: 0 to 1,180 feet Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 145 to 240 days Farmland classification: Not prime farmland

#### Map Unit Composition

*Canton, extremely stony, and similar soils:* 80 percent *Minor components:* 20 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Canton, Extremely Stony**

#### Setting

Landform: Moraines, hills, ridges Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Nose slope, side slope, crest Down-slope shape: Convex, linear Across-slope shape: Convex Parent material: Coarse-loamy over sandy melt-out till derived from gneiss, granite, and/or schist

#### **Typical profile**

*Oi - 0 to 2 inches:* slightly decomposed plant material *A - 2 to 5 inches:* fine sandy loam *Bw1 - 5 to 16 inches:* fine sandy loam *Bw2 - 16 to 22 inches:* gravelly fine sandy loam *2C - 22 to 67 inches:* gravelly loamy sand

#### Properties and qualities

Slope: 0 to 8 percent
Surface area covered with cobbles, stones or boulders: 9.0 percent
Depth to restrictive feature: 19 to 39 inches to strongly contrasting textural stratification
Drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high (0.14 to 14.17 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)
Available water supply, 0 to 60 inches: Low (about 3.4 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s Hydrologic Soil Group: B Ecological site: F144AY034CT - Well Drained Till Uplands Hydric soil rating: No

#### **Minor Components**

#### Charlton, extremely stony

Percent of map unit: 6 percent Landform: Ridges, ground moraines, hills Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Side slope, crest Down-slope shape: Convex, linear Across-slope shape: Convex Hydric soil rating: No

#### Scituate, extremely stony

Percent of map unit: 6 percent Landform: Hills, ground moraines, drumlins Landform position (two-dimensional): Summit, backslope, footslope Landform position (three-dimensional): Side slope, crest Down-slope shape: Convex, linear Across-slope shape: Convex Hydric soil rating: No

#### Swansea

Percent of map unit: 4 percent Landform: Marshes, depressions, bogs, swamps, kettles Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

#### Montauk, extremely stony

Percent of map unit: 4 percent Landform: Recessionial moraines, ground moraines, hills, drumlins Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Side slope, crest Down-slope shape: Convex, linear Across-slope shape: Convex Hydric soil rating: No

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# Field Soils Evaluation Appendix 3



Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

Deep Observation Hole Number: DTH #1

Depth	Soil Horizon/ Layer	Soil Matrix: Color-Moist (Munsell)	Redo	oximorphic Fea (mottles)	tures	Soil Texture (USDA)	Coarse Fragments % by Volume		Soil Structure	Soil Consistence (Moist)	Other
(In.)			Depth	Color	Percent		Gravel	Cobbles & Stones			
0-10	А	10YR 3/3	-	-	-	S.L.	0	0	-	-	-
10-30	В	10YR 5/6	-	-	-	S.L.	0	0	-	-	-
30-108	С	2.5Y 5/4	-	-	-	SAND	20	20	-	-	-

Additional Notes WEEPING @ 96"



## Deep Observation Hole Number: DTH #2

Depth	Soil Horizon/ Layer	Soil Matrix: Color-Moist (Munsell)	Redo	ximorphic Fea (mottles)	tures	Soil Texture (USDA)	ure % by Volume DA)		Soil Structure	Soil Consistence (Moist)	Other
(In.)			Depth	Color	Percent		Gravel	Cobbles & Stones			
0-10	А	10YR 3/3	-	-	-	S.L.	0	0	-	-	-
10-20	В	10YR 5/6	-	-	-	S.L.	0	0	-	-	-
20-136	С	2.5Y 5/4	-	-	-	SAND	20	20	-	-	-

Additional Notes WEEPING @ 126"



Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

Deep Observation Hole Number: DTH-3

Depth	Soil Horizon/ Layer	Soil Matrix: Color-Moist (Munsell)	Redo	oximorphic Fea (mottles)	tures	Soil Texture (USDA)	Coarse Fragments % by Volume		Soil Structure	Soil Consistence (Moist)	Other
(In.)			Depth	Color	Percent		Gravel	Cobbles & Stones			
0-8	А	10YR 3/3	-	-	-	S.L.	0	0	-	-	-
8-30	В	10YR 5/6	-	-	-	S.L.	0	0	-	-	-
30-130	С	2.5Y 5/4	-	-	-	SAND	20	20	-	-	-

Additional Notes NO MOTTLES / WEEPING



# Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

Deep Observation Hole Number: DTH #4

Depth	Depth (In ) Soil Soil Matrix: Horizon/ Layer (Munsell)		Redoximorphic Features (mottles)			Soil Texture (USDA)	Coarse F % by \	ragments /olume	Soil Structure	Soil Consistence (Moist)	Other
(In.)			Depth	Color	Percent		Gravel	Cobbles & Stones			
0-8	А	10YR 3/3	-	-	-	S.L.	0	0	-	-	-
8-26	В	10YR 5/6	-	-	-	S.L.	0	0	-	-	-
26-156	С	2.5Y 5/4	-	-	-	SAND	20	20	-	-	-

Additional Notes WEEPING @ 156"



# Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

Deep Observation Hole Number: DTH #5

Depth	Soil Soil Matrix: Horizon/ Color-Moist Layer (Munsell)		Redoximorphic Features (mottles)			Soil Texture (USDA)	Coarse F % by \	ragments /olume	Soil Structure	Soil Consistence (Moist)	Other
(ln.)			Depth	Color	Percent		Gravel	Cobbles & Stones			
0-6	А	10YR 3/3	-	-	-	S.L.	0	0	-	-	-
6-18	В	10YR 5/6	-	-	-	S.L.	0	0	-	-	-
18-190	С	2.5Y 5/4	-	-	-	SAND	20	20	-	-	-

Additional Notes WEEPING @ 190"



## Deep Observation Hole Number: DTH #6

Soil Horizon/ Layer	Soil Matrix: Color-Moist (Munsell)	ist (mottles)			Soil Texture (USDA)	% by Volume		Soil Structure	Soil Consistence (Moist)	Other
		Depth	Color	Percent	. ,	Gravel	Cobbles & Stones		. ,	
A	10YR 3/3	-	-	-	S.L.	0	0	-	-	-
В	10YR 5/6	-	-	-	S.L.	0	0	-	-	-
С	2.5Y 5/4	-	-	-	SAND	20	20	-	-	-
	Horizon/ Layer A B	Horizon/ LayerColor-Moist (Munsell)A10YR 3/3B10YR 5/6	Horizon/ LayerColor-Moist (Munsell)DepthA10YR 3/3B10YR 5/6	Horizon/ LayerColor-Moist (Munsell)(mottles)DepthColorA10YR 3/3-B10YR 5/6-	Horizon/ LayerColor-Moist (Munsell)(mottles)DepthColorPercentA10YR 3/3B10YR 5/6	Horizon/ LayerColor-Moist (Munsell)(mottles)Texture (USDA) $A$ 10YR 3/3 $    B$ 10YR 5/6 $   S.L.$	Horizon/ LayerColor-Moist (Munsell)(mottles)Texture (USDA)% by M 	Horizon/ LayerColor-Moist (Munsell)(mottles)Texture (USDA)% by Volume $\overline{Depth}$ ColorPercent $\overline{Gravel}$ Cobbles & StonesA10YR 3/3S.L.00B10YR 5/6S.L.00	Horizon/ LayerColor-Moist (Munsell)(mottles)Texture (USDA)% by Volume $\overline{Depth}$ ColorPercent $\overline{Gravel}$ Cobbles & StonesA10YR 3/3S.L.00B10YR 5/6S.L.00-	Horizon/ LayerColor-Moist (Munsell)Image: mottles)Texture (USDA)% by VolumeCobbles & StonesConsistence (Moist)A10YR 3/3S.L.00B10YR 5/6S.L.00

Additional Notes NO MOTTLES OR WEEPING



Deep Observation Hole Number: DTH #7

Soil Horizon/ Layer	Soil Matrix: Color-Moist (Munsell)	st (mottles)			Soil Texture (USDA)	% by Volume		Soil Structure	Soil Consistence (Moist)	Other
		Depth	Color	Percent	, ,	Gravel	Cobbles & Stones		. ,	
А	10YR 3/3	-	-	-	S.L.	0	0	-	-	-
В	10YR 5/6	-	-	-	S.L.	0	0	-	-	-
С	2.5Y 5/4	-	-	-	L.S.	20	20	-	-	-
	Horizon/ Layer A B	Horizon/ LayerColor-Moist (Munsell)A10YR 3/3B10YR 5/6	Horizon/ LayerColor-Moist (Munsell)A10YR 3/3A10YR 5/6B10YR 5/6	Horizon/ LayerColor-Moist (Munsell)(mottles)DepthColorA10YR 3/3-B10YR 5/6-	Horizon/ LayerColor-Moist (Munsell)(mottles)DepthColorPercentA10YR 3/3B10YR 5/6	Horizon/ LayerColor-Moist (Munsell)(mottles)Texture (USDA) $Depth$ ColorPercentA10YR 3/3B10YR 5/6S.L.	Horizon/ LayerColor-Moist (Munsell)(mottles)Texture (USDA)% by Y $\overline{Depth}$ ColorPercent $\overline{Color}$ $Colo$	Horizon/ LayerColor-Moist (Munsell)(mottles)Texture (USDA)% by Volume $\overline{Depth}$ ColorPercent $\overline{Gravel}$ Cobbles & StonesA10YR 3/3S.L.00B10YR 5/6S.L.00	Horizon/ LayerColor-Moist (Munsell)(mottles)Texture (USDA)% by VolumeDepthColorPercentGravelCobbles & StonesA10YR 3/3S.L.00B10YR 5/6S.L.00-	Horizon/ LayerColor-Moist (Munsell)(mottles)Texture (USDA)% by VolumeConsistence (Moist)Consistence (Moist)A10YR 3/3-ColorPercentS.L.00B10YR 5/6S.L.00

Additional Notes NO MOTTLES OR WEEPING



Deep Observation Hole Number: DTH #8

Depth	Soil Horizon/ Layer	Soil Matrix: Color-Moist (Munsell)	t (mottles)			Soil Texture (USDA)	Coarse F % by V	ragments /olume	Soil Structure	Soil Consistence (Moist)	Other
(ln.)		. ,	Depth	Color	Percent	, ,	Gravel	Cobbles & Stones		. ,	
0-8	А	10YR 3/3	-	-	-	S.L.	0	0	-	-	-
8-24	В	10YR 5/6	-	-	-	S.L.	0	0	-	-	-
24-103	С	2.5Y 5/4	-	-	-	SAND	20	20	-	-	-

Additional Notes WATER @ 92"



Deep Observation Hole Number: DTH #9

Depth	Soil Horizon/ Layer	Soil Matrix: Color-Moist (Munsell)	Redoximorphic Features (mottles)			Soil Texture (USDA)	Coarse F % by V	Fragments Volume	Soil Structure	Soil Consistence (Moist)	Other
(ln.)			Depth	Color	Percent	. ,	Gravel	Cobbles & Stones		. ,	
0-48	F	-	-	-	-	-	-	-	-	-	-
48-108	С	2.5Y 5/4	-	-	-	SAND	20	20	-	-	-

Additional Notes WEEPING @ 80"



Deep Observation Hole Number: DTH #10

Depth	Soil Horizon/ Layer	Soil Matrix: Color-Moist (Munsell)	Redoximorphic Features (mottles)			Soil Texture (USDA)	Coarse F % by \	ragments /olume	Soil Structure	Soil Consistence (Moist)	Other
(ln.)		. ,	Depth	Color	Percent	. ,	Gravel	Cobbles & Stones			
0-14	А	10YR 3/3	-	-	-	S.L.	0	0	-	-	-
14-28	В	10YR 5/6	-	-	-	S.L.	0	0	-	-	-
28-42	C1	2.5Y 6/2	-	-	-	S.L.	0	0	-	-	-
42-100	C2	2.5Y 5/4	48"	-	-	SAND	20	20	-	-	-

Additional Notes WEEPING @ 86"



Deep Observation Hole Number: DTH #11

Soil Horizon/ Layer	Soil Matrix: Color-Moist (Munsell)	bist (mottles)			Soil Texture (USDA)	Coarse Fragments % by Volume		Soil Structure	Soil Consistence (Moist)	Other
		Depth	Color	Percent	, ,	Gravel	Cobbles & Stones		. ,	
А	10YR 3/3	-	-	-	S.L.	0	0	-	-	-
В	10YR 5/6	-	-	-	S.L.	0	0	-	-	-
С	2.5Y 5/4	-	-	-	SAND	20	20	-	-	-
	Horizon/ Layer A B	Horizon/ LayerColor-Moist (Munsell)A10YR 3/3B10YR 5/6	Horizon/ LayerColor-Moist (Munsell)DepthA10YR 3/3B10YR 5/6	Horizon/ LayerColor-Moist (Munsell)(mottles)DepthColorA10YR 3/3-B10YR 5/6-	Horizon/ LayerColor-Moist (Munsell)(mottles)DepthColorPercentA10YR 3/3B10YR 5/6	Horizon/ LayerColor-Moist (Munsell)(mottles)Texture (USDA)DepthColorPercentA10YR 3/3B10YR 5/6S.L.UUUUU	Horizon/ LayerColor-Moist (Munsell)(mottles)Texture (USDA)% by Y $\overline{Depth}$ ColorPercent $\overline{COD}$ $\overline{Cravel}$ $\overline{A}$ 10YR 3/3 $S.L.$ $0$ $\overline{B}$ 10YR 5/6 $S.L.$ $0$	Horizon/ LayerColor-Moist (Munsell)(mottles)Texture (USDA)% by Volume $\overline{Depth}$ ColorPercent $\overline{Gravel}$ Cobbles & StonesA10YR 3/3S.L.00B10YR 5/6S.L.00	Horizon/ LayerColor-Moist (Munsell)(mottles)Texture (USDA)% by Volume $\overline{Depth}$ ColorPercent $\overline{Gravel}$ Cobbles & StonesA10YR 3/3S.L.00B10YR 5/6S.L.00-	Horizon/ LayerColor-Moist (Munsell)(mottles)Texture (USDA)% by VolumeCobbles & StonesConsistence (Moist)A10YR 3/3S.L.00B10YR 5/6S.L.00

Additional Notes WEEPING @ 96"



Deep Observation Hole Number: DTH #12

Depth	Soil Horizon/ Layer	Soil Matrix: Color-Moist (Munsell)	st (mottles) )			Soil Texture (USDA)	Coarse F % by V	ragments /olume	Soil Structure	Soil Consistence (Moist)	Other
(ln.)			Depth	Color	Percent	, , ,	Gravel	Cobbles & Stones			
0-12	А	10YR 3/3	-	-	-	S.L.	0	0	-	-	-
12-104	С	2.5Y 5/4	-	-	-	SAND	20	20	-	-	-

Additional Notes WEEPING @ 90"



Deep Observation Hole Number: DTH #13

Depth	Soil Horizon/ Layer	Soil Matrix: Color-Moist (Munsell)	Redo	oximorphic Fea (mottles)	itures	Soil Texture (USDA)	Coarse Fragments % by Volume		Soil Structure		Other
(ln.)			Depth	Color	Percent		Gravel	Cobbles & Stones		. ,	
0-12	А	10YR 3/3	-	-	-	S.L.	0	0	-	-	-
12-24	В	10YR 5/6	-	-	-	S.L.	0	0	-	-	-
24-103	С	2.5Y 5/4	-	-	-	SAND	20	20	-	-	-

Additional Notes STANDING WATER @ 100"

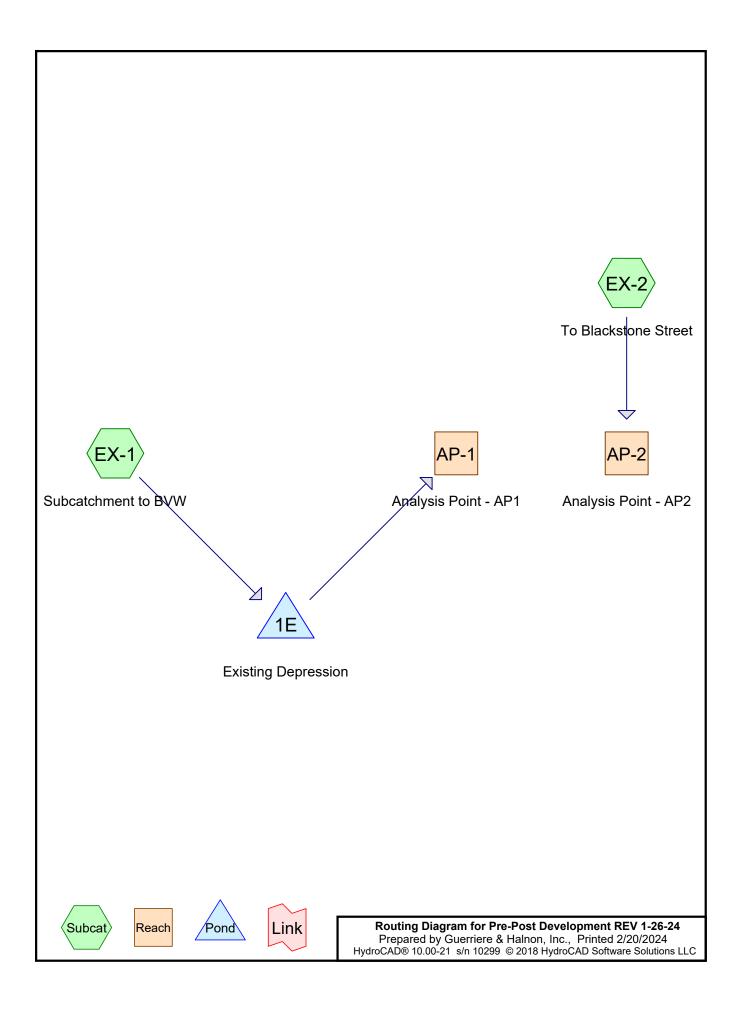


Deep Observation Hole Number: DTH #14

Depth	Soil Horizon/ Layer	Soil Matrix: Color-Moist (Munsell)	Redo	ximorphic Fea (mottles)	atures	Soil Texture (USDA)	Coarse Fragments % by Volume		Soil Structure Soil Consister (Moist)		e Other
(In.)			Depth	Color	Percent	. ,	Gravel	Cobbles & Stones			
0-6	А	10YR 3/3	-	-	-	S.L.	0	0	-	-	-
6-30	В	10YR 5/6	-	-	-	S.L.	0	0	-	-	-
30-114	С	2.5Y 5/4	-	-	-	SAND	20	20	-	-	-

Additional Notes WEEPING @ 100"

HydroCAD Calculations Appendix 4



Pre-Post Development REV 1-26-24 Prepared by Guerriere & Halnon, Inc. HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD Software Solutions LLC

## Area Listing (selected nodes)

Area	CN	Description	
(acres)		(subcatchment-numbers)	
3.753	39	>75% Grass cover, Good, HSG A (EX-1, EX-2)	
0.860	61	>75% Grass cover, Good, HSG B (EX-1, EX-2)	
0.646	98	Water Surface, HSG A (EX-1)	
2.399	30	Woods, Good, HSG A (EX-1, EX-2)	
13.720	55	Woods, Good, HSG B (EX-1, EX-2)	
21.377	51	TOTAL AREA	

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## Soil Listing (selected nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
6.798	HSG A	EX-1, EX-2
14.579	HSG B	EX-1, EX-2
0.000	HSG C	
0.000	HSG D	
0.000	Other	
21.377		TOTAL AREA

## Pre-Post Development REV 1-26-24

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 HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
 3.753	0.860	0.000	0.000	0.000	4.612	>75% Grass cover, Good	EX-1,
							EX-2
0.646	0.000	0.000	0.000	0.000	0.646	Water Surface	EX-1
2.399	13.720	0.000	0.000	0.000	16.119	Woods, Good	EX-1,
							EX-2
6.798	14.579	0.000	0.000	0.000	21.377	TOTAL AREA	

## Ground Covers (selected nodes)

Pre-Post Development REV 1-26-24 Prepared by Guerriere & Halnon, Inc. HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD	NRCC 24-hr C 2-Year Rainfall=3.26" Printed 2/20/2024 Software Solutions LLC Page 5
Runoff by SCS TR-20 m	hrs, dt=0.05 hrs, 1441 points hethod, UH=SCS, Weighted-CN hod - Pond routing by Dyn-Stor-Ind method
	off Area=844,997 sf  3.33% Impervious  Runoff Depth=0.14" gth=1,712'  Tc=41.8 min  CN=50  Runoff=0.41 cfs  0.228 af
	noff Area=86,206 sf   0.00% Impervious   Runoff Depth=0.30" ength=586'   Tc=15.6 min   CN=56   Runoff=0.21 cfs  0.049 af
Reach AP-1: Analysis Point - AP1	Inflow=0.00 cfs 0.000 af Outflow=0.00 cfs 0.000 af
Reach AP-2: Analysis Point - AP2	Inflow=0.21 cfs 0.049 af Outflow=0.21 cfs 0.049 af

Pond 1E: Existing DepressionPeak Elev=307.63' Storage=903 cfInflow=0.41 cfs0.228 afDiscarded=0.31 cfs0.228 afPrimary=0.00 cfs0.000 afOutflow=0.31 cfs0.228 af

Total Runoff Area = 21.377 acRunoff Volume = 0.277 afAverage Runoff Depth = 0.16"96.98% Pervious = 20.731 ac3.02% Impervious = 0.646 ac

Pre-Post Development REV 1-26-24

Prepared by Guerriere & Halnon, Inc. HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD Software Solutions LLC

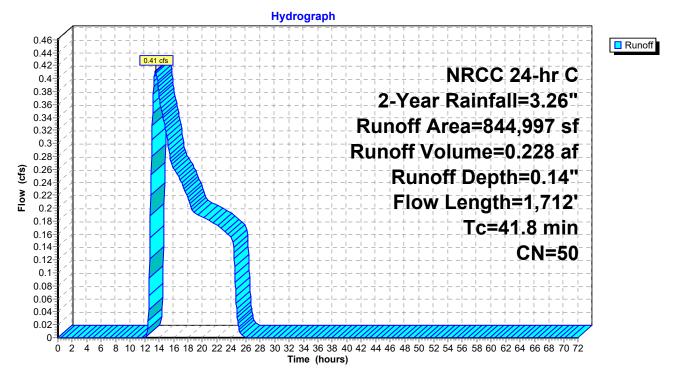
#### Summary for Subcatchment EX-1: Subcatchment to BVW

Runoff = 0.41 cfs @ 13.52 hrs, Volume= 0.228 af, Depth= 0.14"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 2-Year Rainfall=3.26"

A	rea (sf)	CN E	Description				
5	28,369	55 V	Woods, Good, HSG B				
	20,766	61 >	75% Gras	s cover, Go	bod, HSG B		
1	63,331	39 >	75% Gras	s cover, Go	bod, HSG A		
1	04,370	30 V	Voods, Go	od, HSG A			
	28,161	98 V	Vater Surfa	ace, HSG A	ι		
8	44,997	50 V	Veighted A	verage			
8	16,836	ç	96.67% Pei	vious Area			
	28,161	3	8.33% Impe	ervious Are	а		
Tc	Length	Slope	Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
7.0	50	0.0800	0.12		Sheet Flow, Segment A-B		
					Woods: Light underbrush n= 0.400 P2= 3.26"		
0.9	78	0.0800	1.41		Shallow Concentrated Flow, Segment B-C		
					Woodland Kv= 5.0 fps		
12.7	592	0.0240	0.77		Shallow Concentrated Flow, Segment C-D		
					Woodland Kv= 5.0 fps		
14.1	581	0.0190	0.69		Shallow Concentrated Flow, Segment D-E		
					Woodland Kv= 5.0 fps		
7.1	411	0.0190	0.96		Shallow Concentrated Flow, Segment E-F		
					Short Grass Pasture Kv= 7.0 fps		
41.8	1,712	Total					

#### Subcatchment EX-1: Subcatchment to BVW



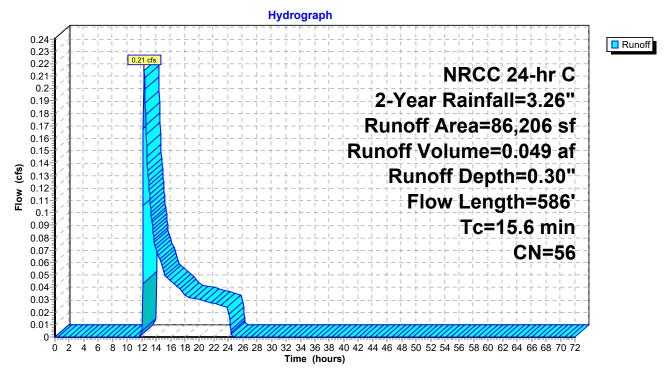
#### Summary for Subcatchment EX-2: To Blackstone Street

Runoff = 0.21 cfs @ 12.36 hrs, Volume= 0.049 af, Depth= 0.30"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 2-Year Rainfall=3.26"

A	rea (sf)	CN I	Description		
	69,268	55	Noods, Go	od, HSG B	
	16,676	61 :	>75% Gras	s cover, Go	bod, HSG B
	131	39 :	>75% Gras	s cover, Go	bod, HSG A
	131	30	Noods, Go	od, HSG A	
	86,206	56	Neighted A	verage	
	86,206		100.00% Pe	ervious Are	a
Tc	Length	Slope		Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
7.8	50	0.0610	0.11		Sheet Flow, Segment A-B
					Woods: Light underbrush n= 0.400 P2= 3.26"
2.8	215	0.0640	1.26		Shallow Concentrated Flow, Segment B-C
					Woodland Kv= 5.0 fps
2.2	103	0.0240	0.77		Shallow Concentrated Flow, Segment C-D
					Woodland Kv= 5.0 fps
2.8	218	0.0340	1.29		Shallow Concentrated Flow, Segment D-E
					Short Grass Pasture Kv= 7.0 fps
15.6	586	Total			

#### Subcatchment EX-2: To Blackstone Street



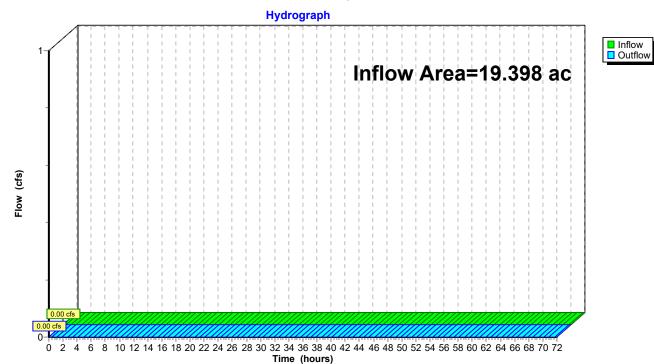
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## Summary for Reach AP-1: Analysis Point - AP1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =	19.398 ac,	3.33% Impervious, I	nflow Depth = 0.00	" for 2-Year event
Inflow =	0.00 cfs @	0.00 hrs, Volume=	0.000 af	
Outflow =	0.00 cfs @	0.00 hrs, Volume=	0.000 af, <i>A</i>	Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



## **Reach AP-1: Analysis Point - AP1**

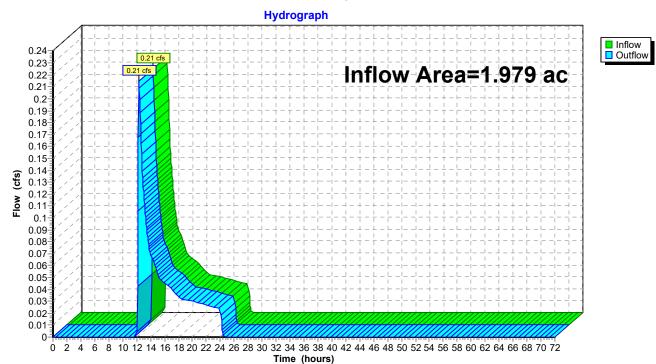
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### Summary for Reach AP-2: Analysis Point - AP2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area	a =	1.979 ac,	0.00% Impervious	, Inflow Depth = 0.3	30" for 2-Year event
Inflow	=	0.21 cfs @	12.36 hrs, Volum	e= 0.049 af	
Outflow	=	0.21 cfs @	12.36 hrs, Volum	e= 0.049 af,	Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



## Reach AP-2: Analysis Point - AP2

#### Summary for Pond 1E: Existing Depression

Inflow Area =	19.398 ac,	3.33% Impervious, Inflow [	Depth = 0.14" for 2-Year event
Inflow =	0.41 cfs @	13.52 hrs, Volume=	0.228 af
Outflow =	0.31 cfs @	15.06 hrs, Volume=	0.228 af, Atten= 24%, Lag= 92.2 min
Discarded =	0.31 cfs @	15.06 hrs, Volume=	0.228 af
Primary =	0.00 cfs @	0.00 hrs, Volume=	0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 307.63' @ 15.06 hrs Surf.Area= 5,351 sf Storage= 903 cf Flood Elev= 309.20' Surf.Area= 30,032 sf Storage= 29,481 cf

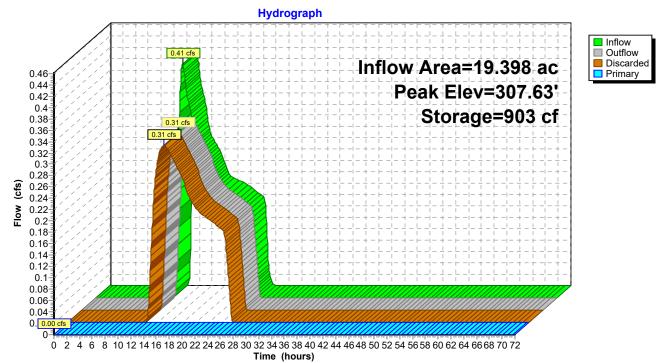
Plug-Flow detention time= 36.8 min calculated for 0.228 af (100% of inflow) Center-of-Mass det. time= 36.8 min (1,098.5 - 1,061.7)

Volume	Invert	Avail.Sto	brage Storage Description				
#1	307.30'	53,50	)7 cf Custom	n Stage Data (P	Prismatic)Listed below (Recalc)		
Flovetia		unf Arrag	In a Ctara	Curra Chara			
Elevatio		urf.Area	Inc.Store	Cum.Store			
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)			
307.3	30	48	0	0			
308.0	00	11,143	3,917	3,917			
309.00		28,160	19,652	23,568			
309.1	10	30,032	2,910	26,478			
310.0	00	30,032	27,029	53,507			
Device	Routing	Invert	Outlet Device	es			
#1	Discarded	307.30'	2.410 in/hr Exfiltration over Surface area		r Surface area		
			Conductivity to Groundwater Elevation = 304.00' Phase-In= 0.01'				
#2	Primary 309.05'		30.0' long x 5.0' breadth Broad-Crested Rectangular Weir				
<b>,</b>		Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00					
2.50 3.00 3.50 4.00							
				.70 2.68 2.68 2.66 2.65 2.65 2.65			
				66 2.68 2.70 2			
			2.05 2.07 2.	00 2.00 2.70 2	2.14 2.19 2.00		

**Discarded OutFlow** Max=0.31 cfs @ 15.06 hrs HW=307.63' (Free Discharge) **1=Exfiltration** (Controls 0.31 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=307.30' TW=0.00' (Dynamic Tailwater) 2=Broad-Crested Rectangular Weir( Controls 0.00 cfs) Prepared by Guerriere & Halnon, Inc. HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD Software Solutions LLC





<b>Pre-Post Development REV 1-26-24</b> Prepared by Guerriere & Halnon, Inc. <u>HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD Software Solut</u>	NRCC 24-hr C         10-Year Rainfall=4.88"           Printed         2/20/2024           ions LLC         Page 13						
Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method							
	97 sf  3.33% Impervious  Runoff Depth=0.64" =41.8 min  CN=50  Runoff=4.25 cfs  1.041 af						
	06 sf   0.00% Impervious   Runoff Depth=0.98" =15.6 min   CN=56   Runoff=1.43 cfs   0.162 af						
Reach AP-1: Analysis Point - AP1	Inflow=0.00 cfs 0.000 af Outflow=0.00 cfs 0.000 af						
Reach AP-2: Analysis Point - AP2	Inflow=1.43 cfs 0.162 af Outflow=1.43 cfs 0.162 af						
	Storage=12,684 cf Inflow=4.25 cfs 1.041 af						

ond 1E: Existing DepressionPeak Elev=308.55' Storage=12,684 cfInflow=4.25 cfs1.041 afDiscarded=1.33 cfs1.041 afPrimary=0.00 cfs0.000 afOutflow=1.33 cfs1.041 af

Total Runoff Area = 21.377 acRunoff Volume = 1.203 afAverage Runoff Depth = 0.68"96.98% Pervious = 20.731 ac3.02% Impervious = 0.646 ac

Pre-Post Development REV 1-26-24

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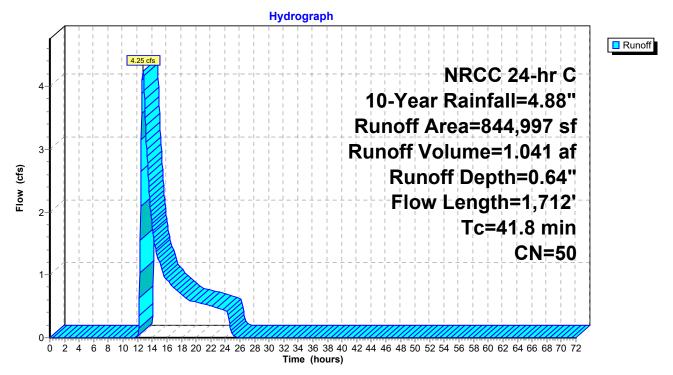
#### Summary for Subcatchment EX-1: Subcatchment to BVW

Runoff = 4.25 cfs @ 12.74 hrs, Volume= 1.041 af, Depth= 0.64"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 10-Year Rainfall=4.88"

A	rea (sf)	CN [	Description				
5	528,369 55 Woods, Good, HSG B			od, HSG B			
	20,766	61 >75% Grass cover, Good, HSG B					
1	163,331 39 >75% Grass cover, Go		s cover, Go	bod, HSG A			
104,370 30 Woods, Good, HS		od, HSG A					
28,161 98		98 V	Water Surface, HSG A				
8	844,997		Weighted Average				
8	816,836		96.67% Pervious Area				
28,161		3	3.33% Impervious Area				
Тс	Length	Slope		Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
7.0	50	0.0800	0.12		Sheet Flow, Segment A-B		
					Woods: Light underbrush n= 0.400 P2= 3.26"		
0.9	78	0.0800	1.41		Shallow Concentrated Flow, Segment B-C		
					Woodland Kv= 5.0 fps		
12.7	592	0.0240	0.77		Shallow Concentrated Flow, Segment C-D		
					Woodland Kv= 5.0 fps		
14.1	581	0.0190	0.69		Shallow Concentrated Flow, Segment D-E		
					Woodland Kv= 5.0 fps		
7.1	411	0.0190	0.96		Shallow Concentrated Flow, Segment E-F		
					Short Grass Pasture Kv= 7.0 fps		
41.8	1,712	Total					

## Subcatchment EX-1: Subcatchment to BVW



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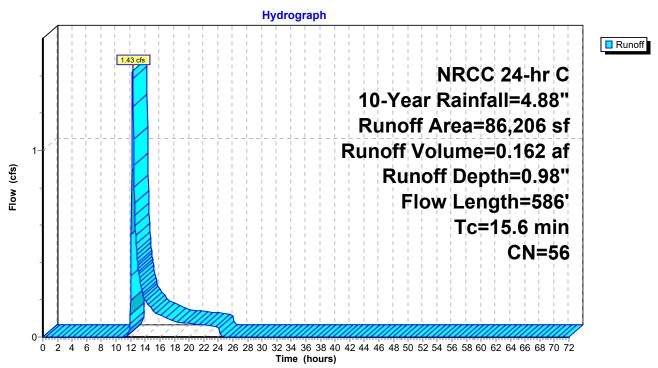
### Summary for Subcatchment EX-2: To Blackstone Street

Runoff = 1.43 cfs @ 12.27 hrs, Volume= 0.162 af, Depth= 0.98"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 10-Year Rainfall=4.88"

A	rea (sf)	CN	Description		
	69,268	55	Woods, Go	od, HSG B	
	16,676	61	>75% Gras	s cover, Go	bod, HSG B
	131	39	>75% Gras	s cover, Go	bod, HSG A
	131	30	Woods, Go	od, HSG A	
	86,206	56	Weighted A	verage	
	86,206		100.00% P	ervious Are	a
Tc	Length	Slope		Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
7.8	50	0.0610	0.11		Sheet Flow, Segment A-B
					Woods: Light underbrush n= 0.400 P2= 3.26"
2.8	215	0.0640	) 1.26		Shallow Concentrated Flow, Segment B-C
					Woodland Kv= 5.0 fps
2.2	103	0.0240	0.77		Shallow Concentrated Flow, Segment C-D
					Woodland Kv= 5.0 fps
2.8	218	0.0340	) 1.29		Shallow Concentrated Flow, Segment D-E
					Short Grass Pasture Kv= 7.0 fps
15.6	586	Total			

## Subcatchment EX-2: To Blackstone Street

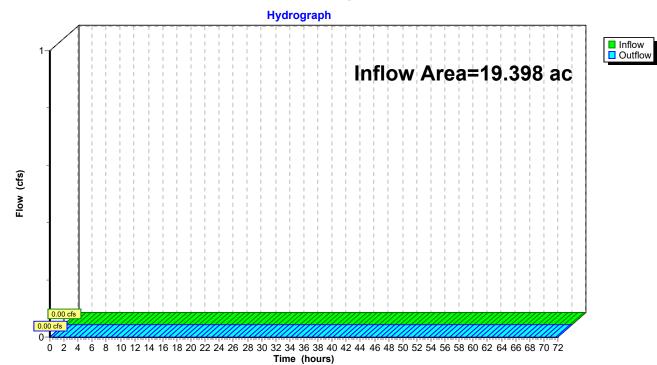


## Summary for Reach AP-1: Analysis Point - AP1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =	19.398 ac,	3.33% Impervious, Inflo	ow Depth = 0.00"	for 10-Year event
Inflow =	0.00 cfs @	0.00 hrs, Volume=	0.000 af	
Outflow =	0.00 cfs @	0.00 hrs, Volume=	0.000 af, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



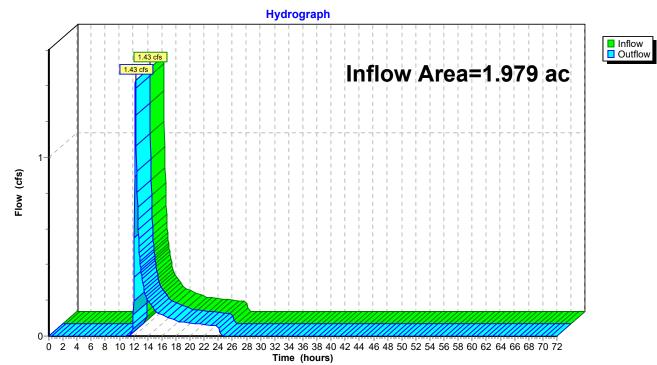
**Reach AP-1: Analysis Point - AP1** 

## Summary for Reach AP-2: Analysis Point - AP2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =	1.979 ac,	0.00% Impervious, Inflow D	epth = 0.98"	for 10-Year event
Inflow =	1.43 cfs @	12.27 hrs, Volume=	0.162 af	
Outflow =	1.43 cfs @	12.27 hrs, Volume=	0.162 af, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



# Reach AP-2: Analysis Point - AP2

## Summary for Pond 1E: Existing Depression

Inflow Area =	19.398 ac,	3.33% Impervious, Inflow E	Depth = 0.64" for 10-Year event
Inflow =	4.25 cfs @	12.74 hrs, Volume=	1.041 af
Outflow =	1.33 cfs @	14.65 hrs, Volume=	1.041 af, Atten= 69%, Lag= 114.5 min
Discarded =	1.33 cfs @	14.65 hrs, Volume=	1.041 af
Primary =	0.00 cfs @	0.00 hrs, Volume=	0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 308.55'@ 14.65 hrs Surf.Area= 20,556 sf Storage= 12,684 cf Flood Elev= 309.20' Surf.Area= 30,032 sf Storage= 29,481 cf

Plug-Flow detention time= 125.6 min calculated for 1.040 af (100% of inflow) Center-of-Mass det. time= 125.6 min (1,094.8 - 969.2)

Volume	Invert	Avail.Stor	rage Storage	Description	
#1	307.30'	53,50	)7 cf Custom	n Stage Data (P	rismatic)Listed below (Recalc)
	0	- <b>F</b> A		0	
Elevatio		rf.Area	Inc.Store	Cum.Store	
(fee	t)	(sq-ft)	(cubic-feet)	(cubic-feet)	
307.3	0	48	0	0	
308.0	0	11,143	3,917	3,917	
309.0	0	28,160	19,652	23,568	
309.1	0	30,032	2,910	26,478	
310.0	0	30,032	27,029	53,507	
Device	Routing	Invert	Outlet Device	es	
#1	Discarded	307.30'	2.410 in/hr E	xfiltration over	Surface area
			Conductivity	to Groundwater	Elevation = 304.00' Phase-In= 0.01'
#2	Primary	309.05'	30.0' long x	5.0' breadth Br	oad-Crested Rectangular Weir
	-		Head (feet) (	0.20 0.40 0.60	0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00 3.	50 4.00 4.50 5	.00 5.50
			Coef. (Englis	h) 2.34 2.50 2.	70 2.68 2.68 2.66 2.65 2.65 2.65
			( U	66 2.68 2.70 2	
			Conductivity 30.0' long x Head (feet) ( 2.50 3.00 3. Coef. (Englis	to Groundwater <b>5.0' breadth Br</b> 0.20 0.40 0.60 50 4.00 4.50 5 h) 2.34 2.50 2.	Elevation = 304.00' Phase-In= 0.01' oad-Crested Rectangular Weir 0.80 1.00 1.20 1.40 1.60 1.80 2.00 5.00 5.50 70 2.68 2.68 2.66 2.65 2.65 2.65

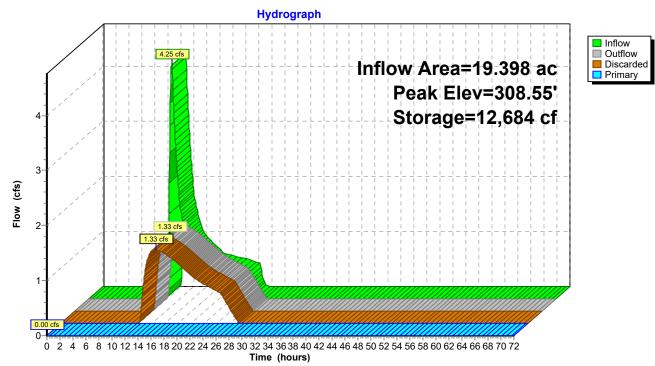
**Discarded OutFlow** Max=1.33 cfs @ 14.65 hrs HW=308.55' (Free Discharge) **1=Exfiltration** (Controls 1.33 cfs)

**Primary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=307.30' TW=0.00' (Dynamic Tailwater) **2=Broad-Crested Rectangular Weir**(Controls 0.00 cfs)

## Pre-Post Development REV 1-26-24

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# Pond 1E: Existing Depression



Pre-Post Development REV 1-26-24 Prepared by Guerriere & Halnon, Inc. HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD Software Solution	NRCC 24-hr C 25-Year Rainfall=6.15" Printed 2/20/2024 ons LLC Page 21
Time span=0.00-72.00 hrs, dt=0.05 h Runoff by SCS TR-20 method, UH=SC Reach routing by Dyn-Stor-Ind method - Pond roo	CS, Weighted-CN
	7 sf 3.33% Impervious Runoff Depth=1.22" 1.8 min CN=50 Runoff=10.15 cfs 1.968 af
	6 sf 0.00% Impervious Runoff Depth=1.69" :15.6 min CN=56 Runoff=2.74 cfs 0.278 af
Reach AP-1: Analysis Point - AP1	Inflow=1.65 cfs 0.147 af Outflow=1.65 cfs 0.147 af
Reach AP-2: Analysis Point - AP2	Inflow=2.74 cfs 0.278 af Outflow=2.74 cfs 0.278 af
	Storage=27,439 cf Inflow=10.15 cfs 1.968 af 1.65 cfs 0.147 af Outflow=3.71 cfs 1.968 af

Total Runoff Area = 21.377 acRunoff Volume = 2.246 afAverage Runoff Depth = 1.26"96.98% Pervious = 20.731 ac3.02% Impervious = 0.646 ac

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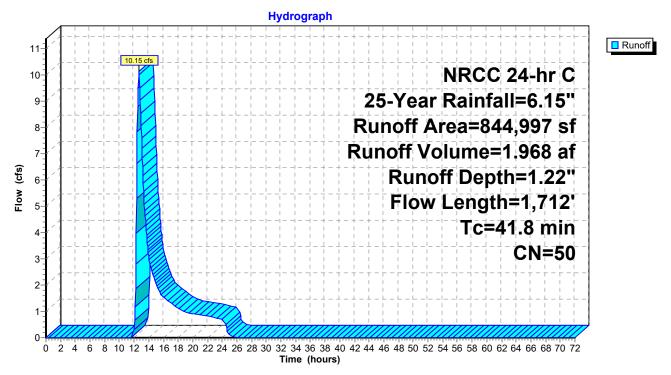
## Summary for Subcatchment EX-1: Subcatchment to BVW

Runoff = 10.15 cfs @ 12.67 hrs, Volume= 1.968 af, Depth= 1.22"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 25-Year Rainfall=6.15"

A	rea (sf)	CN [	Description		
5	28,369	55 V	Voods, Go	od, HSG B	
	20,766	61 >	75% Gras	s cover, Go	bod, HSG B
1	63,331	39 >	•75% Gras	s cover, Go	bod, HSG A
1	04,370	30 V	Voods, Go	od, HSG A	
	28,161	98 V	Vater Surfa	ace, HSG A	ι
8	44,997	50 V	Veighted A	verage	
8	16,836	ç	96.67% Pei	vious Area	
	28,161	3	8.33% Impe	ervious Are	а
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
7.0	50	0.0800	0.12		Sheet Flow, Segment A-B
					Woods: Light underbrush n= 0.400 P2= 3.26"
0.9	78	0.0800	1.41		Shallow Concentrated Flow, Segment B-C
					Woodland Kv= 5.0 fps
12.7	592	0.0240	0.77		Shallow Concentrated Flow, Segment C-D
					Woodland Kv= 5.0 fps
14.1	581	0.0190	0.69		Shallow Concentrated Flow, Segment D-E
					Woodland Kv= 5.0 fps
7.1	411	0.0190	0.96		Shallow Concentrated Flow, Segment E-F
					Short Grass Pasture Kv= 7.0 fps
41.8	1,712	Total			

## Subcatchment EX-1: Subcatchment to BVW



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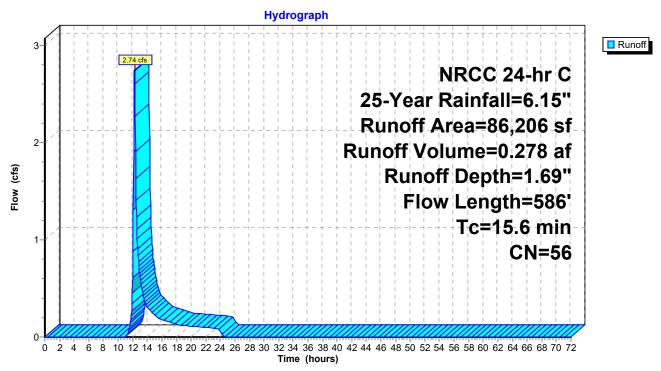
### Summary for Subcatchment EX-2: To Blackstone Street

Runoff = 2.74 cfs @ 12.26 hrs, Volume= 0.278 af, Depth= 1.69"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 25-Year Rainfall=6.15"

A	rea (sf)	CN	Description		
	69,268	55	Woods, Go	od, HSG B	
	16,676	61	>75% Gras	s cover, Go	bod, HSG B
	131	39	>75% Gras	s cover, Go	bod, HSG A
	131	30	Woods, Go	od, HSG A	
	86,206	56	Weighted A	verage	
	86,206		100.00% P	ervious Are	a
Tc	Length	Slope		Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
7.8	50	0.0610	0.11		Sheet Flow, Segment A-B
					Woods: Light underbrush n= 0.400 P2= 3.26"
2.8	215	0.0640	1.26		Shallow Concentrated Flow, Segment B-C
					Woodland Kv= 5.0 fps
2.2	103	0.0240	0.77		Shallow Concentrated Flow, Segment C-D
					Woodland Kv= 5.0 fps
2.8	218	0.0340	1.29		Shallow Concentrated Flow, Segment D-E
					Short Grass Pasture Kv= 7.0 fps
15.6	586	Total			

## Subcatchment EX-2: To Blackstone Street

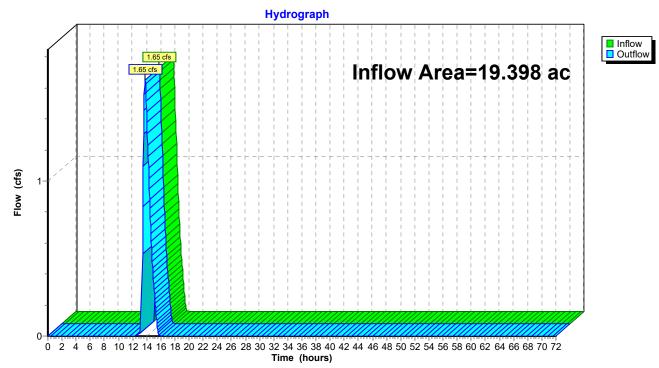


## Summary for Reach AP-1: Analysis Point - AP1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =	19.398 ac,	3.33% Impervious, Inflow I	Depth = 0.09"	for 25-Year event
Inflow =	1.65 cfs @	13.77 hrs, Volume=	0.147 af	
Outflow =	1.65 cfs @	13.77 hrs, Volume=	0.147 af, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



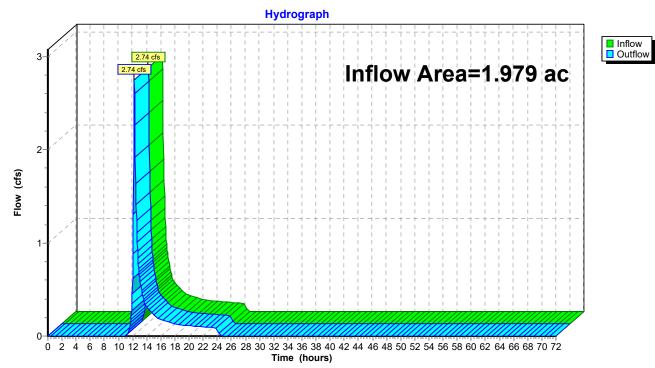
# Reach AP-1: Analysis Point - AP1

## Summary for Reach AP-2: Analysis Point - AP2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area	a =	1.979 ac,	0.00% Impervious,	Inflow Depth = 1.6	9" for 25-Year event
Inflow	=	2.74 cfs @	12.26 hrs, Volum	e= 0.278 af	
Outflow	=	2.74 cfs @	12.26 hrs, Volume	e= 0.278 af,	Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



# Reach AP-2: Analysis Point - AP2

## Summary for Pond 1E: Existing Depression

Inflow Area =	19.398 ac,	3.33% Impervious, Inflow D	epth = 1.22" for 25-Year event
Inflow =	10.15 cfs @	12.67 hrs, Volume=	1.968 af
Outflow =	3.71 cfs @	13.77 hrs, Volume=	1.968 af, Atten= 63%, Lag= 66.0 min
Discarded =	2.06 cfs @	13.77 hrs, Volume=	1.821 af
Primary =	1.65 cfs @	13.77 hrs, Volume=	0.147 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 309.13' @ 13.77 hrs Surf.Area= 30,032 sf Storage= 27,439 cf Flood Elev= 309.20' Surf.Area= 30,032 sf Storage= 29,481 cf

Plug-Flow detention time= 163.1 min calculated for 1.966 af (100% of inflow) Center-of-Mass det. time= 163.2 min (1,104.2 - 941.0)

Volume	Invert	Avail.Sto	rage Storage	Description	
#1	307.30	53,50	07 cf Custom	n Stage Data (P	rismatic)Listed below (Recalc)
Elevatio (fee 307.3 308.0 309.0 309.7 310.0	et) 30 00 00 10	urf.Area (sq-ft) 48 11,143 28,160 30,032 30,032	Inc.Store (cubic-feet) 0 3,917 19,652 2,910 27,029	Cum.Store (cubic-feet) 0 3,917 23,568 26,478 53,507	
Device	Routing	Invert	Outlet Device		
#1	Discarded	307.30'	2.410 in/hr E	xfiltration over	Surface area
#2	Primary	309.05'	<b>30.0' long x</b> Head (feet) 0 2.50 3.00 3.4 Coef. (English	<b>5.0' breadth Br</b> 0.20 0.40 0.60 50 4.00 4.50 5	70 2.68 2.68 2.66 2.65 2.65 2.65

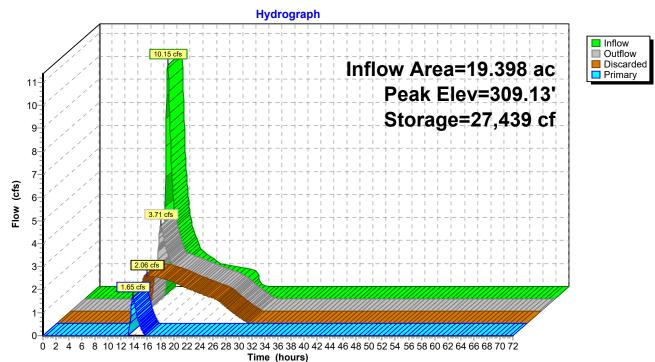
**Discarded OutFlow** Max=2.06 cfs @ 13.77 hrs HW=309.13' (Free Discharge) **1=Exfiltration** (Controls 2.06 cfs)

Primary OutFlow Max=1.65 cfs @ 13.77 hrs HW=309.13' TW=0.00' (Dynamic Tailwater) ←2=Broad-Crested Rectangular Weir (Weir Controls 1.65 cfs @ 0.67 fps)

# Pre-Post Development REV 1-26-24

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# Pond 1E: Existing Depression



<b>Pre-Post Development REV 1-26-24</b> Prepared by Guerriere & Halnon, Inc. HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD Software Sol	NRCC 24-hr C 100-Year Rainfall=8.74" Printed 2/20/2024 utions LLC Page 29
Time span=0.00-72.00 hrs, dt=0.0 Runoff by SCS TR-20 method, UH= Reach routing by Dyn-Stor-Ind method - Pond	SCS, Weighted-CN
	,997 sf  3.33% Impervious  Runoff Depth=2.71" c=41.8 min  CN=50  Runoff=26.44 cfs  4.387 af
	,206 sf 0.00% Impervious Runoff Depth=3.42" Fc=15.6 min CN=56 Runoff=5.94 cfs 0.564 af
Reach AP-1: Analysis Point - AP1	Inflow=19.70 cfs 1.933 af Outflow=19.70 cfs 1.933 af
Reach AP-2: Analysis Point - AP2	Inflow=5.94 cfs 0.564 af Outflow=5.94 cfs 0.564 af
	' Storage=37,263 cf Inflow=26.44 cfs 4.387 af 19.70 cfs 1.933 af Outflow=21.89 cfs 4.387 af

Total Runoff Area = 21 377 ac. Runoff Volume = 4 951 af. Average Runoff Denth = 2 78

Total Runoff Area = 21.377 acRunoff Volume = 4.951 afAverage Runoff Depth = 2.78"96.98% Pervious = 20.731 ac3.02% Impervious = 0.646 ac

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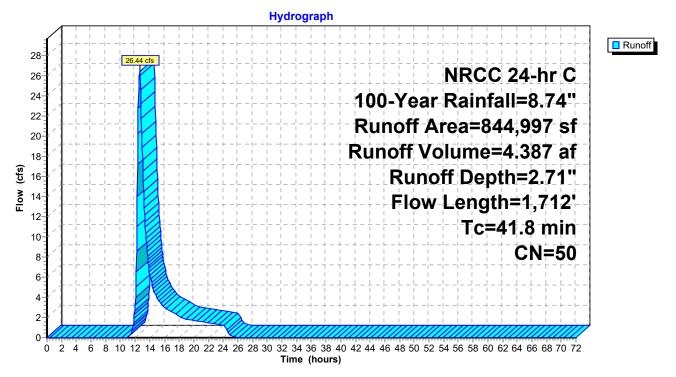
## Summary for Subcatchment EX-1: Subcatchment to BVW

Runoff = 26.44 cfs @ 12.61 hrs, Volume= 4.387 af, Depth= 2.71"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 100-Year Rainfall=8.74"

A	rea (sf)	CN [	Description		
5	28,369	55 V	Voods, Go	od, HSG B	
	20,766	61 >	75% Gras	s cover, Go	bod, HSG B
1	63,331	39 >	•75% Gras	s cover, Go	bod, HSG A
1	04,370	30 V	Voods, Go	od, HSG A	
	28,161	98 V	Vater Surfa	ace, HSG A	ι
8	44,997	50 V	Veighted A	verage	
8	16,836	ç	96.67% Pei	vious Area	
	28,161	3	8.33% Impe	ervious Are	а
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
7.0	50	0.0800	0.12		Sheet Flow, Segment A-B
					Woods: Light underbrush n= 0.400 P2= 3.26"
0.9	78	0.0800	1.41		Shallow Concentrated Flow, Segment B-C
					Woodland Kv= 5.0 fps
12.7	592	0.0240	0.77		Shallow Concentrated Flow, Segment C-D
					Woodland Kv= 5.0 fps
14.1	581	0.0190	0.69		Shallow Concentrated Flow, Segment D-E
					Woodland Kv= 5.0 fps
7.1	411	0.0190	0.96		Shallow Concentrated Flow, Segment E-F
					Short Grass Pasture Kv= 7.0 fps
41.8	1,712	Total			

## Subcatchment EX-1: Subcatchment to BVW



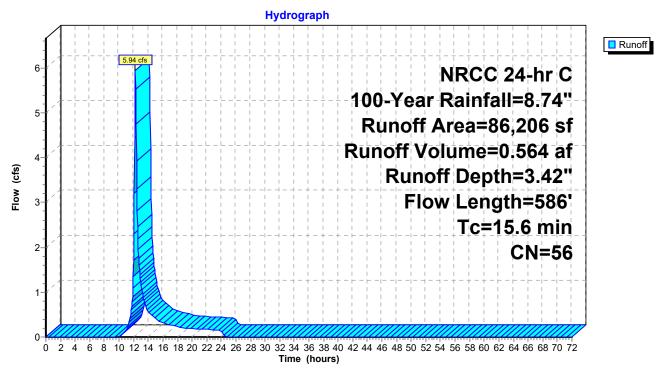
## Summary for Subcatchment EX-2: To Blackstone Street

Runoff = 5.94 cfs @ 12.25 hrs, Volume= 0.564 af, Depth= 3.42"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 100-Year Rainfall=8.74"

A	rea (sf)	CN	Description		
	69,268	55	Woods, Go	od, HSG B	
	16,676	61	>75% Gras	s cover, Go	bod, HSG B
	131	39	>75% Gras	s cover, Go	bod, HSG A
	131	30	Woods, Go	od, HSG A	
	86,206	56	Weighted A	verage	
	86,206		100.00% P	ervious Are	a
Tc	Length	Slope		Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
7.8	50	0.0610	0.11		Sheet Flow, Segment A-B
					Woods: Light underbrush n= 0.400 P2= 3.26"
2.8	215	0.0640	1.26		Shallow Concentrated Flow, Segment B-C
					Woodland Kv= 5.0 fps
2.2	103	0.0240	0.77		Shallow Concentrated Flow, Segment C-D
					Woodland Kv= 5.0 fps
2.8	218	0.0340	1.29		Shallow Concentrated Flow, Segment D-E
					Short Grass Pasture Kv= 7.0 fps
15.6	586	Total			

## Subcatchment EX-2: To Blackstone Street

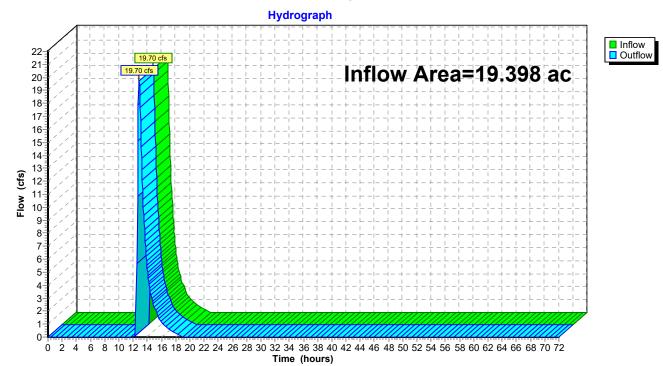


## Summary for Reach AP-1: Analysis Point - AP1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Are	a =	19.398 ac,	3.33% Impervious	, Inflow Depth = 1.20	0" for 100-Year event
Inflow	=	19.70 cfs @	12.85 hrs, Volum	ie= 1.933 af	
Outflow	=	19.70 cfs @	12.85 hrs, Volum	e= 1.933 af, <i>i</i>	Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



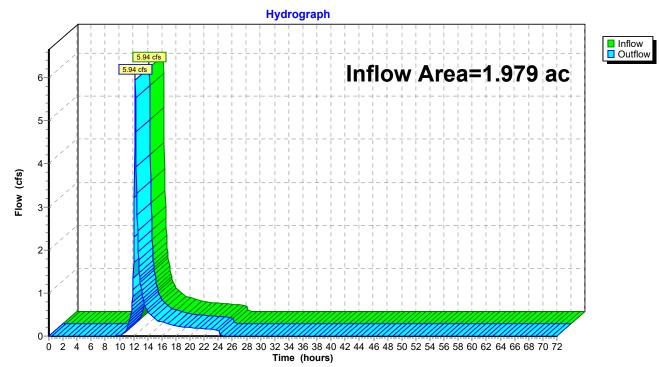
**Reach AP-1: Analysis Point - AP1** 

## Summary for Reach AP-2: Analysis Point - AP2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area	=	1.979 ac,	0.00% Impervious, Inflow	/ Depth = 3.42"	for 100-Year event
Inflow	=	5.94 cfs @	12.25 hrs, Volume=	0.564 af	
Outflow	=	5.94 cfs @	12.25 hrs, Volume=	0.564 af, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



# Reach AP-2: Analysis Point - AP2

## Summary for Pond 1E: Existing Depression

[58] Hint: Peaked 0.26' above defined flood level

Inflow Area =	19.398 ac,	3.33% Impervious, Inflow D	epth = 2.71" for 100-Year event
Inflow =	26.44 cfs @	12.61 hrs, Volume=	4.387 af
Outflow =	21.89 cfs @	12.85 hrs, Volume=	4.387 af, Atten= 17%, Lag= 14.2 min
Discarded =	2.20 cfs @	12.85 hrs, Volume=	2.453 af
Primary =	19.70 cfs @	12.85 hrs, Volume=	1.933 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 309.46'@ 12.85 hrs Surf.Area= 30,032 sf Storage= 37,263 cf Flood Elev= 309.20' Surf.Area= 30,032 sf Storage= 29,481 cf

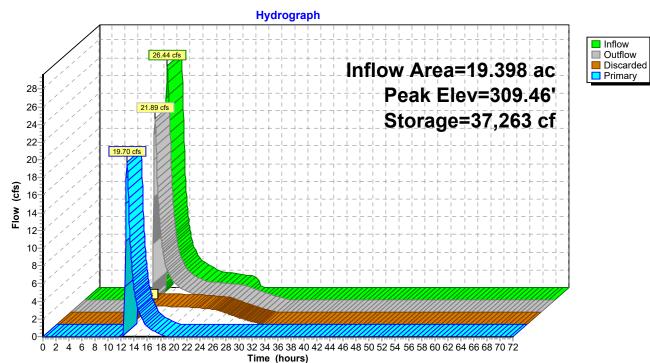
Plug-Flow detention time= 111.2 min calculated for 4.384 af (100% of inflow) Center-of-Mass det. time= 111.4 min (1,022.5 - 911.2)

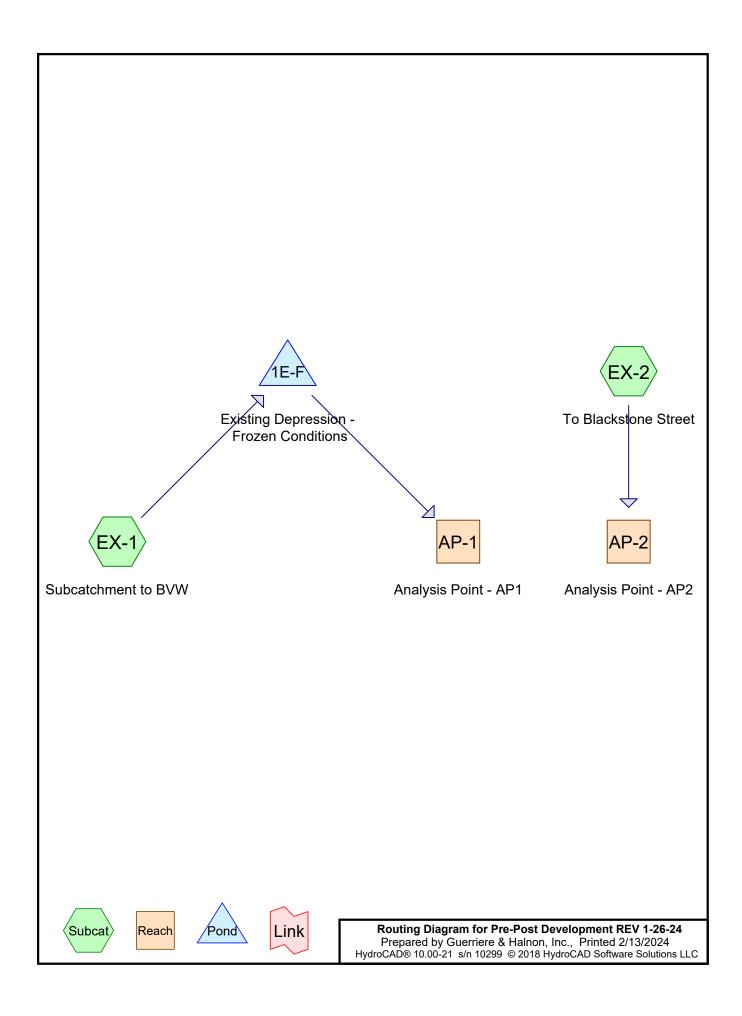
Volume	Invert	Avail.Sto	rage Storage	Description	
#1	307.30	53,50	07 cf Custom	Stage Data (P	rismatic)Listed below (Recalc)
<b>-</b> 1		<b>E A</b>		0	
Elevatio		urf.Area	Inc.Store	Cum.Store	
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)	
307.3	30	48	0	0	
308.0	00	11,143	3,917	3,917	
309.0	)0	28,160	19,652	23,568	
309.1	0	30,032	2,910	26,478	
310.0	00	30,032	27,029	53,507	
Device	Routing	Invert	Outlet Device	S	
#1	Discarded	307.30'	2.410 in/hr E	xfiltration over	Surface area
			Conductivity t	o Groundwater	Elevation = 304.00' Phase-In= 0.01'
#2	Primary	309.05'			oad-Crested Rectangular Weir
	5				0.80 1.00 1.20 1.40 1.60 1.80 2.00
			( )	50 4.00 4.50 5	
			Coef. (Enalish	n) 2.34 2.50 2.	70 2.68 2.68 2.66 2.65 2.65 2.65
				66 2.68 2.70 2	
			-	-	

**Discarded OutFlow** Max=2.20 cfs @ 12.85 hrs HW=309.46' (Free Discharge) **1=Exfiltration** (Controls 2.20 cfs)

Primary OutFlow Max=19.70 cfs @ 12.85 hrs HW=309.46' TW=0.00' (Dynamic Tailwater) ←2=Broad-Crested Rectangular Weir (Weir Controls 19.70 cfs @ 1.60 fps) Prepared by Guerriere & Halnon, Inc. HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD Software Solutions LLC

Pond 1E: Existing Depression





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## Area Listing (selected nodes)

Area	CN	Description
(acres)		(subcatchment-numbers)
3.753	39	>75% Grass cover, Good, HSG A (EX-1, EX-2)
0.860	61	>75% Grass cover, Good, HSG B (EX-1, EX-2)
0.646	98	Water Surface, HSG A (EX-1)
2.399	30	Woods, Good, HSG A (EX-1, EX-2)
13.720	55	Woods, Good, HSG B (EX-1, EX-2)
21.377	51	TOTAL AREA

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## Soil Listing (selected nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
6.798	HSG A	EX-1, EX-2
14.579	HSG B	EX-1, EX-2
0.000	HSG C	
0.000	HSG D	
0.000	Other	
21.377		TOTAL AREA

# Pre-Post Development REV 1-26-24

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 HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
 3.753	0.860	0.000	0.000	0.000	4.612	>75% Grass cover, Good	EX-1,
							EX-2
0.646	0.000	0.000	0.000	0.000	0.646	Water Surface	EX-1
2.399	13.720	0.000	0.000	0.000	16.119	Woods, Good	EX-1,
							EX-2
6.798	14.579	0.000	0.000	0.000	21.377	TOTAL AREA	

# Ground Covers (selected nodes)

<b>Pre-Post Development REV 1-26-24</b> Prepared by Guerriere & Halnon, Inc. <u>HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD Software Solut</u>	NRCC 24-hr C 25-Year Rainfall=6.15" Printed 2/13/2024 ions LLC Page 5
Time span=0.00-72.00 hrs, dt=0.05 Runoff by SCS TR-20 method, UH=S Reach routing by Dyn-Stor-Ind method - Pond ro	CS, Weighted-CN
	97 sf  3.33% Impervious  Runoff Depth=1.22" 41.8 min  CN=50  Runoff=10.15 cfs  1.968 af
	06 sf 0.00% Impervious Runoff Depth=1.69" =15.6 min CN=56 Runoff=2.74 cfs 0.278 af
Reach AP-1: Analysis Point - AP1	Inflow=4.38 cfs 1.394 af Outflow=4.38 cfs 1.394 af
Reach AP-2: Analysis Point - AP2	Inflow=2.74 cfs 0.278 af Outflow=2.74 cfs 0.278 af
Pond 1E-F: Existing Depression - Frozen Peak Elev=309.21'	Storage=29,702 cf Inflow=10.15 cfs 1.968 af Outflow=4.38 cfs 1.394 af
Total Runoff Area = 21.377 ac   Runoff Volum 96.98% Pervious :	<b>v</b> .

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## Summary for Subcatchment EX-1: Subcatchment to BVW

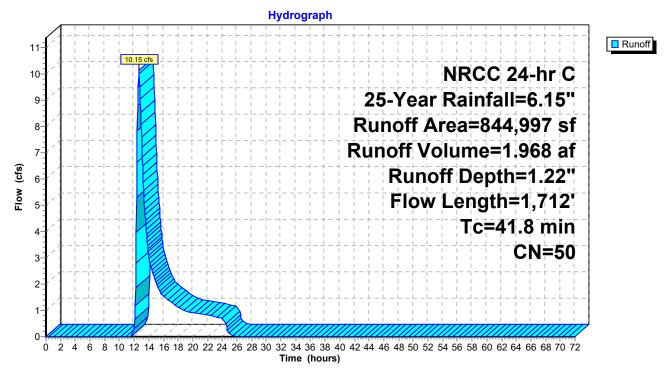
Runoff = 10.15 cfs @ 12.67 hrs, Volume= 1.968 af, Depth= 1.22"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 25-Year Rainfall=6.15"

_	A	rea (sf)	CN [	Description		
528,369 55 Woods, Good, HSG B					od, HSG B	
20,766 61 >75% Grass cover, Goo					s cover, Go	bod, HSG B
163,331 39 >75% Grass cover, Goo					,	,
104,370 30 Woods, Good, HSG A					,	
		28,161	98 \	Nater Surfa	ace, HSG A	l
		44,997		Neighted A		
		16,836	-		rvious Area	
		28,161	3	3.33% Impe	ervious Are	а
	-				0	
	Tc	Length	Slope		Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	7.0	50	0.0800	0.12		Sheet Flow, Segment A-B
		70				Woods: Light underbrush n= 0.400 P2= 3.26"
	0.9	78	0.0800	1.41		Shallow Concentrated Flow, Segment B-C
	40 7	500	0 00 40	0.77		Woodland Kv= 5.0 fps
	12.7	592	0.0240	0.77		Shallow Concentrated Flow, Segment C-D
	111	E01	0.0100	0.60		Woodland Kv= 5.0 fps
	14.1	581	0.0190	0.69		Shallow Concentrated Flow, Segment D-E Woodland Kv= 5.0 fps
	7.1	411	0.0190	0.96		Shallow Concentrated Flow, Segment E-F
	1.1	411	0.0190	0.90		Short Grass Pasture Kv= 7.0 fps
_	41.8	1 712	Total			

41.8 1,712 Total

# Subcatchment EX-1: Subcatchment to BVW



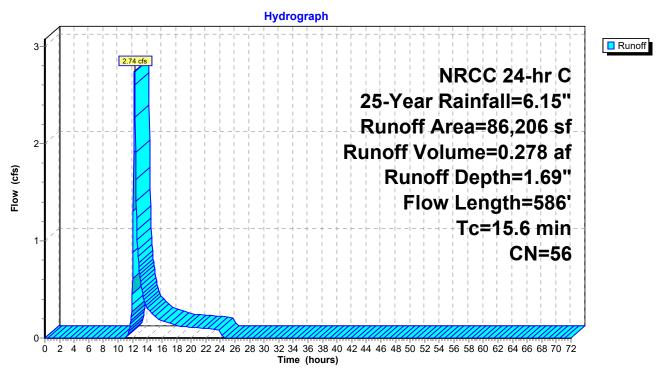
## Summary for Subcatchment EX-2: To Blackstone Street

Runoff = 2.74 cfs @ 12.26 hrs, Volume= 0.278 af, Depth= 1.69"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 25-Year Rainfall=6.15"

A	rea (sf)	CN	Description						
	69,268	55	55 Woods, Good, HSG B						
	16,676	61	>75% Gras	s cover, Go	bod, HSG B				
	131		>75% Grass cover, Good, HSG A						
	131	30	Woods, Go	od, HSG A					
	86,206		Weighted A						
	86,206		100.00% Pe	ervious Are	a				
Tc	Length	Slope		Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
7.8	50	0.0610	0.11		Sheet Flow, Segment A-B				
					Woods: Light underbrush n= 0.400 P2= 3.26"				
2.8	215	0.0640	1.26		Shallow Concentrated Flow, Segment B-C				
					Woodland Kv= 5.0 fps				
2.2	103	0.0240	0.77		Shallow Concentrated Flow, Segment C-D				
					Woodland Kv= 5.0 fps				
2.8	218	0.0340	1.29		Shallow Concentrated Flow, Segment D-E				
					Short Grass Pasture Kv= 7.0 fps				
15.6	586	Total							

### Subcatchment EX-2: To Blackstone Street

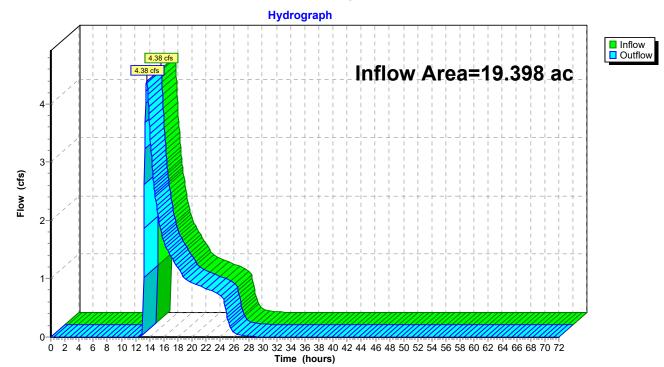


## Summary for Reach AP-1: Analysis Point - AP1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =	19.398 ac,	3.33% Impervious, Inflow	Depth = 0.86"	for 25-Year event
Inflow =	4.38 cfs @	13.57 hrs, Volume=	1.394 af	
Outflow =	4.38 cfs @	13.57 hrs, Volume=	1.394 af, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



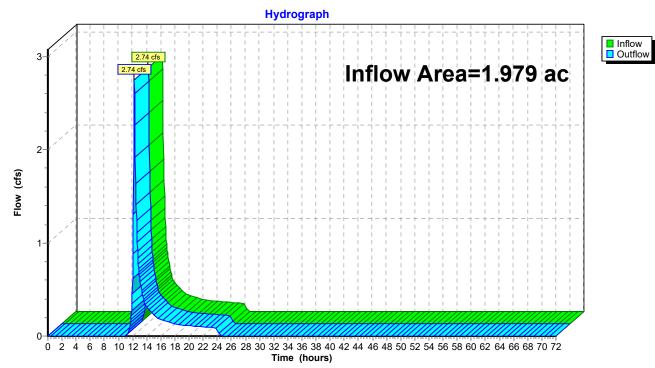
## Reach AP-1: Analysis Point - AP1

## Summary for Reach AP-2: Analysis Point - AP2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area	a =	1.979 ac,	0.00% Impervious,	Inflow Depth = 1.6	9" for 25-Year event
Inflow	=	2.74 cfs @	12.26 hrs, Volume	e= 0.278 af	
Outflow	=	2.74 cfs @	12.26 hrs, Volume	e= 0.278 af, .	Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



# Reach AP-2: Analysis Point - AP2

## Summary for Pond 1E-F: Existing Depression - Frozen Conditions

[58] Hint: Peaked 0.01' above defined flood level

Inflow Area =	19.398 ac,	3.33% Impervious, In	flow Depth = 1.22" for 25-Year event
Inflow =	10.15 cfs @	12.67 hrs, Volume=	1.968 af
Outflow =	4.38 cfs @	13.57 hrs, Volume=	1.394 af, Atten= 57%, Lag= 54.0 min
Primary =	4.38 cfs @	13.57 hrs, Volume=	1.394 af

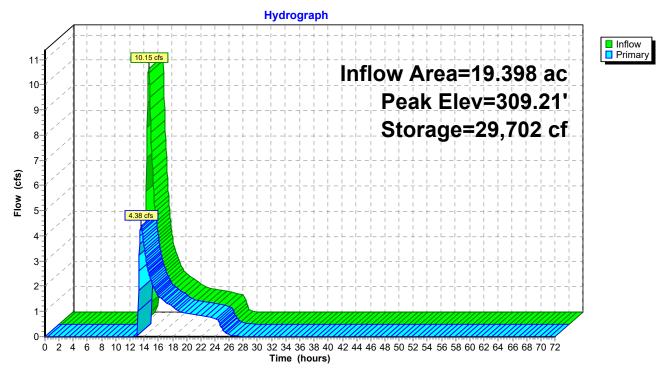
Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 309.21'@ 13.57 hrs Surf.Area= 30,032 sf Storage= 29,702 cf Flood Elev= 309.20' Surf.Area= 30,032 sf Storage= 29,481 cf

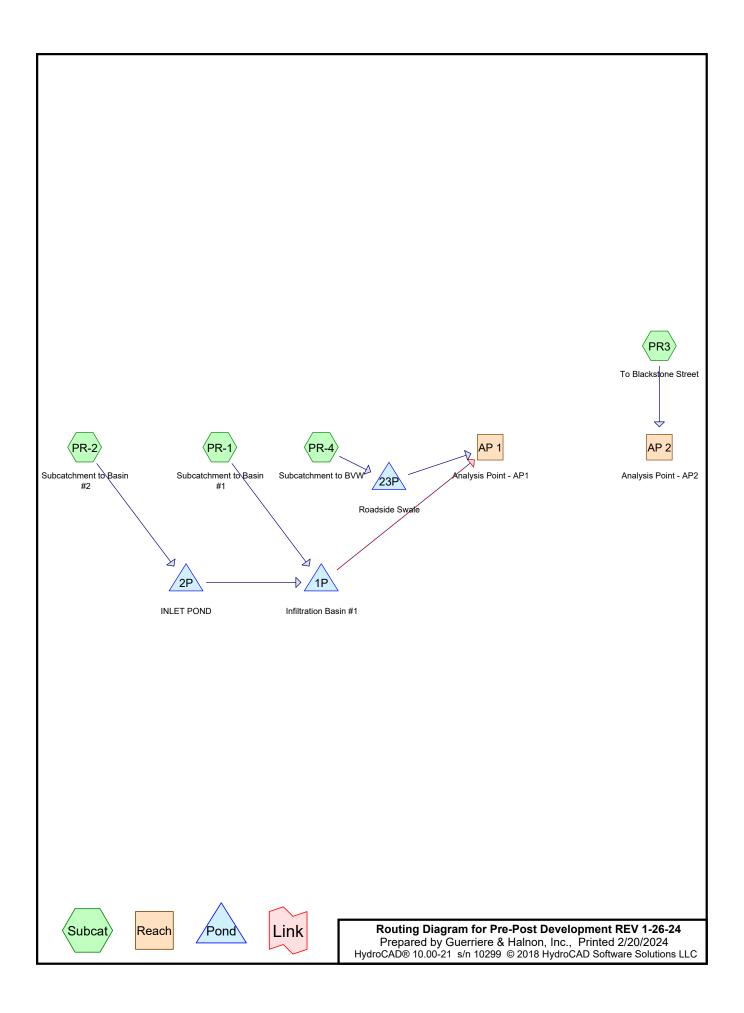
Plug-Flow detention time= 216.6 min calculated for 1.393 af (71% of inflow) Center-of-Mass det. time= 100.4 min (1,041.3 - 941.0)

Volume	Inve	ert Avail.Sto	orage Storage D	escription		
#1	307.3	30' 53,5	07 cf Custom S	cf Custom Stage Data (Prismatic)Listed below (Recalc)		
Elevation (feet)		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)		
307.30	)	48	0	0		
308.00	)	11,143	3,917	3,917		
309.00	)	28,160	19,652	23,568		
309.10	)	30,032	2,910	26,478		
310.00	)	30,032	27,029	53,507		
Device I	Routing	Invert	Outlet Devices			
#1 I	Primary	309.05'	30.0' long x 5.	0' breadth Br	oad-Crested Rectangular Weir	
			Head (feet) 0.2	0 0.40 0.60	0.80 1.00 1.20 1.40 1.60 1.80 2.00	
			2.50 3.00 3.50	4.00 4.50 5	5.00 5.50	
			Coef. (English)	2.34 2.50 2.	70 2.68 2.68 2.66 2.65 2.65 2.65	
			2.65 2.67 2.66	2.68 2.70 2	2.74 2.79 2.88	

Primary OutFlow Max=4.38 cfs @ 13.57 hrs HW=309.21' TW=0.00' (Dynamic Tailwater) **1=Broad-Crested Rectangular Weir** (Weir Controls 4.38 cfs @ 0.93 fps)

# Pond 1E-F: Existing Depression - Frozen Conditions





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## Area Listing (selected nodes)

Area	CN	Description	
(acres)		(subcatchment-numbers)	
2.918	39	>75% Grass cover, Good, HSG A (PR-1, PR-2, PR-4)	
0.786	61	>75% Grass cover, Good, HSG B (PR-2, PR3)	
0.874	98	Paved roads w/curbs & sewers (PR-1)	
0.443	98	Roofs (PR-1)	
0.474	98	Water Surface, HSG A (PR-1)	
2.222	30	Woods, Good, HSG A (PR-2)	
13.663	55	Woods, Good, HSG B (PR-2, PR3)	
21.378	54	TOTAL AREA	

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# Soil Listing (selected nodes)

Soil	Subcatchment
Group	Numbers
HSG A	PR-1, PR-2, PR-4
HSG B	PR-2, PR3
HSG C	
HSG D	
Other	PR-1
	TOTAL AREA
	Group HSG A HSG B HSG C HSG D

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HSG-A	HSG-B	HSG-C	HSG-D	Other	Total	Ground	Subcatchment
 (acres)	(acres)	(acres)	(acres)	(acres)	(acres)	Cover	Numbers
2.918	0.786	0.000	0.000	0.000	3.703	>75% Grass cover, Good	PR
							-1,
							PR
							-2,
							PR
							-4,
							PR
							3
0.000	0.000	0.000	0.000	0.874	0.874	Paved roads w/curbs & sewers	PR
							-1
0.000	0.000	0.000	0.000	0.443	0.443	Roofs	PR
							-1
0.474	0.000	0.000	0.000	0.000	0.474	Water Surface	PR
							-1
2.222	13.663	0.000	0.000	0.000	15.884	Woods, Good	PR
							-2,
							PR
							3
5.613	14.448	0.000	0.000	1.317	21.378	TOTAL AREA	

# Ground Covers (selected nodes)

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Line#	Node Number	In-Invert (feet)	Out-Invert (feet)	Length (feet)	Slope (ft/ft)	n	Diam/Width (inches)	Height (inches)	Inside-Fill (inches)
 1	PR-2	0.00	0.00	312.0	0.0230	0.013	24.0	0.0	0.0
2	PR-4	0.00	0.00	47.0	0.0050	0.011	12.0	0.0	0.0
3	1P	306.00	305.53	94.2	0.0050	0.011	24.0	0.0	0.0
4	2P	310.60	307.00	363.4	0.0099	0.013	24.0	0.0	0.0

# Pipe Listing (selected nodes)

Pre-Post Development REV 1-26-24 Prepared by Guerriere & Halnon, Inc. HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD Softwa	NRCC 24-hr C 2-Year Rainfall=3.26" Printed 2/20/2024 are Solutions LLC Page 6
Time span=0.00-72.00 hrs, o Runoff by SCS TR-20 method Reach routing by Dyn-Stor-Ind method -	, UH=SCS, Weighted-CN
SubcatchmentPR-1: Subcatchmentto Runoff Area	=141,517 sf 55.11% Impervious Runoff Depth=0.97" Tc=6.0 min CN=72 Runoff=3.71 cfs 0.262 af
	a=670,872 sf 0.00% Impervious Runoff Depth=0.16" 673' Tc=37.2 min CN=51 Runoff=0.42 cfs 0.210 af
SubcatchmentPR-4: Subcatchmentto BVW Runoff Are Flow Length=5	ea=33,131 sf 0.00% Impervious Runoff Depth=0.00" 544' Tc=10.6 min CN=39 Runoff=0.00 cfs 0.000 af
	ea=85,707 sf 0.00% Impervious Runoff Depth=0.30" 572' Tc=15.5 min CN=56 Runoff=0.21 cfs 0.049 af
Reach AP 1: Analysis Point - AP1	Inflow=0.00 cfs 0.000 af Outflow=0.00 cfs 0.000 af
Reach AP 2: Analysis Point - AP2	Inflow=0.21 cfs 0.049 af Outflow=0.21 cfs 0.049 af
Pond 1P: Infiltration Basin #1Peak Eviscarded=2.07 cfs0.472 afPrimary=0.00 cfs0.000 afSec	lev=305.57' Storage=715 cf Inflow=3.71 cfs 0.472 af condary=0.00 cfs 0.000 af Outflow=2.07 cfs 0.472 af
	Elev=312.00' Storage=0 cf Inflow=0.42 cfs 0.210 af Primary=0.42 cfs 0.210 af Outflow=0.42 cfs 0.210 af
	Elev=306.01' Storage=0 cf Inflow=0.00 cfs 0.000 af Primary=0.00 cfs 0.000 af Outflow=0.00 cfs 0.000 af
	f Volume = 0.521 af Average Runoff Depth = 0.29 rvious = 19.588 ac 8.38% Impervious = 1.790 ac

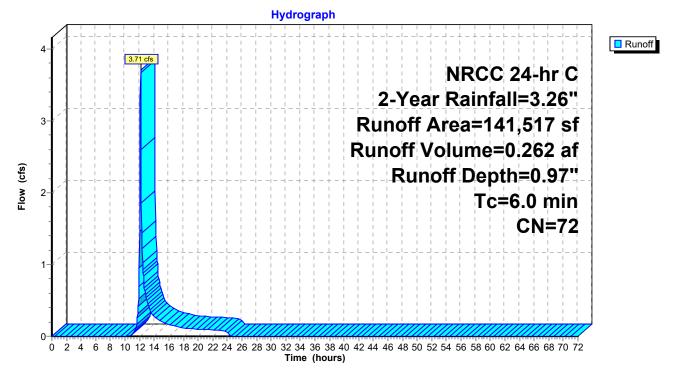
#### Summary for Subcatchment PR-1: Subcatchment to Basin #1

Runoff = 3.71 cfs @ 12.14 hrs, Volume= 0.262 af, Depth= 0.97"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 2-Year Rainfall=3.26"

_	Area (s	f) CN	Description				
*	38,06	98 26	Paved road	ls w/curbs a	& sewers		
*	19,29	98 36	Roofs				
	63,52	24 39	>75% Gras	>75% Grass cover, Good, HSG A			
*	20,63	88 98	Water Surfa	ace, HSG A	Α		
	141,51	7 72	Weighted A	verage			
	63,52	24	44.89% Pe	44.89% Pervious Area			
	77,99	)3	55.11% lm	55.11% Impervious Area			
	Tc Leng			Capacity			
_	(min) (fe	et) (ft	/ft) (ft/sec)	(cfs)			
	6.0				Direct Entry,		

#### Subcatchment PR-1: Subcatchment to Basin #1



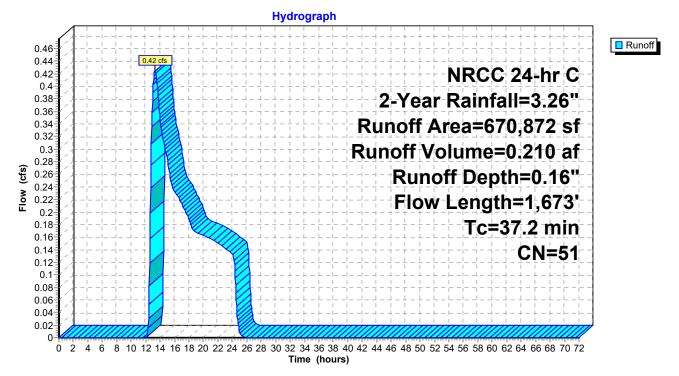
# Summary for Subcatchment PR-2: Subcatchment to Basin #2

Runoff = 0.42 cfs @ 13.29 hrs, Volume= 0.210 af, Depth= 0.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 2-Year Rainfall=3.26"

A	rea (sf)	CN D	escription			
5	27,673	55 V	5 Woods, Good, HSG B			
	96,783	30 V	/oods, Go	od, HSG A		
	15,981	61 >	75% Gras	s cover, Go	bod, HSG B	
	30,435	39 >	75% Gras	s cover, Go	ood, HSG A	
6	70,872	51 V	/eighted A	verage		
6	70,872	1	00.00% Pe	ervious Are	а	
Тс	Length	Slope	Velocity		Description	
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
7.0	50	0.0800	0.12		Sheet Flow, Segment A-B	
					Woods: Light underbrush n= 0.400 P2= 3.26"	
0.9	78	0.0800	1.41		Shallow Concentrated Flow, Segment B-C	
					Woodland Kv= 5.0 fps	
12.7	592	0.0240	0.77		Shallow Concentrated Flow, Segment C-D	
					Woodland Kv= 5.0 fps	
14.1	581	0.0190	0.69		Shallow Concentrated Flow, Segment D-E	
0.0	00	0.0400	0.50		Woodland Kv= 5.0 fps	
2.0	60	0.0100	0.50		Shallow Concentrated Flow, Segment E-F	
0.5	040	0 0000	40.00	04.04	Woodland Kv= 5.0 fps	
0.5	312	0.0230	10.92	34.31	Pipe Channel, Segment F-G	
					24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'	
07.0	4.070	<b></b>			n= 0.013 Concrete pipe, straight & clean	
37.2	1,673	Total				

#### Subcatchment PR-2: Subcatchment to Basin #2



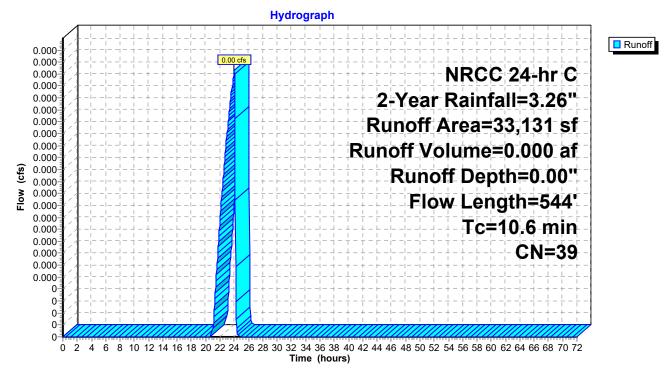
#### Summary for Subcatchment PR-4: Subcatchment to BVW

Runoff = 0.00 cfs @ 24.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 2-Year Rainfall=3.26"

_	A	rea (sf)	CN	Description					
		33,131	39	39 >75% Grass cover, Good, HSG A					
_		33,131		100.00% P	ervious Are	a			
	Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description			
-	5.6	50	0.0200	0.15		Sheet Flow, Segment A-B			
						Grass: Short n= 0.150 P2= 3.26"			
	2.0	194	0.0550	1.64		Shallow Concentrated Flow, Segment B-C			
		<i>.</i> _				Short Grass Pasture Kv= 7.0 fps			
	0.2	47	0.0050	3.79	2.98				
						12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'			
	~ ~ ~	050	0.0400	4 50		n= 0.011 Concrete pipe, straight & clean			
	2.8	253	0.0100	1.50		Shallow Concentrated Flow, Segment D-E Grassed Waterway Kv= 15.0 fps			
-	10.6	511	Total			Glassed Waterway IN- 13.0 lps			
	10.6	544	Total						

#### Subcatchment PR-4: Subcatchment to BVW



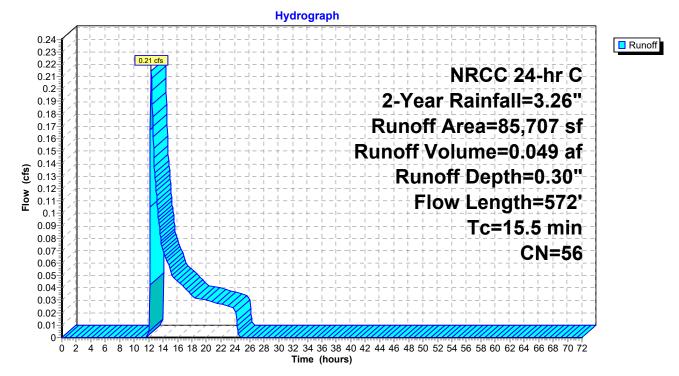
#### Summary for Subcatchment PR3: To Blackstone Street

Runoff = 0.21 cfs @ 12.36 hrs, Volume= 0.049 af, Depth= 0.30"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 2-Year Rainfall=3.26"

Α	rea (sf)	CN D	escription		
	67,471	55 V	Voods, Go	od, HSG B	
	18,236	61 >	75% Gras	s cover, Go	ood, HSG B
	85,707	56 V	Veighted A	verage	
	85,707	1	00.00% Pe	ervious Are	а
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
7.8	50	0.0610	0.11		Sheet Flow, Segment A-B
					Woods: Light underbrush n= 0.400 P2= 3.26"
2.8	215	0.0640	1.26		Shallow Concentrated Flow, Segment B-C
					Woodland Kv= 5.0 fps
2.2	103	0.0240	0.77		Shallow Concentrated Flow, Segment C-D
					Woodland Kv= 5.0 fps
2.7	204	0.0320	1.25		Shallow Concentrated Flow, Segment D-E
					Short Grass Pasture Kv= 7.0 fps
15.5	572	Total			

#### Subcatchment PR3: To Blackstone Street

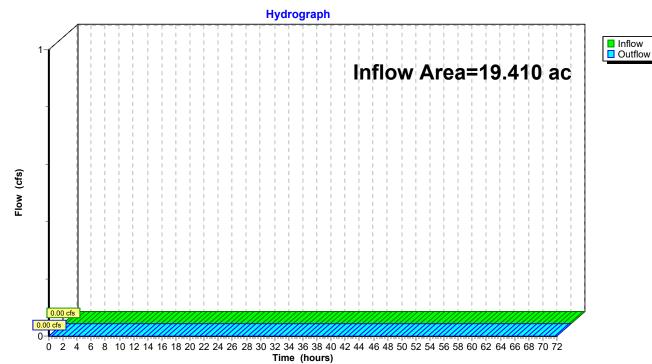


# Summary for Reach AP 1: Analysis Point - AP1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =	19.410 ac,	9.22% Impervious, Inflow	Depth = 0.00"	for 2-Year event
Inflow =	0.00 cfs @	0.00 hrs, Volume=	0.000 af	
Outflow =	0.00 cfs @	0.00 hrs, Volume=	0.000 af, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



# Reach AP 1: Analysis Point - AP1

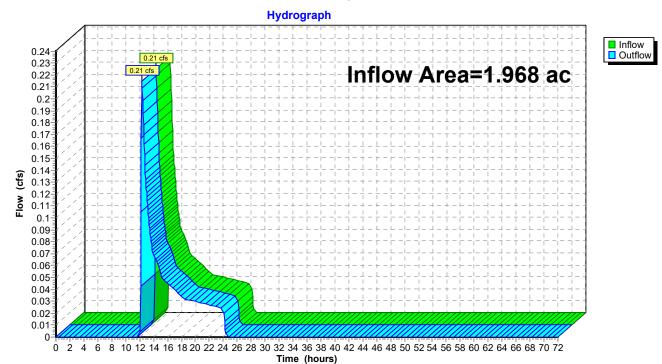
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# Summary for Reach AP 2: Analysis Point - AP2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =	1.968 ac,	0.00% Impervious, Inflow D	Depth = $0.30"$	for 2-Year event
Inflow =	0.21 cfs @	12.36 hrs, Volume=	0.049 af	
Outflow =	0.21 cfs @	12.36 hrs, Volume=	0.049 af, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



# Reach AP 2: Analysis Point - AP2

# Summary for Pond 1P: Infiltration Basin #1

Inflow Area =	18.650 ac,	9.60% Impervious, Inflow	Depth = 0.30" for 2-Year event
Inflow =	3.71 cfs @	12.14 hrs, Volume=	0.472 af
Outflow =	2.07 cfs @	12.24 hrs, Volume=	0.472 af, Atten= 44%, Lag= 6.0 min
Discarded =	2.07 cfs @	12.24 hrs, Volume=	0.472 af
Primary =	0.00 cfs @	0.00 hrs, Volume=	0.000 af
Secondary =	0.00 cfs @	0.00 hrs, Volume=	0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 305.57' @ 12.24 hrs Surf.Area= 10,581 sf Storage= 715 cf Flood Elev= 310.50' Surf.Area= 20,637 sf Storage= 77,211 cf

Plug-Flow detention time= 1.3 min calculated for 0.472 af (100% of inflow) Center-of-Mass det. time= 1.3 min (954.8 - 953.5)

Volume	Invert	Avail.Stor	rage Storage	
#1	305.50'	87,52	29 cf Custom	n Stage Data (Prismatic)Listed below (Recalc)
Elevatio		rf.Area	Inc.Store	Cum.Store
(fee	/	(sq-ft)	(cubic-feet)	(cubic-feet)
305.5		10,451	0	0
306.0		11,407	5,465	5,465
308.0		15,368	26,775	32,240
310.0		19,555	34,923	67,163
310.5		20,637	10,048	77,211
311.0	00	20,637	10,319	87,529
Device	Routing	Invert	Outlet Device	es
#1	Primary	306.00'	24.0" Round	d Culvert
			L= 94.2' RC	CP, groove end w/headwall, Ke= 0.200
			Inlet / Outlet I	Invert= 306.00' / 305.53' S= 0.0050 '/' Cc= 0.900
			n= 0.011 Co	oncrete pipe, straight & clean, Flow Area= 3.14 sf
#2	Device 1	308.55'	48.0" x 48.0"	"Horiz. Orifice/Grate C= 0.600
			Limited to we	eir flow at low heads
#3	Device 1	307.00'	12.0" W x 9.0	0" H Vert. Orifice/Grate C= 0.600
#4	Discarded	305.50'	8.270 in/hr E	Exfiltration over Horizontal area
			Conductivity	to Groundwater Elevation = 302.70' Phase-In= 0.01'
#5	Secondary	309.90'		10.0' breadth Broad-Crested Rectangular Weir
	2		Head (feet) (	0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
				sh) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

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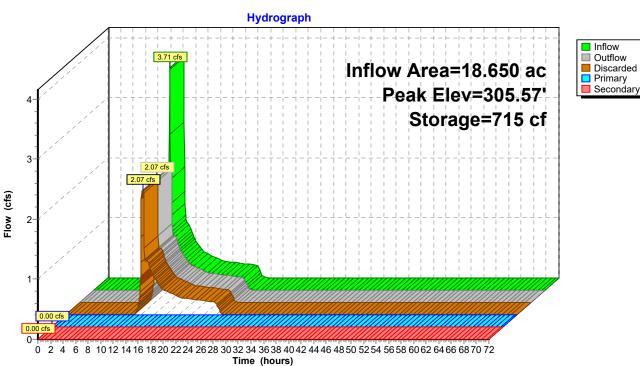
**Discarded OutFlow** Max=2.07 cfs @ 12.24 hrs HW=305.57' (Free Discharge) **4=Exfiltration** (Controls 2.07 cfs)

**Primary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=305.50' TW=0.00' (Dynamic Tailwater)

-2=Orifice/Grate (Controls 0.00 cfs)

**3=Orifice/Grate** (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=305.50' TW=0.00' (Dynamic Tailwater) 5=Broad-Crested Rectangular Weir( Controls 0.00 cfs)



Pond 1P: Infiltration Basin #1

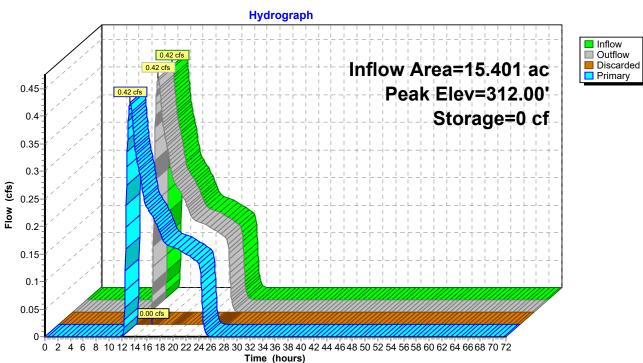
# Summary for Pond 2P: INLET POND

Inflow Ar Inflow Outflow Discarde Primary	= = ed =	0.42 cfs @ 13 0.42 cfs @ 13 0.00 cfs @ 14	00% Impervious 3.29 hrs, Volum 3.29 hrs, Volum 4.47 hrs, Volum 3.29 hrs, Volum	e= 0.2 e= 0.2 e= 0.0	n = 0.16" for 2-Ye 210 af 210 af, Atten= 0%, L 000 af 210 af		
	Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 312.00' @ 0.00 hrs Surf.Area= 1,182 sf Storage= 0 cf						
Center-o	Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 0.0 min(1,043.8 - 1,043.8)						
Volume	Inver		rage Storage D				
#1	312.00	)' 3,48	30 cf Custom	Stage Data (P	rismatic)Listed below	w (Recalc)	
Elevatio (feet		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)			
312.0	/	1,182	0				
313.0	-	1,690	1,436	1,436			
314.0		2,398	2,044	3,480			
Device	Routing	Invert	Outlet Devices	,			
#1	Primary	310.60'	24.0" Round	Culvert			
					e headwall, Ke= 0.50		
					' 307.00' S= 0.0099		
					ids & connections, F	low Area= 3.14 sf	
#2	Discarded	I 312.00'	8.270 in/hr Ex				
			Conductivity to	Groundwater	Elevation = 304.67'	Phase-In= 0.01'	
<b>Bis sended OctEless Marcol 0.00</b> (Fr. O. 44, 47 has 1004, 040,001, (Fr. S. Bissharras)							

**Discarded OutFlow** Max=0.00 cfs @ 14.47 hrs HW=312.00' (Free Discharge) **2=Exfiltration** (Controls 0.00 cfs)

**Primary OutFlow** Max=0.00 cfs @ 13.29 hrs HW=312.00' TW=305.50' (Dynamic Tailwater) **1=Culvert** (Passes 0.00 cfs of 9.46 cfs potential flow)

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# Pond 2P: INLET POND

# Summary for Pond 23P: Roadside Swale

Inflow Area =	0.761 ac,	0.00% Impervious, Inflow De	epth = 0.00" for 2-Year event
Inflow =	0.00 cfs @	24.00 hrs, Volume=	0.000 af
Outflow =	0.00 cfs @	24.00 hrs, Volume=	0.000 af, Atten= 0%, Lag= 0.4 min
Discarded =	0.00 cfs @	24.00 hrs, Volume=	0.000 af
Primary =	0.00 cfs @	0.00 hrs, Volume=	0.000 af

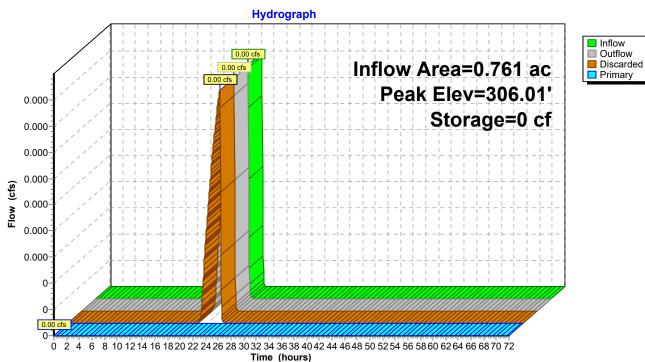
Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 306.01' @ 24.00 hrs Surf.Area= 4 sf Storage= 0 cf

Plug-Flow detention time= 0.4 min calculated for 0.000 af (100% of inflow) Center-of-Mass det. time= 0.4 min (1,382.4 - 1,382.0)

Volume	Invert	Avail.Sto	rage Storage	e Description	
#1	306.00'	1,36	65 cf Custon	n Stage Data (P	rismatic)Listed below (Recalc)
Elevatio (fee		urf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
306.0	00	0	0	0	
307.0	00	700	350	350	
308.0	00	1,330	1,015	1,365	
Device	Routing	Invert	Outlet Device	es	
#1 #2	Discarded Primary	306.00' 307.25'	8.270 in/hr E 10.0' long x Head (feet) ( 2.50 3.00 3.	<b>2.0' breadth Br</b> 0.20 0.40 0.60 50 h) 2.54 2.61 2.	Surface area Phase-In= 0.01' oad-Crested Rectangular Weir 0.80 1.00 1.20 1.40 1.60 1.80 2.00 61 2.60 2.66 2.70 2.77 2.89 2.88
Disconded QuitFlow May-0.00 of @ 24.00 km UN/-200 041 (Erec Discharge)					

**Discarded OutFlow** Max=0.00 cfs @ 24.00 hrs HW=306.01' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.00 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=306.00' TW=0.00' (Dynamic Tailwater) 2=Broad-Crested Rectangular Weir( Controls 0.00 cfs)



# Pond 23P: Roadside Swale

Pre-Post Development REV 1-26- Prepared by Guerriere & Halnon, Inc. HydroCAD® 10.00-21 s/n 10299 © 2018 Hy			C 10-Year Rainfall=4.88" Printed 2/20/2024 Page 20
		=SCS, Weighted-Cl	
SubcatchmentPR-1: Subcatchmentto	Runoff Area=141,		ervious Runoff Depth=2.11" 2 Runoff=8.38 cfs 0.570 af
SubcatchmentPR-2: Subcatchmentto			ervious Runoff Depth=0.70" 1 Runoff=4.09 cfs 0.894 af
SubcatchmentPR-4: Subcatchmentto I			ervious Runoff Depth=0.18" 9 Runoff=0.02 cfs 0.011 af
SubcatchmentPR3: To Blackstone Stre			ervious Runoff Depth=0.98" 6 Runoff=1.42 cfs 0.161 af
Reach AP 1: Analysis Point - AP1			Inflow=0.00 cfs 0.000 af Outflow=0.00 cfs 0.000 af
Reach AP 2: Analysis Point - AP2			Inflow=1.42 cfs 0.161 af Outflow=1.42 cfs 0.161 af
<b>Pond 1P: Infiltration Basin #1</b> Discarded=3.07 cfs 1.464 af Primary=0.00 cfs		0	cf Inflow=8.58 cfs 1.464 af Outflow=3.07 cfs 1.464 af
Pond 2P: INLET POND Discarded=0.00			cf Inflow=4.09 cfs 0.894 af Outflow=4.09 cfs 0.894 af
Pond 23P: Roadside Swale Discarded=0.02			cf Inflow=0.02 cfs 0.011 af Outflow=0.02 cfs 0.011 af
Total Runoff Area = 21.3	78 ac Runoff Vol 91.62% Perviou		verage Runoff Depth = 0.92" 38% Impervious = 1.790 ac

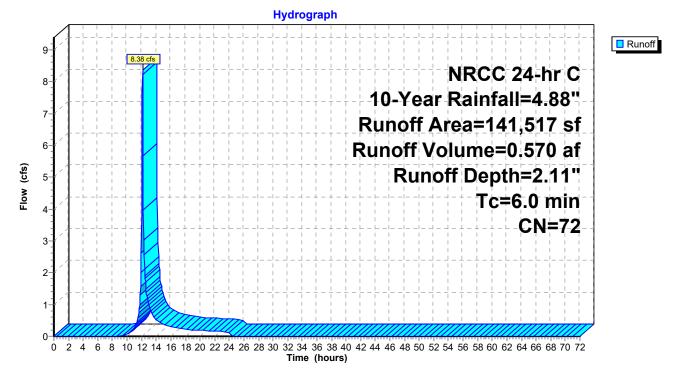
#### Summary for Subcatchment PR-1: Subcatchment to Basin #1

Runoff = 8.38 cfs @ 12.13 hrs, Volume= 0.570 af, Depth= 2.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 10-Year Rainfall=4.88"

	Area (sf)	CN	Description		
*	38,062	98	Paved road	s w/curbs a	& sewers
*	19,293	98	Roofs		
	63,524	39	>75% Gras	s cover, Go	lood, HSG A
*	20,638	98	Water Surfa	ace, HSG A	Α
	141,517	72	Weighted A	verage	
	63,524		44.89% Per	vious Area	a
	77,993		55.11% lmp	pervious Ar	rea
	Tc Length			Capacity	•
(	min) (feet)	(ft/1	ft) (ft/sec)	(cfs)	
	6.0				Direct Entry,

#### Subcatchment PR-1: Subcatchment to Basin #1



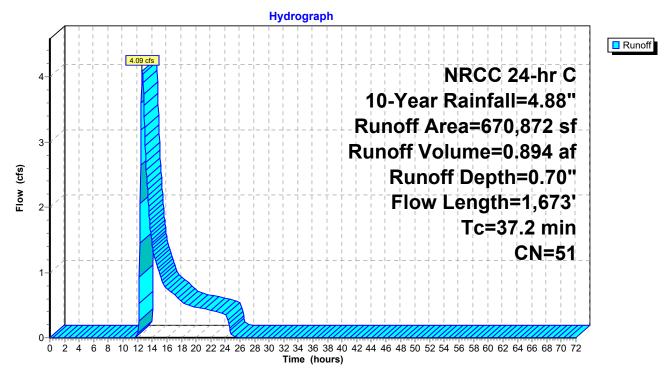
# Summary for Subcatchment PR-2: Subcatchment to Basin #2

Runoff = 4.09 cfs @ 12.65 hrs, Volume= 0.894 af, Depth= 0.70"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 10-Year Rainfall=4.88"

A	rea (sf)	CN D	escription				
5	27,673	55 V	55 Woods, Good, HSG B				
	96,783	30 V	/oods, Go	od, HSG A			
	15,981	61 >	75% Gras	s cover, Go	bod, HSG B		
	30,435	39 >	75% Gras	s cover, Go	ood, HSG A		
6	70,872	51 V	/eighted A	verage			
6	70,872	1	00.00% Pe	ervious Are	а		
Тс	Length	Slope	Velocity		Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
7.0	50	0.0800	0.12		Sheet Flow, Segment A-B		
					Woods: Light underbrush n= 0.400 P2= 3.26"		
0.9	78	0.0800	1.41		Shallow Concentrated Flow, Segment B-C		
					Woodland Kv= 5.0 fps		
12.7	592	0.0240	0.77		Shallow Concentrated Flow, Segment C-D		
					Woodland Kv= 5.0 fps		
14.1	581	0.0190	0.69		Shallow Concentrated Flow, Segment D-E		
0.0	00	0.0400	0.50		Woodland Kv= 5.0 fps		
2.0	60	0.0100	0.50		Shallow Concentrated Flow, Segment E-F		
0.5	040	0 0000	40.00	04.04	Woodland Kv= 5.0 fps		
0.5	312	0.0230	10.92	34.31	Pipe Channel, Segment F-G		
					24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'		
07.0	4.070	<b></b>			n= 0.013 Concrete pipe, straight & clean		
37.2	1,673	Total					

# Subcatchment PR-2: Subcatchment to Basin #2



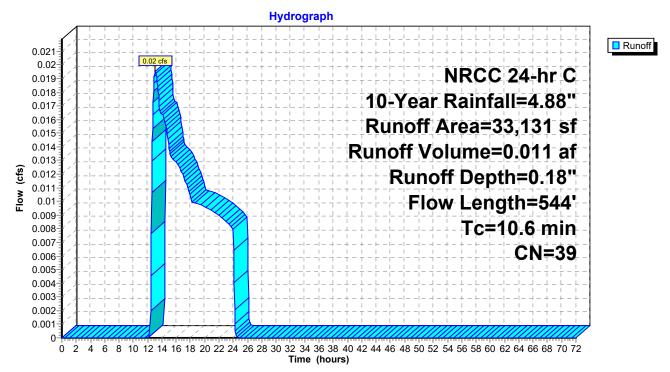
#### Summary for Subcatchment PR-4: Subcatchment to BVW

Runoff = 0.02 cfs @ 13.06 hrs, Volume= 0.011 af, Depth= 0.18"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 10-Year Rainfall=4.88"

_	A	rea (sf)	CN	Description					
		33,131	39	39 >75% Grass cover, Good, HSG A					
_		33,131		100.00% P	ervious Are	a			
	Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description			
-	5.6	50	0.0200	0.15		Sheet Flow, Segment A-B			
						Grass: Short n= 0.150 P2= 3.26"			
	2.0	194	0.0550	1.64		Shallow Concentrated Flow, Segment B-C			
						Short Grass Pasture Kv= 7.0 fps			
	0.2	47	0.0050	3.79	2.98				
						12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'			
	~ ~ ~	050	0.0400	4 50		n= 0.011 Concrete pipe, straight & clean			
	2.8	253	0.0100	1.50		Shallow Concentrated Flow, Segment D-E Grassed Waterway Kv= 15.0 fps			
-	10.6	511	Total			Glassed Waterway IN- 13.0 lps			
	10.6	544	Total						

#### Subcatchment PR-4: Subcatchment to BVW



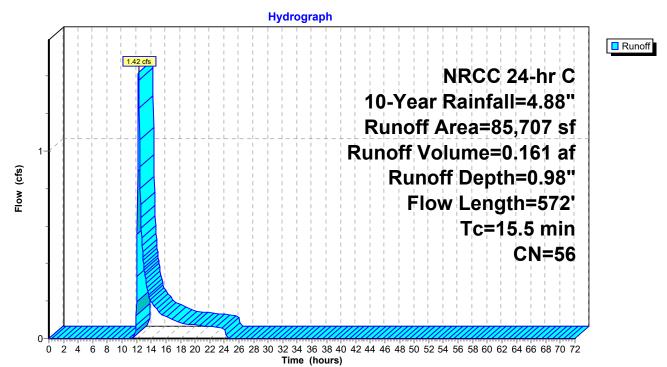
#### Summary for Subcatchment PR3: To Blackstone Street

Runoff = 1.42 cfs @ 12.27 hrs, Volume= 0.161 af, Depth= 0.98"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 10-Year Rainfall=4.88"

A	rea (sf)	CN D	escription		
	67,471	55 V	loods, Go	od, HSG B	
	18,236	61 >	75% Gras	s cover, Go	ood, HSG B
	85,707	56 V	Veighted A	verage	
	85,707	1	00.00% Pe	ervious Are	а
Tc	Length	Slope	Velocity	Capacity	Description
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)	
7.8	50	0.0610	0.11		Sheet Flow, Segment A-B
					Woods: Light underbrush n= 0.400 P2= 3.26"
2.8	215	0.0640	1.26		Shallow Concentrated Flow, Segment B-C
					Woodland Kv= 5.0 fps
2.2	103	0.0240	0.77		Shallow Concentrated Flow, Segment C-D
					Woodland Kv= 5.0 fps
2.7	204	0.0320	1.25		Shallow Concentrated Flow, Segment D-E
					Short Grass Pasture Kv= 7.0 fps
15.5	572	Total			

#### Subcatchment PR3: To Blackstone Street



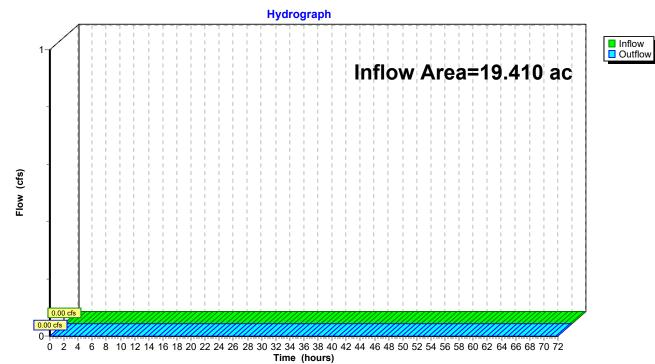
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# Summary for Reach AP 1: Analysis Point - AP1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =	19.410 ac,	9.22% Impervious, Int	flow Depth = 0.00"	for 10-Year event
Inflow =	0.00 cfs @	0.00 hrs, Volume=	0.000 af	
Outflow =	0.00 cfs @	0.00 hrs, Volume=	0.000 af, Att	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



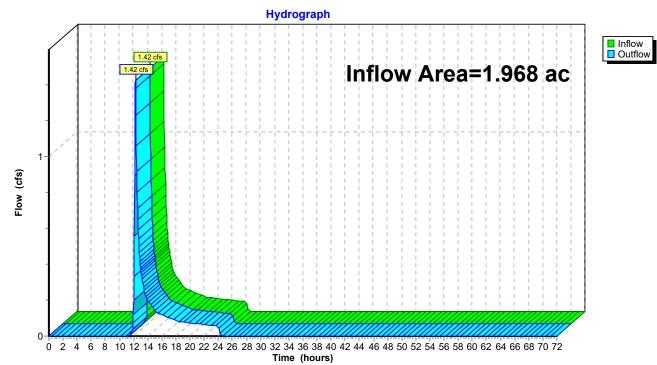
# Reach AP 1: Analysis Point - AP1

# Summary for Reach AP 2: Analysis Point - AP2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =	1.968 ac,	0.00% Impervious, Inflow D	epth = 0.98"	for 10-Year event
Inflow =	1.42 cfs @	12.27 hrs, Volume=	0.161 af	
Outflow =	1.42 cfs @	12.27 hrs, Volume=	0.161 af, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



# Reach AP 2: Analysis Point - AP2

# Summary for Pond 1P: Infiltration Basin #1

Inflow Area =	18.650 ac,	9.60% Impervious, Infl	ow Depth = 0.94" for 10-Year event
Inflow =	8.58 cfs @	12.14 hrs, Volume=	1.464 af
Outflow =	3.07 cfs @	13.33 hrs, Volume=	1.464 af, Atten= 64%, Lag= 71.5 min
Discarded =	3.07 cfs @	13.33 hrs, Volume=	1.464 af
Primary =	0.00 cfs @	0.00 hrs, Volume=	0.000 af
Secondary =	0.00 cfs @	0.00 hrs, Volume=	0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 306.44' @ 13.33 hrs Surf.Area= 12,280 sf Storage= 10,684 cf Flood Elev= 310.50' Surf.Area= 20,637 sf Storage= 77,211 cf

Plug-Flow detention time= 25.6 min calculated for 1.463 af (100% of inflow) Center-of-Mass det. time= 25.6 min (944.3 - 918.7)

Volume	Invert	Avail.Stor	rage Storage	e Description
#1	305.50'	87,52	29 cf Custom	n Stage Data (Prismatic)Listed below (Recalc)
Elevatio		uf Aug a	Inc. Ctore	Curre Chare
Elevatio (fee		rf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
305.5	/	<u>(34-11)</u> 10,451	0	0
306.0		11,407	5,465	5,465
308.0		15,368	26,775	32,240
310.0		19,555	34,923	67,163
310.5		20,637	10,048	77,211
311.0	00	20,637	10,319	87,529
Device	Routing	Invert	Outlet Device	es
#1	Primary	306.00'	24.0" Round	d Culvert
				P, groove end w/headwall, Ke= 0.200
				Invert= 306.00' / 305.53' S= 0.0050 '/' Cc= 0.900
	During			ncrete pipe, straight & clean, Flow Area= 3.14 sf
#2	Device 1	308.55'		<b>' Horiz. Orifice/Grate</b> C= 0.600 Fir flow at low heads
#3	Device 1	307.00'		0" H Vert. Orifice/Grate C= 0.600
#0 #4	Discarded	305.50'		Exfiltration over Horizontal area
				to Groundwater Elevation = 302.70' Phase-In= 0.01'
#5	Secondary	309.90'	30.0' long x	10.0' breadth Broad-Crested Rectangular Weir
				0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (Englisl	h) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

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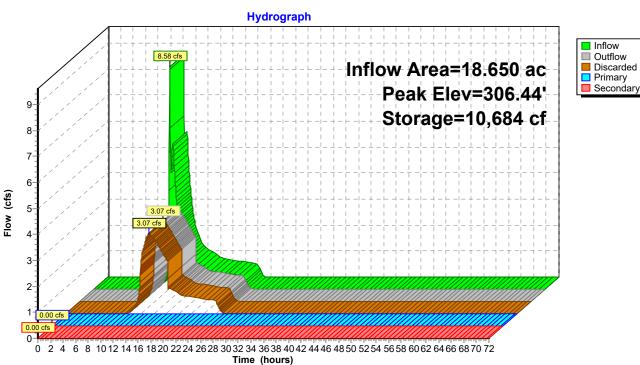
**Discarded OutFlow** Max=3.07 cfs @ 13.33 hrs HW=306.44' (Free Discharge) **4=Exfiltration** (Controls 3.07 cfs)

**Primary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=305.50' TW=0.00' (Dynamic Tailwater)

**2=Orifice/Grate** (Controls 0.00 cfs)

-3=Orifice/Grate (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=305.50' TW=0.00' (Dynamic Tailwater) 5=Broad-Crested Rectangular Weir( Controls 0.00 cfs)



Pond 1P: Infiltration Basin #1

# Summary for Pond 2P: INLET POND

Inflow Area =	15.401 ac,	0.00% Impervious, Inflow De	epth = 0.70" for 10-Year event
Inflow =	4.09 cfs @	12.65 hrs, Volume=	0.894 af
Outflow =	4.09 cfs @	12.65 hrs, Volume=	0.894 af, Atten= 0%, Lag= 0.0 min
Discarded =	0.00 cfs @	24.91 hrs, Volume=	0.000 af
Primary =	4.09 cfs @	12.65 hrs, Volume=	0.894 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 312.00' @ 12.65 hrs Surf.Area= 1,182 sf Storage= 0 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 0.0 min (959.3 - 959.3)

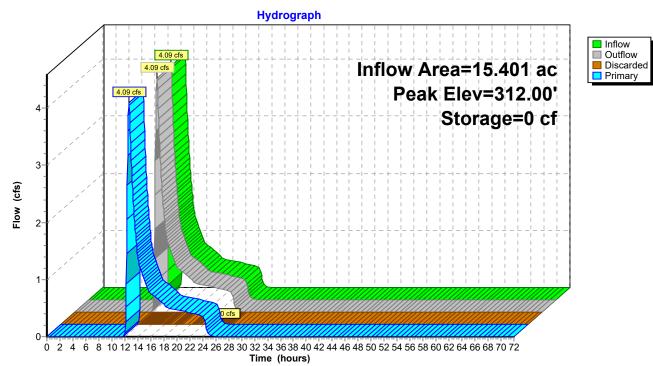
Volume	Invert	Avail.Sto	rage Storage	Description	
#1	312.00'	3,48	30 cf Custom	Stage Data (P	rismatic)Listed below (Recalc)
Elevatio	on Su	ırf.Area	Inc.Store	Cum.Store	
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)	
312.0	312.00 1,182		0	0	
313.0	313.00 1,690		1,436	1,436	
314.00		2,398	2,044	3,480	
Device	Routing	Invert	Outlet Device	S	
#1	Primary	310.60'	<ul> <li>24.0" Round Culvert</li> <li>L= 363.4' RCP, square edge headwall, Ke= 0</li> <li>Inlet / Outlet Invert= 310.60' / 307.00' S= 0.00</li> <li>n= 0.013 Concrete pipe, bends &amp; connections</li> </ul>		307.00' S= 0.0099 '/' Cc= 0.900
#2	Discarded	312.00'	8.270 in/hr E	xfiltration over	

**Discarded OutFlow** Max=0.00 cfs @ 24.91 hrs HW=312.00' (Free Discharge) **2=Exfiltration** (Controls 0.00 cfs)

Primary OutFlow Max=9.46 cfs @ 12.65 hrs HW=312.00' TW=306.19' (Dynamic Tailwater) **1=Culvert** (Inlet Controls 9.46 cfs @ 4.03 fps)

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Pond 2P: INLET POND



# Summary for Pond 23P: Roadside Swale

Inflow Area =	0.761 ac,	0.00% Impervious, Inflow D	epth = 0.18" for 10-Year event
Inflow =	0.02 cfs @	13.06 hrs, Volume=	0.011 af
Outflow =	0.02 cfs @	13.35 hrs, Volume=	0.011 af, Atten= 4%, Lag= 17.3 min
Discarded =	0.02 cfs @	13.35 hrs, Volume=	0.011 af
Primary =	0.00 cfs @	0.00 hrs, Volume=	0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 306.14' @ 13.35 hrs Surf.Area= 98 sf Storage= 7 cf

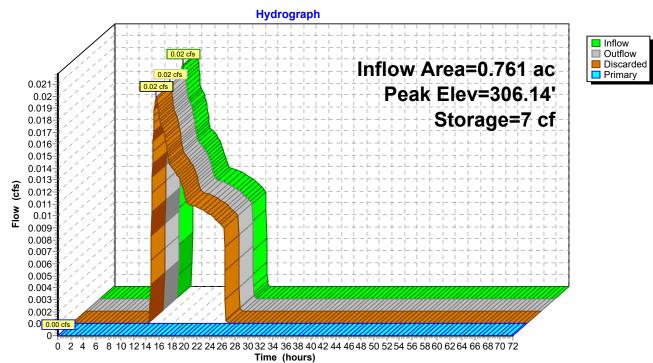
Plug-Flow detention time= 4.0 min calculated for 0.011 af (100% of inflow) Center-of-Mass det. time= 4.0 min (1,053.4 - 1,049.4)

Volume	Invert	Avail.Sto	rage Storage	e Description			
#1	#1 306.00' 1,365		65 cf Custon	n Stage Data (P	rismatic)Listed below (Recalc)		
Elevatio (fee		urf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)			
306.0	306.00 0		0	0			
307.0	307.00 700		350	350			
308.0	308.00 1,330		1,015	1,365			
Device	Routing	Invert	Outlet Device	es			
#1 #2	Discarded Primary	306.00' 307.25'	<b>10.0' long x</b> Head (feet) ( 2.50 3.00 3.	<b>2.0' breadth Br</b> 0.20 0.40 0.60 .50 h) 2.54 2.61 2.	Surface area Phase-In= 0.01' oad-Crested Rectangular Weir 0.80 1.00 1.20 1.40 1.60 1.80 2.00 61 2.60 2.66 2.70 2.77 2.89 2.88		
Discorded OutFlow May-0.02 of @ 12.25 hrs. LIW-206.14! (Free Discharge)							

**Discarded OutFlow** Max=0.02 cfs @ 13.35 hrs HW=306.14' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.02 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=306.00' TW=0.00' (Dynamic Tailwater) 2=Broad-Crested Rectangular Weir( Controls 0.00 cfs)





Pre-Post Development REV 1-26-24 Prepared by Guerriere & Halnon, Inc. HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD Soft	NRCC 24-hr C 25-Year Rainfall=6.15" Printed 2/20/2024 ware Solutions LLC Page 34
Time span=0.00-72.00 hrs Runoff by SCS TR-20 metho Reach routing by Dyn-Stor-Ind method	, dt=0.05 hrs, 1441 points od, UH=SCS, Weighted-CN
SubcatchmentPR-1: Subcatchmentto Runoff Are	ea=141,517 sf 55.11% Impervious Runoff Depth=3.12" Tc=6.0 min CN=72 Runoff=12.42 cfs 0.844 af
	rea=670,872 sf 0.00% Impervious Runoff Depth=1.29" 1,673' Tc=37.2 min CN=51 Runoff=9.42 cfs 1.658 af
SubcatchmentPR-4: Subcatchmentto BVW Runoff Flow Length	Area=33,131 sf 0.00% Impervious Runoff Depth=0.49" n=544' Tc=10.6 min CN=39 Runoff=0.12 cfs 0.031 af
	Area=85,707 sf 0.00% Impervious Runoff Depth=1.69" n=572' Tc=15.5 min CN=56 Runoff=2.73 cfs 0.276 af
Reach AP 1: Analysis Point - AP1	Inflow=1.30 cfs 0.124 af Outflow=1.30 cfs 0.124 af
Reach AP 2: Analysis Point - AP2	Inflow=2.73 cfs 0.276 af Outflow=2.73 cfs 0.276 af
Pond 1P: Infiltration Basin #1Peak ElevDiscarded=4.45 cfs2.377 afPrimary=1.30 cfs0.124 afS	v=307.55' Storage=25,472 cf Inflow=13.81 cfs 2.501 af econdary=0.00 cfs 0.000 af Outflow=5.75 cfs 2.501 af
	ak Elev=312.01' Storage=6 cf Inflow=9.42 cfs 1.658 af Primary=9.30 cfs 1.657 af Outflow=9.42 cfs 1.658 af
	Elev=306.55' Storage=105 cf Inflow=0.12 cfs 0.031 af Primary=0.00 cfs 0.000 af Outflow=0.07 cfs 0.031 af
	off Volume = 2.810 af Average Runoff Depth = 1.58 Pervious = 19.588 ac 8.38% Impervious = 1.790 ac

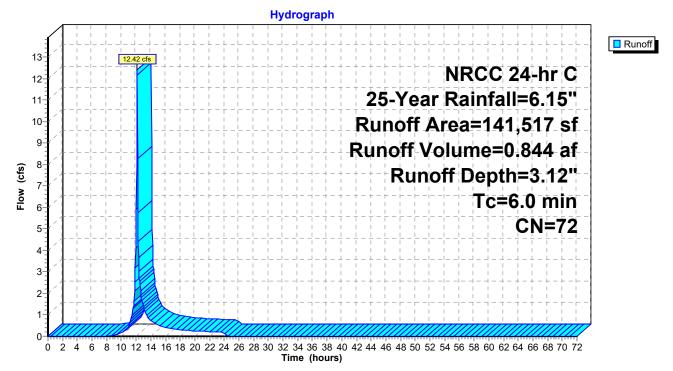
#### Summary for Subcatchment PR-1: Subcatchment to Basin #1

Runoff = 12.42 cfs @ 12.13 hrs, Volume= 0.844 af, Depth= 3.12"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 25-Year Rainfall=6.15"

	Area (sf)	CN	Description						
*	38,062	98	Paved road	s w/curbs &	& sewers				
*	19,293	98	Roofs						
	63,524	39	>75% Gras	s cover, Go	lood, HSG A				
*	20,638	98	Water Surfa	ace, HSG A	Α				
	141,517	72	Weighted A	Weighted Average					
	63,524		44.89% Pe	44.89% Pervious Area					
	77,993		55.11% lmp	55.11% Impervious Area					
	Tc Length			Capacity	•				
_	(min) (feet)	(ft/	ft) (ft/sec)	(cfs)					
	6.0				Direct Entry,				

#### Subcatchment PR-1: Subcatchment to Basin #1



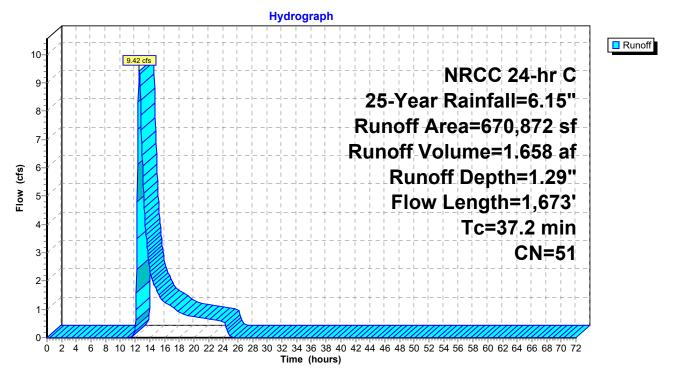
# Summary for Subcatchment PR-2: Subcatchment to Basin #2

Runoff = 9.42 cfs @ 12.59 hrs, Volume= 1.658 af, Depth= 1.29"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 25-Year Rainfall=6.15"

A	rea (sf)	CN D	escription		
5	27,673	55 V	/oods, Go	od, HSG B	
	96,783	30 V	/oods, Go	od, HSG A	
	15,981				bod, HSG B
	30,435	39 >	75% Gras	s cover, Go	bod, HSG A
6	70,872		/eighted A		
6	70,872	1	00.00% Pe	ervious Are	a
_				<b>•</b> •	<b>—</b> • • •
, Tc	Length	Slope	Velocity		Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
7.0	50	0.0800	0.12		Sheet Flow, Segment A-B
	70	0 0000			Woods: Light underbrush n= 0.400 P2= 3.26"
0.9	78	0.0800	1.41		Shallow Concentrated Flow, Segment B-C
40.7	500	0 00 40	0.77		Woodland Kv= 5.0 fps
12.7	592	0.0240	0.77		Shallow Concentrated Flow, Segment C-D
14.1	581	0.0190	0.69		Woodland Kv= 5.0 fps Shallow Concentrated Flow, Segment D-E
14.1	501	0.0190	0.09		Woodland Kv= 5.0 fps
2.0	60	0.0100	0.50		Shallow Concentrated Flow, Segment E-F
2.0	00	0.0100	0.00		Woodland Kv= 5.0 fps
0.5	312	0.0230	10.92	34.31	Pipe Channel, Segment F-G
0.0	0.2	0.0200	10.02	0 110 1	24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'
					n= 0.013 Concrete pipe, straight & clean
37.2	1,673	Total			

#### Subcatchment PR-2: Subcatchment to Basin #2



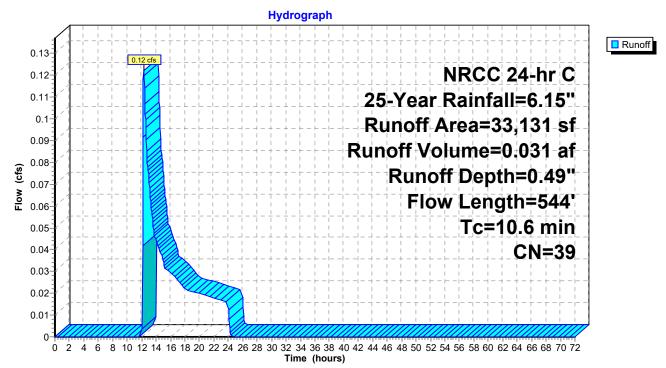
#### Summary for Subcatchment PR-4: Subcatchment to BVW

Runoff = 0.12 cfs @ 12.31 hrs, Volume= 0.031 af, Depth= 0.49"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 25-Year Rainfall=6.15"

_	A	rea (sf)	CN	Description		
		33,131	39	>75% Gras	s cover, Go	bod, HSG A
_		33,131		100.00% P	ervious Are	a
	Tc (min)	Length (feet)	Slope (ft/ft		Capacity (cfs)	Description
-	5.6	50	0.0200	0.15		Sheet Flow, Segment A-B
						Grass: Short n= 0.150 P2= 3.26"
	2.0	194	0.0550	) 1.64		Shallow Concentrated Flow, Segment B-C
						Short Grass Pasture Kv= 7.0 fps
	0.2	47	0.0050	) 3.79	2.98	
						12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'
	0.0	050	0.0400	4 50		n= 0.011 Concrete pipe, straight & clean
	2.8	253	0.0100	) 1.50		Shallow Concentrated Flow, Segment D-E Grassed Waterway Kv= 15.0 fps
-	10.6	544	Total			Glassed Waterway INV- 10.0 lps
	10.0	044	rolai			

# Subcatchment PR-4: Subcatchment to BVW



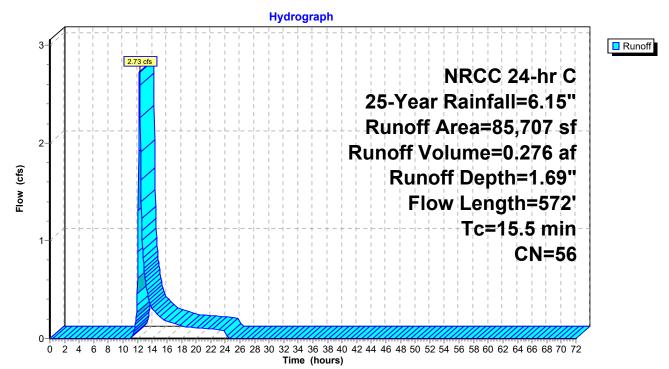
#### Summary for Subcatchment PR3: To Blackstone Street

Runoff = 2.73 cfs @ 12.26 hrs, Volume= 0.276 af, Depth= 1.69"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 25-Year Rainfall=6.15"

Α	rea (sf)	CN D	escription		
	67,471	55 V	Voods, Go	od, HSG B	
	18,236	61 >	75% Gras	s cover, Go	bod, HSG B
	85,707	56 V	Veighted A	verage	
	85,707	1	00.00% Pe	ervious Are	а
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
7.8	50	0.0610	0.11		Sheet Flow, Segment A-B
					Woods: Light underbrush n= 0.400 P2= 3.26"
2.8	215	0.0640	1.26		Shallow Concentrated Flow, Segment B-C
					Woodland Kv= 5.0 fps
2.2	103	0.0240	0.77		Shallow Concentrated Flow, Segment C-D
					Woodland Kv= 5.0 fps
2.7	204	0.0320	1.25		Shallow Concentrated Flow, Segment D-E
					Short Grass Pasture Kv= 7.0 fps
15.5	572	Total			

#### Subcatchment PR3: To Blackstone Street

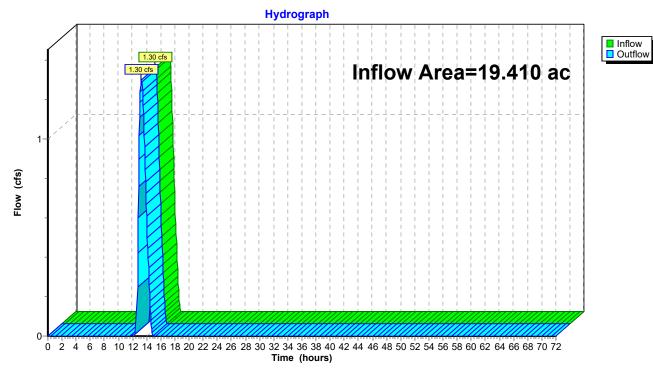


### Summary for Reach AP 1: Analysis Point - AP1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =	19.410 ac,	9.22% Impervious, Inflow E	Depth = 0.08"	for 25-Year event
Inflow =	1.30 cfs @	13.25 hrs, Volume=	0.124 af	
Outflow =	1.30 cfs @	13.25 hrs, Volume=	0.124 af, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



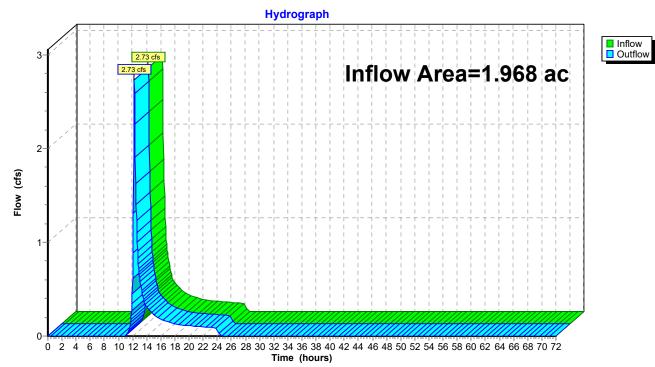
### Reach AP 1: Analysis Point - AP1

### Summary for Reach AP 2: Analysis Point - AP2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area	a =	1.968 ac,	0.00% Impervious	, Inflow Depth = $1.6$	69" for 25-Year event
Inflow	=	2.73 cfs @	12.26 hrs, Volum	e= 0.276 af	
Outflow	=	2.73 cfs @	12.26 hrs, Volum	e= 0.276 af,	Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



### Reach AP 2: Analysis Point - AP2

### Summary for Pond 1P: Infiltration Basin #1

Inflow Area =	18.650 ac,	9.60% Impervious, Infl	ow Depth = 1.61" for 25-Year event
Inflow =	13.81 cfs @	12.14 hrs, Volume=	2.501 af
Outflow =	5.75 cfs @	13.25 hrs, Volume=	2.501 af, Atten= 58%, Lag= 66.4 min
Discarded =	4.45 cfs @	13.25 hrs, Volume=	2.377 af
Primary =	1.30 cfs @	13.25 hrs, Volume=	0.124 af
Secondary =	0.00 cfs @	0.00 hrs, Volume=	0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 307.55' @ 13.25 hrs Surf.Area= 14,470 sf Storage= 25,472 cf Flood Elev= 310.50' Surf.Area= 20,637 sf Storage= 77,211 cf

Plug-Flow detention time= 48.2 min calculated for 2.499 af (100% of inflow) Center-of-Mass det. time= 48.2 min ( 950.5 - 902.4 )

Volume	Invert	Avail.Stor	rage Storage	e Description		
#1	305.50' 87,52		29 cf Custom	n Stage Data (Prismatic)Listed below (Recalc)		
<b>-</b> 1						
Elevatio		rf.Area	Inc.Store	Cum.Store		
(fee	/	<u>(sq-ft)</u>	(cubic-feet)	(cubic-feet)		
305.5		10,451	0	0		
306.0		11,407	5,465	5,465		
308.0		15,368	26,775	32,240		
310.0		19,555	34,923	67,163		
310.5		20,637	10,048	77,211		
311.0	00	20,637	10,319	87,529		
Davias	Douting	Invert	Outlet Device			
Device	Routing	Invert	Outlet Device			
#1	Primary	306.00'	24.0" Round			
				CP, groove end w/headwall, Ke= 0.200		
			Inlet / Outlet Invert= 306.00' / 305.53' S= 0.0050 '/' Cc= 0.900			
				oncrete pipe, straight & clean, Flow Area= 3.14 sf		
#2	Device 1	308.55'		"Horiz. Orifice/Grate C= 0.600		
			Limited to weir flow at low heads			
#3	Device 1	307.00'	12.0" W x 9.0" H Vert. Orifice/Grate C= 0.600			
#4	Discarded	305.50'		Exfiltration over Horizontal area		
			Conductivity	to Groundwater Elevation = 302.70' Phase-In= 0.01'		
#5 Secondary 309.90'		30.0' long x 10.0' breadth Broad-Crested Rectangular Weir				
			Head (feet) (	0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60		
			Coef. (Englis	sh) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64		

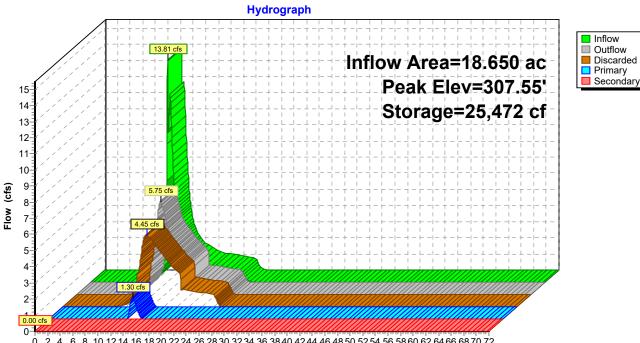
**Discarded OutFlow** Max=4.45 cfs @ 13.25 hrs HW=307.55' (Free Discharge) **4=Exfiltration** (Controls 4.45 cfs)

**Primary OutFlow** Max=1.30 cfs @ 13.25 hrs HW=307.55' TW=0.00' (Dynamic Tailwater) **1=Culvert** (Passes 1.30 cfs of 10.05 cfs potential flow)

2=Orifice/Grate (Controls 0.00 cfs)

-3=Orifice/Grate (Orifice Controls 1.30 cfs @ 2.37 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=305.50' TW=0.00' (Dynamic Tailwater) 5=Broad-Crested Rectangular Weir( Controls 0.00 cfs)



Pond 1P: Infiltration Basin #1

0 2 4 6 8 10 12 14 16 18 20 22 24 26 28 30 32 34 36 38 40 42 44 46 48 50 52 54 56 58 60 62 64 66 68 70 72 Time (hours)

### Summary for Pond 2P: INLET POND

Inflow Area = Inflow = Outflow = Discarded = Primary =	9.42 cfs @ 9.42 cfs @ 0.12 cfs @	0.00% Impervious, Infl 12.59 hrs, Volume= 12.59 hrs, Volume= 12.59 hrs, Volume= 12.59 hrs, Volume=	ow Depth = 1.29" for 25-Year event 1.658 af 1.658 af, Atten= 0%, Lag= 0.2 min 0.001 af 1.657 af			
Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 312.01' @ 12.59 hrs Surf.Area= 1,185 sf Storage= 6 cf						
Plug-Flow detention	on time= (not	calculated: outflow prec	edes inflow)			

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 0.0 min ( 932.7 - 932.7 )

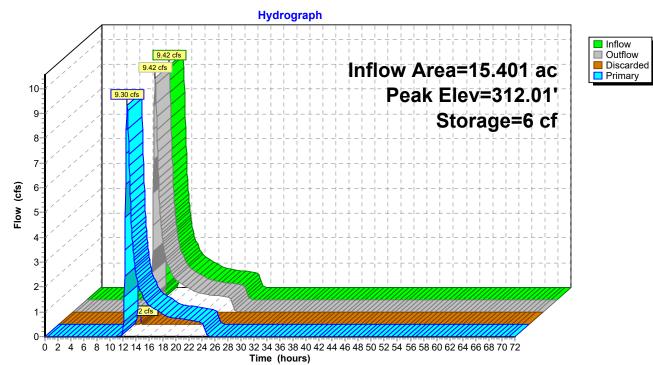
Volume	Inver	t Avail.Sto	rage Storage	Description		
#1	312.00	)' 3,48	30 cf Custom	n Stage Data (P	rismatic)Listed below (Recalc)	
Elevatio (fee		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)		
312.0	, , , , ,		0	0		
313.0	,		1,436	1,436		
314.0	314.00 2,398		2,044	3,480		
Device	Routing	Invert	Outlet Device	es		
#1	Primary	310.60'		CP, square edge	e headwall, Ke= 0.500 / 307.00' S= 0.0099 '/' Cc= 0.900	
#2	Discarded	312.00'	n= 0.013 Concrete pipe, bends & connections, Flow Area= 3.14 sf <b>8.270 in/hr Exfiltration over Surface area</b> Conductivity to Groundwater Elevation = 304.67' Phase-In= 0.01'			
Dieserd	<b>Discourded OutFlow May-0.10 at @ 10 50 hrs. UW-210.01</b> (Free Discharge)					

**Discarded OutFlow** Max=0.12 cfs @ 12.59 hrs HW=312.01' (Free Discharge) **2=Exfiltration** (Controls 0.12 cfs)

Primary OutFlow Max=9.52 cfs @ 12.59 hrs HW=312.01' TW=306.98' (Dynamic Tailwater) ☐ 1=Culvert (Inlet Controls 9.52 cfs @ 4.04 fps)

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Pond 2P: INLET POND



### Summary for Pond 23P: Roadside Swale

Inflow Area =	0.761 ac,	0.00% Impervious, Inflow D	epth = 0.49" for 25-Year event
Inflow =	0.12 cfs @	12.31 hrs, Volume=	0.031 af
Outflow =	0.07 cfs @	12.98 hrs, Volume=	0.031 af, Atten= 40%, Lag= 40.4 min
Discarded =	0.07 cfs @	12.98 hrs, Volume=	0.031 af
Primary =	0.00 cfs @	0.00 hrs, Volume=	0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 306.55' @ 12.98 hrs Surf.Area= 384 sf Storage= 105 cf

Plug-Flow detention time= 13.2 min calculated for 0.031 af (100% of inflow) Center-of-Mass det. time= 13.2 min ( 992.6 - 979.5 )

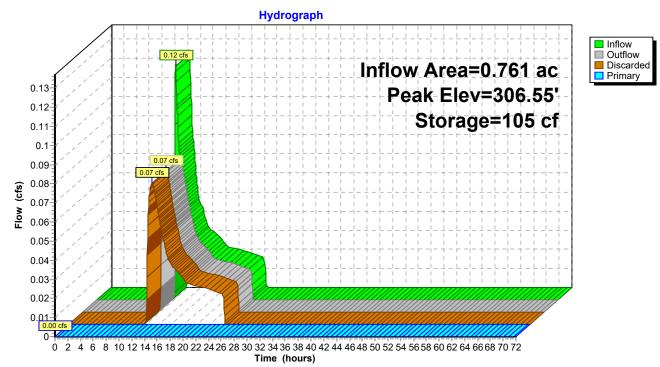
Volume	Invert	Avail.Sto	rage Storage	Description	
#1	306.00'	1,36	65 cf Custom	n Stage Data (P	rismatic)Listed below (Recalc)
Elevatio (fee 306.0 307.0 308.0	)0 00 00	urf.Area (sq-ft) 0 700 1,330	Inc.Store (cubic-feet) 0 350 1,015	Cum.Store (cubic-feet) 0 350 1,365	
Device #1 #2	Routing Discarded Primary	Invert 306.00' 307.25'	<b>10.0' long x</b> Head (feet) ( 2.50 3.00 3.	<b>xfiltration over</b> <b>2.0' breadth Br</b> 0.20 0.40 0.60 50 h) 2.54 2.61 2.	Surface area Phase-In= 0.01' road-Crested Rectangular Weir 0.80 1.00 1.20 1.40 1.60 1.80 2.00 61 2.60 2.66 2.70 2.77 2.89 2.88
Discarded OutFlow Max=0.07 cfs @ 12.98 hrs HW=306.55' (Free Discharge)					

**1=Exfiltration** (Exfiltration Controls 0.07 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=306.00' TW=0.00' (Dynamic Tailwater) —2=Broad-Crested Rectangular Weir( Controls 0.00 cfs)

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### Pond 23P: Roadside Swale



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Runoff by SCS	00-72.00 hrs, dt=0.05 hrs, 1441 points TR-20 method, UH=SCS, Weighted-CN Ind method . Pond routing by Dyn-Stor-Ind method
SubcatchmentPR-1: Subcatchmentto	Runoff Area=141,517 sf 55.11% Impervious Runoff Depth=5.35" Tc=6.0 min CN=72 Runoff=21.07 cfs 1.448 af
SubcatchmentPR-2: Subcatchmentto	Runoff Area=670,872 sf 0.00% Impervious Runoff Depth=2.83" ow Length=1,673' Tc=37.2 min CN=51 Runoff=23.64 cfs 3.632 af
SubcatchmentPR-4: Subcatchmentto E	<b>SVW</b> Runoff Area=33,131 sf 0.00% Impervious Runoff Depth=1.48" Flow Length=544' Tc=10.6 min CN=39 Runoff=0.90 cfs 0.094 af
SubcatchmentPR3: To Blackstone Stre	et Runoff Area=85,707 sf 0.00% Impervious Runoff Depth=3.42" Flow Length=572' Tc=15.5 min CN=56 Runoff=5.90 cfs 0.561 af
Reach AP 1: Analysis Point - AP1	Inflow=15.87 cfs 1.339 af Outflow=15.87 cfs 1.339 af
Reach AP 2: Analysis Point - AP2	Inflow=5.90 cfs 0.561 af Outflow=5.90 cfs 0.561 af
<b>Pond 1P: Infiltration Basin #1</b> carded=6.31 cfs 3.721 af Primary=15.79 cfs	Peak Elev=308.91' Storage=47,100 cf Inflow=27.57 cfs 5.050 af 1.329 af Secondary=0.00 cfs 0.000 af Outflow=22.10 cfs 5.050 af
Pond 2P: INLET POND Discarded=0.50 cf	Peak Elev=313.74' Storage=2,886 cf Inflow=23.64 cfs 3.632 af s 0.031 af Primary=22.14 cfs 3.601 af Outflow=22.64 cfs 3.632 af
Pond 23P: Roadside Swale Discarded=0.17	Peak Elev=307.32' Storage=603 cf Inflow=0.90 cfs 0.094 af cfs 0.083 af Primary=0.42 cfs 0.011 af Outflow=0.59 cfs 0.094 af
Total Runoff Area = 21.3	78 ac Runoff Volume = 5.735 af Average Runoff Depth = 3.2 91.62% Pervious = 19.588 ac  8.38% Impervious = 1.790 a

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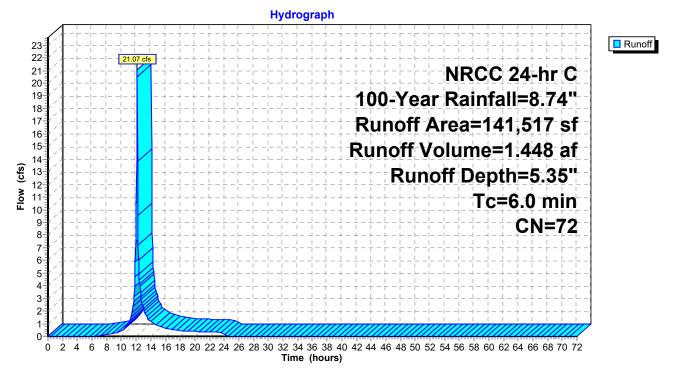
### Summary for Subcatchment PR-1: Subcatchment to Basin #1

Runoff = 21.07 cfs @ 12.13 hrs, Volume= 1.448 af, Depth= 5.35"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 100-Year Rainfall=8.74"

_	Area (sf)	CN	Description	Description					
*	38,062	98	Paved road	s w/curbs &	& sewers				
*	19,293	98	Roofs						
	63,524	39	>75% Gras	s cover, Go	lood, HSG A				
*	20,638	98	Water Surfa	ace, HSG A	Α				
	141,517	72	Weighted A	verage					
	63,524		44.89% Pei	vious Area	а				
	77,993		55.11% Imp	55.11% Impervious Area					
	Tc Length	Slop		Capacity	1				
_	(min) (feet)	(ft/	ft) (ft/sec) (cfs)						
	6.0				Direct Entry,				

### Subcatchment PR-1: Subcatchment to Basin #1



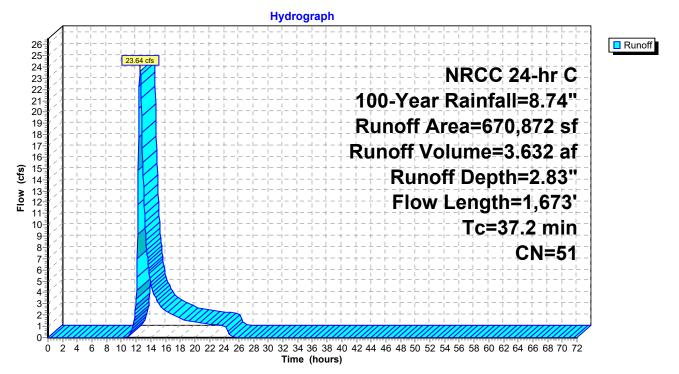
### Summary for Subcatchment PR-2: Subcatchment to Basin #2

Runoff = 23.64 cfs @ 12.55 hrs, Volume= 3.632 af, Depth= 2.83"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 100-Year Rainfall=8.74"

A	rea (sf)	CN D	escription					
5	27,673	55 V	55 Woods, Good, HSG B					
	96,783	30 V	30 Woods, Good, HSG A					
	15,981	61 >	75% Gras	s cover, Go	bod, HSG B			
	30,435	39 >	75% Gras	s cover, Go	ood, HSG A			
6	70,872	51 V	/eighted A	verage				
6	70,872	1	00.00% Pe	ervious Are	а			
Тс	Length	Slope	Velocity		Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
7.0	50	0.0800	0.12		Sheet Flow, Segment A-B			
					Woods: Light underbrush n= 0.400 P2= 3.26"			
0.9	78	0.0800	1.41		Shallow Concentrated Flow, Segment B-C			
					Woodland Kv= 5.0 fps			
12.7	592	0.0240	0.77		Shallow Concentrated Flow, Segment C-D			
					Woodland Kv= 5.0 fps			
14.1	581	0.0190	0.69		Shallow Concentrated Flow, Segment D-E			
0.0	00	0.0400	0.50		Woodland Kv= 5.0 fps			
2.0	60	0.0100	0.50		Shallow Concentrated Flow, Segment E-F			
0.5	040	0 0000	40.00	04.04	Woodland Kv= 5.0 fps			
0.5	312	0.0230	10.92	34.31	Pipe Channel, Segment F-G			
					24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'			
07.0	4.070	<b></b>			n= 0.013 Concrete pipe, straight & clean			
37.2	1,673	Total						

### Subcatchment PR-2: Subcatchment to Basin #2



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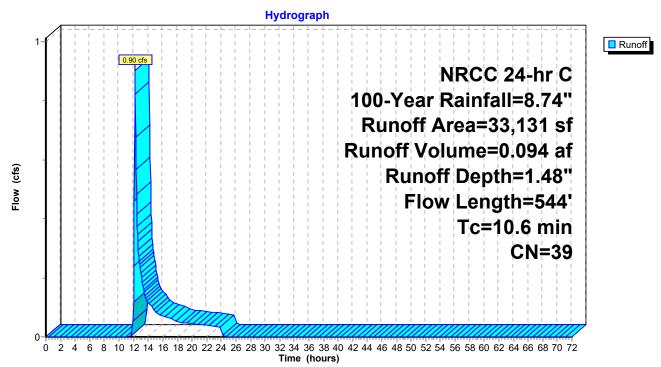
### Summary for Subcatchment PR-4: Subcatchment to BVW

Runoff = 0.90 cfs @ 12.21 hrs, Volume= 0.094 af, Depth= 1.48"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 100-Year Rainfall=8.74"

A	rea (sf)	CN	Description					
	33,131	39	39 >75% Grass cover, Good, HSG A					
	33,131		100.00% P	ervious Are	a			
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description			
5.6	50	0.0200	0.15		Sheet Flow, Segment A-B			
2.0	194	0.0550	1.64		Grass: Short n= 0.150 P2= 3.26" Shallow Concentrated Flow, Segment B-C Short Grass Pasture Kv= 7.0 fps			
0.2	47	0.0050	3.79	2.98				
2.8	253	0.0100	1.50		12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25' n= 0.011 Concrete pipe, straight & clean Shallow Concentrated Flow, Segment D-E Grassed Waterway Kv= 15.0 fps			
10.6	544	Total						

### Subcatchment PR-4: Subcatchment to BVW



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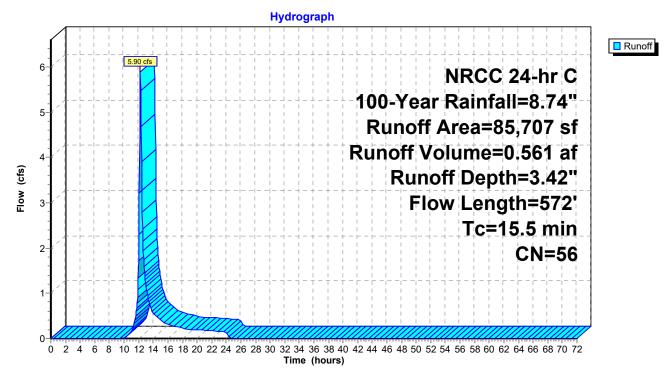
### Summary for Subcatchment PR3: To Blackstone Street

Runoff = 5.90 cfs @ 12.25 hrs, Volume= 0.561 af, Depth= 3.42"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 100-Year Rainfall=8.74"

A	rea (sf)	CN D	escription		
	67,471	55 V	Voods, Go	od, HSG B	
	18,236	61 >	75% Gras	s cover, Go	ood, HSG B
	85,707	56 V	Veighted A	verage	
	85,707	1	00.00% Pe	ervious Are	а
_					
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
7.8	50	0.0610	0.11		Sheet Flow, Segment A-B
					Woods: Light underbrush n= 0.400 P2= 3.26"
2.8	215	0.0640	1.26		Shallow Concentrated Flow, Segment B-C
					Woodland Kv= 5.0 fps
2.2	103	0.0240	0.77		Shallow Concentrated Flow, Segment C-D
					Woodland Kv= 5.0 fps
2.7	204	0.0320	1.25		Shallow Concentrated Flow, Segment D-E
					Short Grass Pasture Kv= 7.0 fps
15.5	572	Total			

### Subcatchment PR3: To Blackstone Street

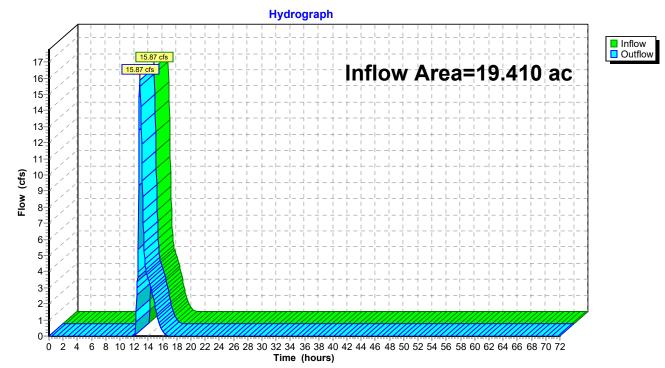


### Summary for Reach AP 1: Analysis Point - AP1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =	= 19.410 a	ac, 9.22% Imperviou	s, Inflow Depth = 0.8	33" for 100-Year event
Inflow =	15.87 cfs	s @ 12.83 hrs, Volur	ne= 1.339 af	
Outflow =	15.87 cfs	s @ 12.83 hrs, Volur	ne= 1.339 af,	Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



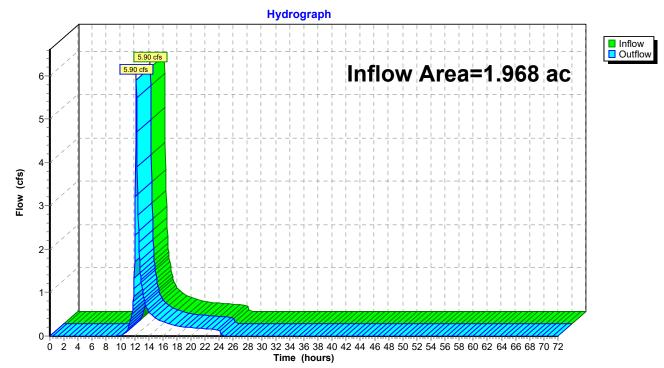
### Reach AP 1: Analysis Point - AP1

### Summary for Reach AP 2: Analysis Point - AP2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area	a =	1.968 ac,	0.00% Impervious, Inflow	/ Depth = 3.42"	for 100-Year event
Inflow	=	5.90 cfs @	12.25 hrs, Volume=	0.561 af	
Outflow	=	5.90 cfs @	12.25 hrs, Volume=	0.561 af, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



Reach AP 2: Analysis Point - AP2

### Summary for Pond 1P: Infiltration Basin #1

Inflow Area =	18.650 ac,	9.60% Impervious, Infle	ow Depth = 3.25" for 100-Year event
Inflow =	27.57 cfs @	12.14 hrs, Volume=	5.050 af
Outflow =	22.10 cfs @	12.83 hrs, Volume=	5.050 af, Atten= 20%, Lag= 41.1 min
Discarded =	6.31 cfs @	12.83 hrs, Volume=	3.721 af
Primary =	15.79 cfs @	12.83 hrs, Volume=	1.329 af
Secondary =	0.00 cfs @	0.00 hrs, Volume=	0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 308.91' @ 12.83 hrs Surf.Area= 17,274 sf Storage= 47,100 cf Flood Elev= 310.50' Surf.Area= 20,637 sf Storage= 77,211 cf

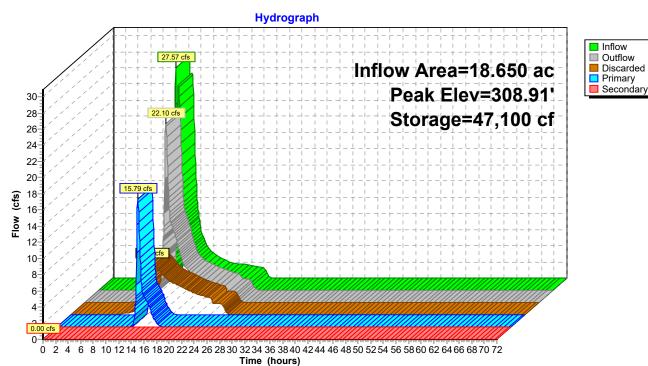
Plug-Flow detention time= 52.1 min calculated for 5.046 af (100% of inflow) Center-of-Mass det. time= 52.0 min ( 934.8 - 882.8 )

Volume	Invert	Avail.Stor	rage Storage	e Description
#1	305.50'	87,52	29 cf Custom	n Stage Data (Prismatic)Listed below (Recalc)
<b>-</b> 1				
Elevatio		rf.Area	Inc.Store	Cum.Store
(fee	/	<u>(sq-ft)</u>	(cubic-feet)	(cubic-feet)
305.5		10,451	0	0
306.0		11,407	5,465	5,465
308.0		15,368	26,775	32,240
310.0		19,555	34,923	67,163
310.5		20,637	10,048	77,211
311.0	00	20,637	10,319	87,529
Davias	Douting	Invort	Outlet Device	
Device	Routing	Invert	Outlet Device	
#1	Primary	306.00'	24.0" Round	
				CP, groove end w/headwall, Ke= 0.200
				Invert= 306.00' / 305.53' S= 0.0050 '/' Cc= 0.900
				oncrete pipe, straight & clean, Flow Area= 3.14 sf
#2	Device 1	308.55'		"Horiz. Orifice/Grate C= 0.600
				eir flow at low heads
#3	Device 1	307.00'	12.0" W x 9.0	0" H Vert. Orifice/Grate C= 0.600
#4	Discarded	305.50'		Exfiltration over Horizontal area
			Conductivity	to Groundwater Elevation = 302.70' Phase-In= 0.01'
#5	Secondary	309.90'	30.0' long x	10.0' breadth Broad-Crested Rectangular Weir
			Head (feet) (	0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (Englis	sh) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

**Discarded OutFlow** Max=6.31 cfs @ 12.83 hrs HW=308.91' (Free Discharge) **4=Exfiltration** (Controls 6.31 cfs)

Primary OutFlow Max=15.71 cfs @ 12.83 hrs HW=308.91' TW=0.00' (Dynamic Tailwater) 1=Culvert (Passes 15.71 cfs of 20.72 cfs potential flow) 2=Orifice/Grate (Weir Controls 11.25 cfs @ 1.96 fps) 3=Orifice/Grate (Orifice Controls 4.46 cfs @ 5.95 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=305.50' TW=0.00' (Dynamic Tailwater) 5=Broad-Crested Rectangular Weir( Controls 0.00 cfs)



### Pond 1P: Infiltration Basin #1

### Summary for Pond 2P: INLET POND

Inflow Area =	15.401 ac,	0.00% Impervious, Inflow De	epth = 2.83" for 100-Year event
Inflow =	23.64 cfs @	12.55 hrs, Volume=	3.632 af
Outflow =	22.64 cfs @	12.64 hrs, Volume=	3.632 af, Atten= 4%, Lag= 5.4 min
Discarded =	0.50 cfs @	12.64 hrs, Volume=	0.031 af
Primary =	22.14 cfs @	12.64 hrs, Volume=	3.601 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 313.74' @ 12.64 hrs Surf.Area= 2,216 sf Storage= 2,886 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 0.5 min ( 904.6 - 904.1 )

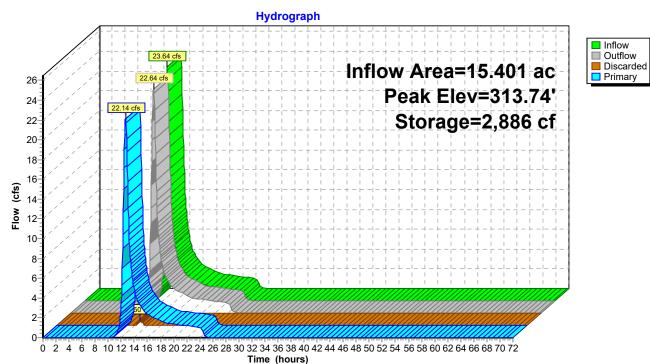
Volume	Invert	Avail.Sto	rage Storage	Description		
#1	312.00'	3,48	30 cf Custom	n Stage Data (P	rismatic)Listed below	w (Recalc)
Elevatio	on Su	ırf.Area	Inc.Store	Cum.Store		
(fee		(sq-ft)	(cubic-feet)	(cubic-feet)		
312.0	00	1,182	0	0		
313.0	00	1,690	1,436	1,436		
314.0	00	2,398	2,044	3,480		
Device	Routing	Invert	Outlet Device	s		
#1	Primary	310.60'	Inlet / Outlet I	CP, square edge nvert= 310.60' /	e headwall, Ke= 0.50 307.00' S= 0.0099 ds & connections, Fl	'/' Cc= 0.900
#2	Discarded	312.00'	8.270 in/hr E	xfiltration over		Phase-In= 0.01'
<b>D</b> .						

**Discarded OutFlow** Max=0.50 cfs @ 12.64 hrs HW=313.74' (Free Discharge) **2=Exfiltration** (Controls 0.50 cfs)

Primary OutFlow Max=22.11 cfs @ 12.64 hrs HW=313.74' TW=308.73' (Dynamic Tailwater) **1=Culvert** (Inlet Controls 22.11 cfs @ 7.04 fps)

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Pond 2P: INLET POND



### Summary for Pond 23P: Roadside Swale

Inflow Area =	0.761 ac,	0.00% Impervious, Inflow D	Pepth = 1.48" for 100-Year event
Inflow =	0.90 cfs @	12.21 hrs, Volume=	0.094 af
Outflow =	0.59 cfs @	12.37 hrs, Volume=	0.094 af, Atten= 35%, Lag= 9.8 min
Discarded =	0.17 cfs @	12.37 hrs, Volume=	0.083 af
Primary =	0.42 cfs @	12.37 hrs, Volume=	0.011 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 307.32' @ 12.37 hrs Surf.Area= 899 sf Storage= 603 cf

Plug-Flow detention time= 31.8 min calculated for 0.094 af (100% of inflow) Center-of-Mass det. time= 31.7 min (954.3 - 922.5)

Volume	Invert	Avail.Sto	rage Storage	e Description		
#1	306.00'	1,30	65 cf Custon	n Stage Data (P	rismatic)Listed below (Recalc)	
Elevatio	t)	urf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)		
306.0	-	0	0	0		
307.0	-	700	350	350		
308.0	00	1,330	1,015	1,365		
Device	Routing	Invert	Outlet Device	es		
#1	Discarded	306.00'	8.270 in/hr E	Exfiltration over	Surface area Phase-In= 0.01'	
#2	Primary	307.25'	10.0' long x	2.0' breadth Br	oad-Crested Rectangular Weir	
		001120	Head (feet) 2.50 3.00 3	0.20 0.40 0.60 .50 :h) 2.54 2.61 2.	0.80 1.00 1.20 1.40 1.60 1.80 2.00 61 2.60 2.66 2.70 2.77 2.89 2.88	
Discord	<b>Discourded OutElow Max = 0.17</b> of $(0, 12, 27)$ http://www.commun.commun.commun.com/					

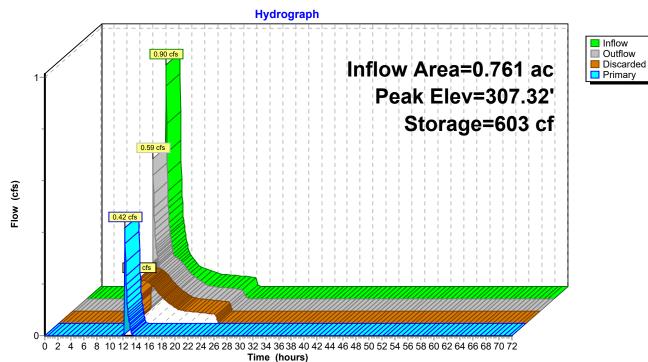
**Discarded OutFlow** Max=0.17 cfs @ 12.37 hrs HW=307.31' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.17 cfs)

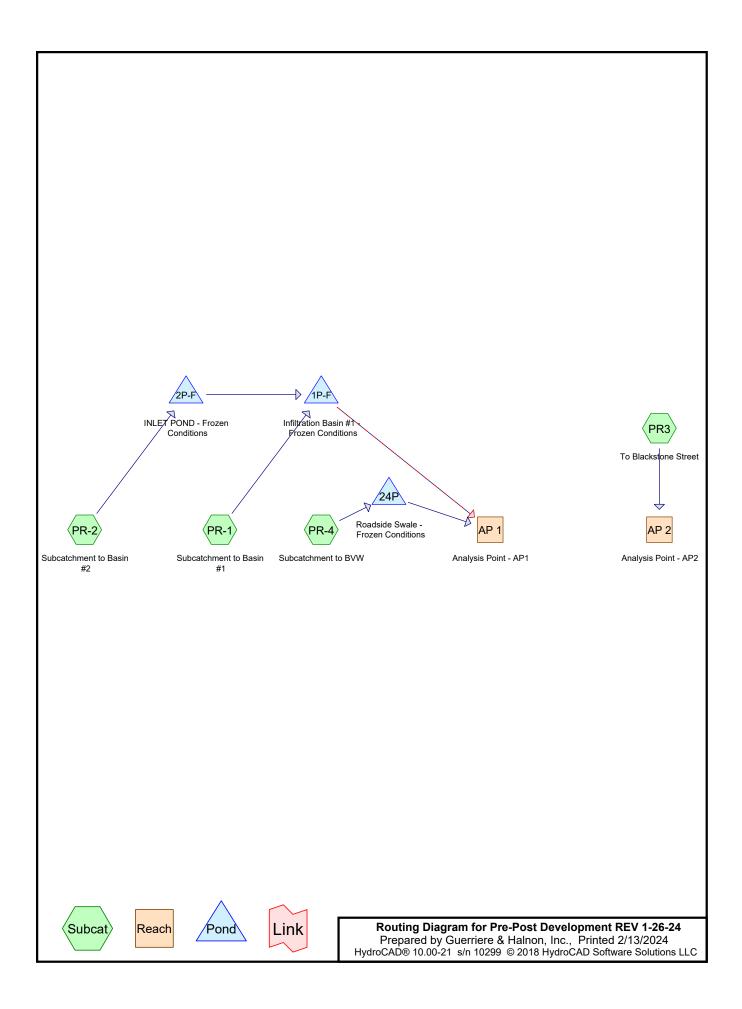
Primary OutFlow Max=0.37 cfs @ 12.37 hrs HW=307.31' TW=0.00' (Dynamic Tailwater) 2=Broad-Crested Rectangular Weir (Weir Controls 0.37 cfs @ 0.62 fps)

NRCC 24-hr C 100-Year Rainfall=8.74" Printed 2/20/2024 ions LLC Page 61

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Pond 23P: Roadside Swale





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### Area Listing (selected nodes)

Area	CN	Description
(acres)		(subcatchment-numbers)
2.918	39	>75% Grass cover, Good, HSG A (PR-1, PR-2, PR-4)
0.786	61	>75% Grass cover, Good, HSG B (PR-2, PR3)
0.874	98	Paved roads w/curbs & sewers (PR-1)
0.443	98	Roofs (PR-1)
0.474	98	Water Surface, HSG A (PR-1)
2.222	30	Woods, Good, HSG A (PR-2)
13.663	55	Woods, Good, HSG B (PR-2, PR3)
21.378	54	TOTAL AREA

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### Soil Listing (selected nodes)

Soil	Subcatchment
Group	Numbers
HSG A	PR-1, PR-2, PR-4
HSG B	PR-2, PR3
HSG C	
HSG D	
Other	PR-1
	TOTAL AREA
	Group HSG A HSG B HSG C HSG D

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HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
 2.918	0.786	0.000	0.000	0.000	3.703	>75% Grass cover, Good	PR
2.010	0.700	0.000	0.000	0.000	0.700		-1,
							PR
							-2,
							PR
							-4,
							PR
							3
0.000	0.000	0.000	0.000	0.874	0.874	Paved roads w/curbs & sewers	PR
							-1
0.000	0.000	0.000	0.000	0.443	0.443	Roofs	PR
							-1
0.474	0.000	0.000	0.000	0.000	0.474	Water Surface	PR
							-1
2.222	13.663	0.000	0.000	0.000	15.884	Woods, Good	PR
							-2,
							PR
							3
5.613	14.448	0.000	0.000	1.317	21.378	TOTAL AREA	

### Ground Covers (selected nodes)

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	Line#	Node	In-Invert	Out-Invert	Length	Slope	n	Diam/Width	Height	Inside-Fill
_		Number	(feet)	(feet)	(feet)	(ft/ft)		(inches)	(inches)	(inches)
	1	PR-2	0.00	0.00	312.0	0.0230	0.013	24.0	0.0	0.0
	2	PR-4	0.00	0.00	47.0	0.0050	0.011	12.0	0.0	0.0
	3	1P-F	306.00	305.52	96.0	0.0050	0.011	24.0	0.0	0.0
	4	2P-F	310.60	307.00	363.4	0.0099	0.013	24.0	0.0	0.0

## Pipe Listing (selected nodes)

Pre-Post Development REV 1-26-24 Prepared by Guerriere & Halnon, Inc. HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCA	NRCC 24-hr C 25-Year Rainfall=6.15" Printed 2/13/2024 D Software Solutions LLC Page 6
Runoff by SCS TR-20	00 hrs, dt=0.05 hrs, 1441 points method, UH=SCS, Weighted-CN ethod - Pond routing by Dyn-Stor-Ind method
SubcatchmentPR-1: Subcatchmentto Run	noff Area=141,517 sf 55.11% Impervious Runoff Depth=3.12" Tc=6.0 min CN=72 Runoff=12.42 cfs 0.844 af
	unoff Area=670,872 sf  0.00% Impervious  Runoff Depth=1.29" ength=1,673'  Tc=37.2 min  CN=51  Runoff=9.42 cfs  1.658 af
	Runoff Area=33,131 sf 0.00% Impervious Runoff Depth=0.49" Length=544' Tc=11.2 min CN=39 Runoff=0.12 cfs 0.031 af
	Runoff Area=85,707 sf 0.00% Impervious Runoff Depth=1.69" Length=572' Tc=15.5 min CN=56 Runoff=2.73 cfs 0.276 af
Reach AP 1: Analysis Point - AP1	Inflow=4.34 cfs 2.110 af Outflow=4.34 cfs 2.110 af
Reach AP 2: Analysis Point - AP2	Inflow=2.73 cfs 0.276 af Outflow=2.73 cfs 0.276 af
	ak Elev=308.59' Storage=41,633 cf Inflow=13.81 cfs 2.502 af 1 af Secondary=0.00 cfs 0.000 af Outflow=4.34 cfs 2.091 af
	Peak Elev=312.01' Storage=11 cf Inflow=9.42 cfs 1.658 af ert n=0.013 L=363.4' S=0.0099 '/' Outflow=9.41 cfs 1.658 af
Pond 24P: Roadside Swale - Frozen	Peak Elev=307.26' Storage=556 cf Inflow=0.12 cfs 0.031 af Outflow=0.04 cfs 0.019 af

Total Runoff Area = 21.378 acRunoff Volume = 2.810 afAverage Runoff Depth = 1.58"91.62% Pervious = 19.588 ac8.38% Impervious = 1.790 ac

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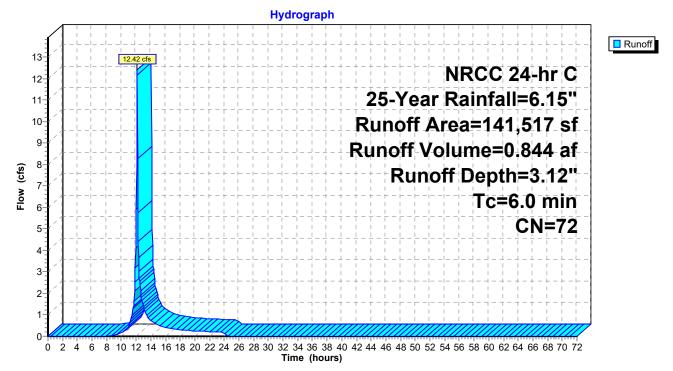
### Summary for Subcatchment PR-1: Subcatchment to Basin #1

Runoff = 12.42 cfs @ 12.13 hrs, Volume= 0.844 af, Depth= 3.12"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 25-Year Rainfall=6.15"

	Area (sf)	CN	Description		
*	38,062	98	Paved road	s w/curbs &	& sewers
*	19,293	98	Roofs		
	63,524	39	>75% Gras	s cover, Go	Good, HSG A
*	20,638	98	Water Surfa	ace, HSG A	Α
	141,517	72	Weighted A	verage	
	63,524		44.89% Per	vious Area	а
	77,993		55.11% lmp	pervious Ar	rea
	Tc Length	Slop		Capacity	
_	(min) (feet)	(ft/	ft) (ft/sec)	(cfs)	
	6.0				Direct Entry,

### Subcatchment PR-1: Subcatchment to Basin #1



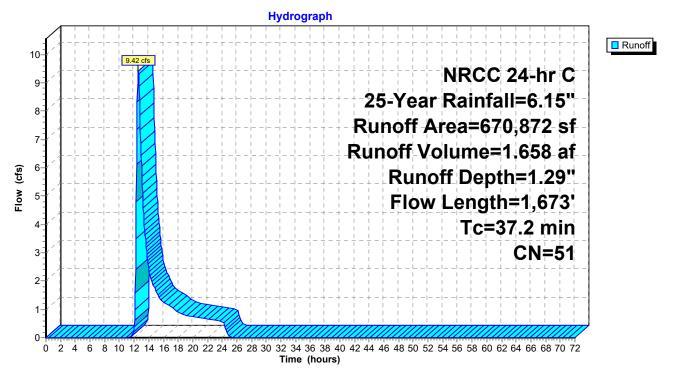
### Summary for Subcatchment PR-2: Subcatchment to Basin #2

Runoff = 9.42 cfs @ 12.59 hrs, Volume= 1.658 af, Depth= 1.29"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 25-Year Rainfall=6.15"

A	rea (sf)	CN D	escription				
5	27,673	55 Woods, Good, HSG B					
	96,783	30 V	/oods, Go	od, HSG A			
	15,981				ood, HSG B		
	30,435	39 >	75% Gras	s cover, Go	ood, HSG A		
6	70,872	51 V	/eighted A	verage			
6	70,872	1	00.00% P	ervious Are	а		
Тс	Length	Slope	Velocity		Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
7.0	50	0.0800	0.12		Sheet Flow, Segment A-B		
					Woods: Light underbrush n= 0.400 P2= 3.26"		
0.9	78	0.0800	1.41		Shallow Concentrated Flow, Segment B-C		
					Woodland Kv= 5.0 fps		
12.7	592	0.0240	0.77		Shallow Concentrated Flow, Segment C-D		
					Woodland Kv= 5.0 fps		
14.1	581	0.0190	0.69		Shallow Concentrated Flow, Segment D-E		
0.0	00	0.0400	0.50		Woodland Kv= 5.0 fps		
2.0	60	0.0100	0.50		Shallow Concentrated Flow, Segment E-F		
0.5	040	0 0000	40.00	04.04	Woodland Kv= 5.0 fps		
0.5	312	0.0230	10.92	34.31	Pipe Channel, Segment F-G		
					24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'		
	4 070	<b>-</b> · ·			n= 0.013 Concrete pipe, straight & clean		
37.2	1,673	Total					

### Subcatchment PR-2: Subcatchment to Basin #2



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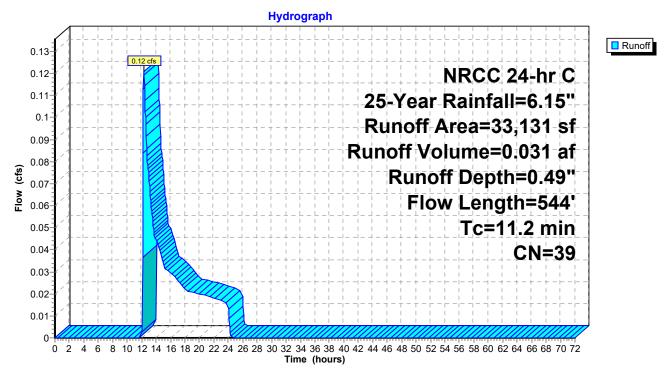
### Summary for Subcatchment PR-4: Subcatchment to BVW

Runoff = 0.12 cfs @ 12.32 hrs, Volume= 0.031 af, Depth= 0.49"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 25-Year Rainfall=6.15"

A	rea (sf)	CN	Description					
	33,131	31 39 >75% Grass cover, Good, HSG A						
	33,131		100.00% P	ervious Are	a			
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description			
5.6	50	0.0200	0.15		Sheet Flow, Segment A-B			
2.0	194	0.0550	1.64		Grass: Short n= 0.150 P2= 3.26" Shallow Concentrated Flow, Segment B-C			
0.2	47	0.0050	3.79	2.98	Short Grass Pasture Kv= 7.0 fps <b>Pipe Channel, RCP_Round 12''</b> 12.0'' Round Area= 0.8 sf Perim= 3.1' r= 0.25'			
3.4	253	0.0070	1.25		n= 0.011 Concrete pipe, straight & clean Shallow Concentrated Flow, Segment D-E Grassed Waterway Kv= 15.0 fps			
11.2	544	Total						

### Subcatchment PR-4: Subcatchment to BVW



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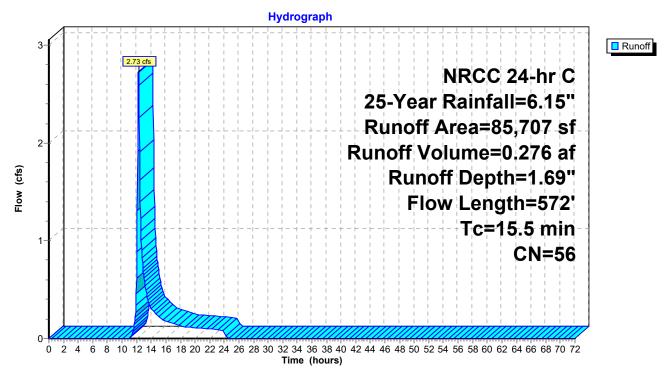
### Summary for Subcatchment PR3: To Blackstone Street

Runoff = 2.73 cfs @ 12.26 hrs, Volume= 0.276 af, Depth= 1.69"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr C 25-Year Rainfall=6.15"

A	rea (sf)	CN D	escription		
	67,471	55 V	Voods, Go	od, HSG B	
	18,236	61 >	75% Gras	s cover, Go	ood, HSG B
	85,707	56 V	Veighted A	verage	
	85,707	1	00.00% Pe	ervious Are	а
_					
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
7.8	50	0.0610	0.11		Sheet Flow, Segment A-B
					Woods: Light underbrush n= 0.400 P2= 3.26"
2.8	215	0.0640	1.26		Shallow Concentrated Flow, Segment B-C
					Woodland Kv= 5.0 fps
2.2	103	0.0240	0.77		Shallow Concentrated Flow, Segment C-D
					Woodland Kv= 5.0 fps
2.7	204	0.0320	1.25		Shallow Concentrated Flow, Segment D-E
					Short Grass Pasture Kv= 7.0 fps
15.5	572	Total			

### Subcatchment PR3: To Blackstone Street

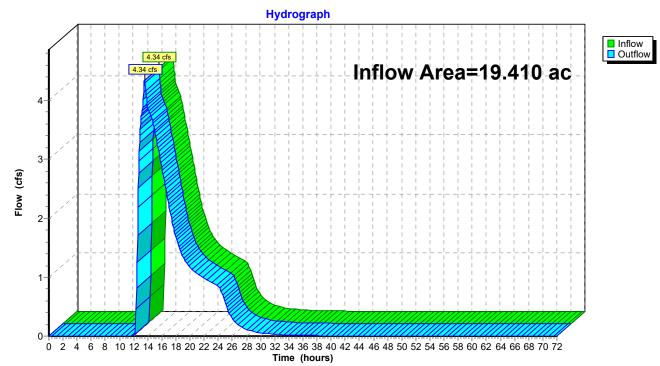


### Summary for Reach AP 1: Analysis Point - AP1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =	19.410 ac,	9.22% Impervious, Inflow E	Depth = 1.30"	for 25-Year event
Inflow =	4.34 cfs @	13.56 hrs, Volume=	2.110 af	
Outflow =	4.34 cfs @	13.56 hrs, Volume=	2.110 af, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



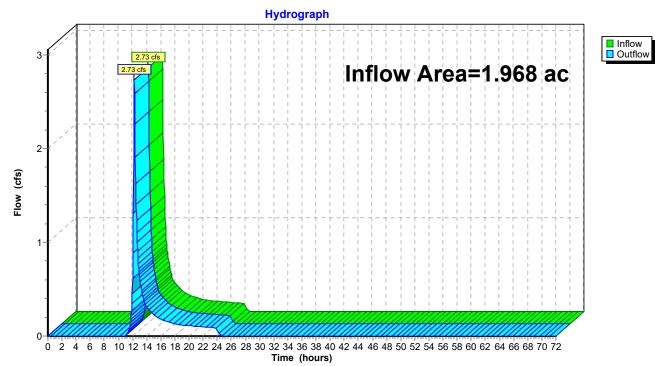
### Reach AP 1: Analysis Point - AP1

### Summary for Reach AP 2: Analysis Point - AP2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area	a =	1.968 ac,	0.00% Impervious	, Inflow Depth = 1.6	69" for 25-Year event
Inflow	=	2.73 cfs @	12.26 hrs, Volum	e= 0.276 af	
Outflow	=	2.73 cfs @	12.26 hrs, Volum	e= 0.276 af,	Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



### Reach AP 2: Analysis Point - AP2

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### Summary for Pond 1P-F: Infiltration Basin #1 - Frozen Conditions

Inflow Area =	18.650 ac,	9.60% Impervious, Inflow E	Depth = 1.61" for 25-Year event
Inflow =	13.81 cfs @	12.14 hrs, Volume=	2.502 af
Outflow =	4.34 cfs @	13.56 hrs, Volume=	2.091 af, Atten= 69%, Lag= 84.9 min
Primary =	4.34 cfs @	13.56 hrs, Volume=	2.091 af
Secondary =	0.00 cfs @	0.00 hrs, Volume=	0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 308.59'@ 13.56 hrs Surf.Area= 16,598 sf Storage= 41,633 cf Flood Elev= 310.50' Surf.Area= 20,637 sf Storage= 77,211 cf

Plug-Flow detention time= 214.5 min calculated for 2.091 af (84% of inflow) Center-of-Mass det. time= 137.9 min (1,040.2 - 902.3)

Volume	Invert	Avail.Stor	rage Storage	Description				
#1	305.50'	87,52	29 cf Custom	Stage Data (Pris	smatic)Listed below (Recalc)			
Elevatio	on Surf	.Area	Inc.Store	Cum.Store				
(fee	et) (	(sq-ft)	(cubic-feet)	(cubic-feet)				
305.5	50 1	0,451	0	0				
306.0	00 1	1,407	5,465	5,465				
308.0	00 1	5,368	26,775	32,240				
310.0	00 1	9,555	34,923	67,163				
310.5	50 2	0,637	10,048	77,211				
311.0	0 2	0,637	10,319	87,529				
Device	Routing	Invert	Outlet Devices	5				
#1	Primary	306.00'	24.0" Round	Culvert				
	-		L= 96.0' RCF	P, groove end w/h	neadwall, Ke= 0.200			
			Inlet / Outlet Ir	nvert= 306.00' / 3	05.52' S= 0.0050 '/' Cc= 0.900			
			n= 0.011 Con	crete pipe, straig	ht & clean, Flow Area= 3.14 sf			
#2	Device 1	308.55'	48.0" x 48.0"	Horiz. Orifice/G	rate C= 0.600			
			Limited to weil	r flow at low head	ls			
#3	Device 1	307.00'	12.0" W x 9.0	" H Vert. Orifice/	/Grate C= 0.600			
#4	Secondary	309.90'	10.0' long x 1	10.0' breadth Bro	oad-Crested Rectangular Weir			
			Head (feet) 0.	.20 0.40 0.60 0.	.80 1.00 1.20 1.40 1.60			
			Coef. (English	) 2.49 2.56 2.70	0 2.69 2.68 2.69 2.67 2.64			
	<b>Primary OutElow May - 4</b> 24 at $(2.12 \text{ from } 1.10)$ - 200 EQL TM-0.001 (Dynamic Tailwater)							

Primary OutFlow Max=4.34 cfs @ 13.56 hrs HW=308.59' TW=0.00' (Dynamic Tailwater)

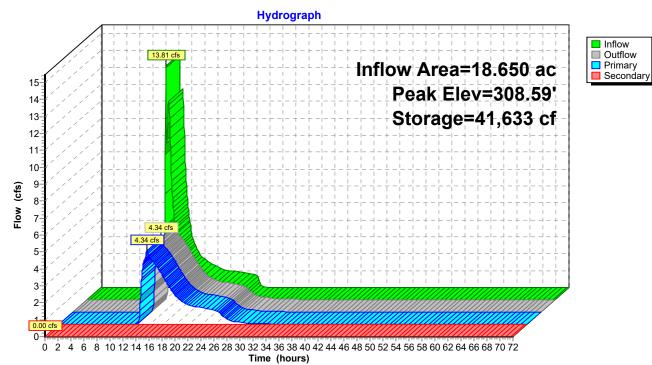
-1=Culvert (Passes 4.34 cfs of 19.04 cfs potential flow)

2=Orifice/Grate (Weir Controls 0.38 cfs @ 0.63 fps)

-3=Orifice/Grate (Orifice Controls 3.96 cfs @ 5.28 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=305.50' TW=0.00' (Dynamic Tailwater) 4=Broad-Crested Rectangular Weir( Controls 0.00 cfs)

#### Pond 1P-F: Infiltration Basin #1 - Frozen Conditions



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#### Summary for Pond 2P-F: INLET POND - Frozen Conditions

Inflow Area =	15.401 ac,	0.00% Impervious, Inflov	w Depth = 1.29" for 25-Year event	
Inflow =	9.42 cfs @	12.59 hrs, Volume=	1.658 af	
Outflow =	9.41 cfs @	12.60 hrs, Volume=	1.658 af, Atten= 0%, Lag= 0.4 min	i i
Primary =	9.41 cfs @	12.60 hrs, Volume=	1.658 af	

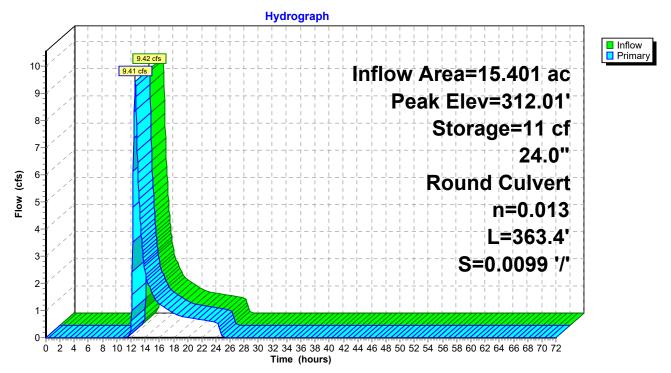
Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 312.01' @ 12.60 hrs Surf.Area= 1,187 sf Storage= 11 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 0.0 min ( 932.7 - 932.7 )

Volume	Inve	ert Avail.Sto	rage Storage [	Description	
#1	312.0	0' 3,48	B0 cf Custom	Stage Data (Pri	smatic)Listed below (Recalc)
Elevation (feet)		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
312.00		1,182	0	0	
313.00		1,690	1,436	1,436	
314.00		2,398	2,044	3,480	
Device R	Routing	Invert	Outlet Devices	5	
#1 F	Primary	310.60'	24.0" Round	Culvert	
	•		L= 363.4' RC	P, square edge	headwall, Ke= 0.500
			Inlet / Outlet In	vert= 310.60 / 3	807.00' S= 0.0099 '/' Cc= 0.900 s & connections, Flow Area= 3.14 sf
<b>Primary OutElow</b> Max-0.56 atc. $(2.60 \text{ brg} + 1)/(-212.01!)$ T/(-207.77!) (Dynamic Tailwater)					

Primary OutFlow Max=9.56 cfs @ 12.60 hrs HW=312.01' TW=307.77' (Dynamic Tailwater) **1=Culvert** (Inlet Controls 9.56 cfs @ 4.04 fps)

#### Pond 2P-F: INLET POND - Frozen Conditions



#### Summary for Pond 24P: Roadside Swale - Frozen Conditions

Inflow Area =	0.761 ac, 0.00% Impervious, Inflow	Depth = 0.49" for 25-Year event
Inflow =	0.12 cfs @ 12.32 hrs, Volume=	0.031 af
Outflow =	0.04 cfs @ 14.62 hrs, Volume=	0.019 af, Atten= 68%, Lag= 138.3 min
Primary =	0.04 cfs @ 14.62 hrs, Volume=	0.019 af

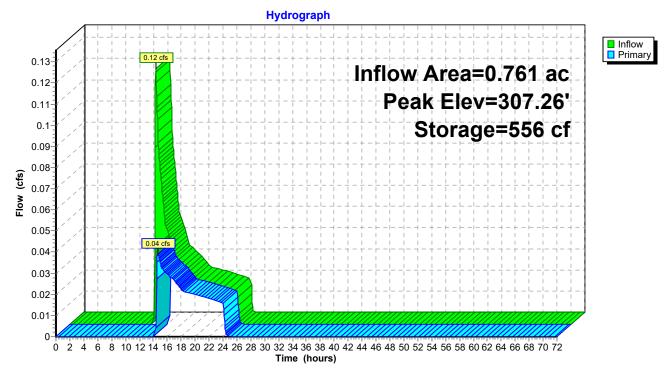
Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 307.26' @ 14.62 hrs Surf.Area= 866 sf Storage= 556 cf

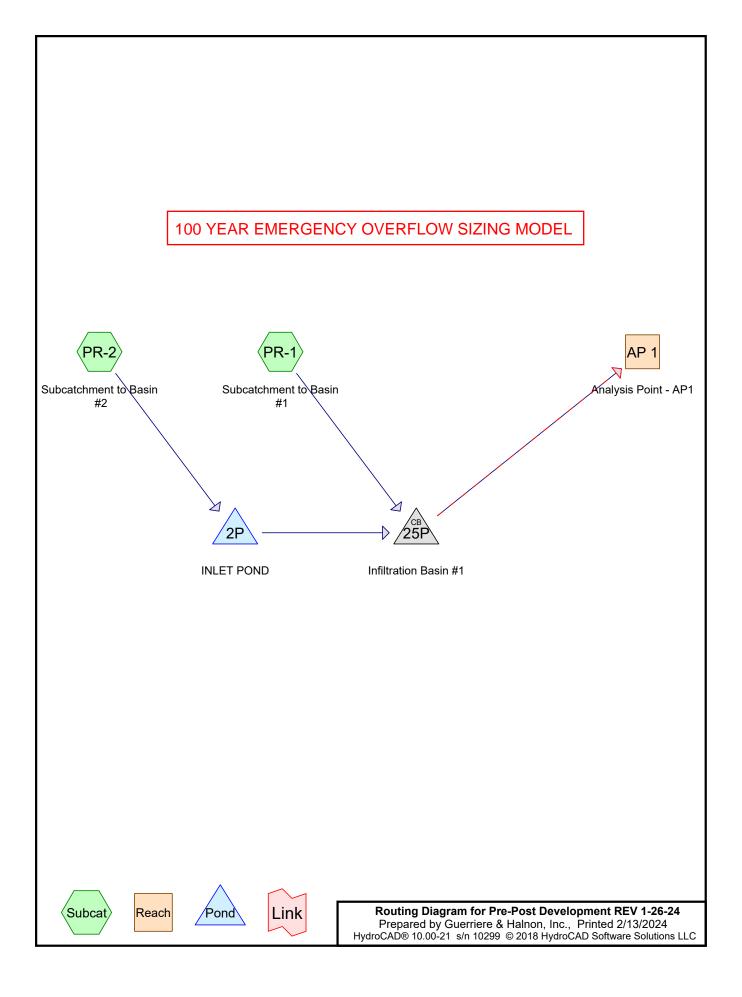
Plug-Flow detention time= 290.8 min calculated for 0.019 af (60% of inflow) Center-of-Mass det. time= 139.2 min (1,119.2 - 980.0)

Volume	Inv	ert Avail.Sto	orage Storage	e Description	
#1	306.	00' 1,3	65 cf Custon	n Stage Data (P	rismatic)Listed below (Recalc)
Elevatio (fee 306.0 307.0 308.0	51 50 50	Surf.Area (sq-ft) 0 700 1,330	Inc.Store (cubic-feet) 0 350 1,015	Cum.Store (cubic-feet) 0 350 1,365	
Device	Routing	Invert	Outlet Device	es	
#1	Primary	307.25'	Head (feet) ( 2.50 3.00 3.	0.20 0.40 0.60 .50 h) 2.54 2.61 2.	oad-Crested Rectangular Weir 0.80 1.00 1.20 1.40 1.60 1.80 2.00 61 2.60 2.66 2.70 2.77 2.89 2.88

**Primary OutFlow** Max=0.04 cfs @ 14.62 hrs HW=307.26' TW=0.00' (Dynamic Tailwater) **1=Broad-Crested Rectangular Weir**(Weir Controls 0.04 cfs @ 0.29 fps)

#### Pond 24P: Roadside Swale - Frozen Conditions





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Runoff by SCS TR	72.00 hrs, dt=0.05 hrs, 1441 points -20 method, UH=SCS, Weighted-CN method - Pond routing by Dyn-Stor-Ind method
SubcatchmentPR-1: Subcatchmentto	Runoff Area=141,517 sf   55.11% Impervious   Runoff Depth=5.35" Tc=6.0 min   CN=72   Runoff=21.07 cfs  1.448 af
SubcatchmentPR-2: Subcatchmentto Flow	Runoff Area=670,872 sf 0.00% Impervious Runoff Depth=2.83" Length=1,673' Tc=37.2 min CN=51 Runoff=23.64 cfs 3.632 af
Reach AP 1: Analysis Point - AP1	Inflow=29.39 cfs 5.050 af Outflow=29.39 cfs 5.050 af
Pond 2P: INLET POND Discarded=0.70 cfs 0	Peak Elev=316.66' Storage=3,480 cf Inflow=23.64 cfs 3.632 af 0.041 af Primary=25.79 cfs 3.591 af Outflow=26.49 cfs 3.632 af
Pond 25P: Infiltration Basin #1	Peak Elev=310.41' Inflow=29.22 cfs 5.039 af Outflow=29.22 cfs 5.039 af
Total Bunoff Aroa - 19 650	ac Bunoff Volume = 5.081 of Average Bunoff Depth = 3.27

Total Runoff Area = 18.650 acRunoff Volume = 5.081 afAverage Runoff Depth = 3.27"90.40% Pervious = 16.859 ac9.60% Impervious = 1.790 ac

NRCC 24-hr C 100-Year Rainfall=8.74" Pre-Post Development REV 1-26-24 Prepared by Guerriere & Halnon, Inc. HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD Software Solutions LLC

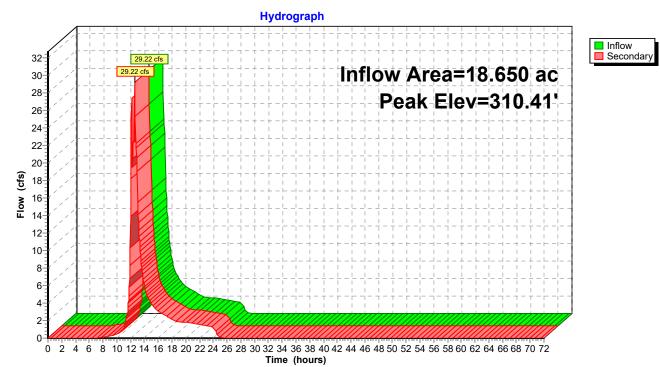
#### Summary for Pond 25P: Infiltration Basin #1

18.650 ac, 9.60% Impervious, Inflow Depth = 3.24" for 100-Year event Inflow Area = Inflow 29.22 cfs @ 12.60 hrs, Volume= = 5.039 af 29.22 cfs @ 12.60 hrs, Volume= 5.039 af, Atten= 0%, Lag= 0.0 min Outflow = Secondary = 29.22 cfs @ 12.60 hrs, Volume= 5.039 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 310.41'@ 12.60 hrs Flood Elev= 310.50'

Device	Routing	Invert	Outlet Devices
#1	Secondary	309.90'	<b>30.0' long x 10.0' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Secondary OutFlow Max=28.96 cfs @ 12.60 hrs HW=310.41' TW=0.00' (Dynamic Tailwater) =Broad-Crested Rectangular Weir (Weir Controls 28.96 cfs @ 1.89 fps)



#### Pond 25P: Infiltration Basin #1

Printed 2/13/2024

100 YEAR WEIR BYPASS MODEL

<u>Stage-Area-Storage Calculations</u> Appendix 5

NRCC 24-hr C 100-Year Rainfall=8.74" Printed 2/13/2024

Pre-Post Development REV 1-26-24NRCC 24Prepared by Guerriere & Halnon, Inc.HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD Software Solutions LLC

#### Stage-Area-Storage for Pond 2P: INLET POND

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
312.00	1,182	0
312.05	1,207	60
312.10	1,233	121
312.15	1,258	183
312.20	1,284	247
312.25	1,309	311
312.30	1,334	377
312.35	1,360	445
312.40	1,385	513
312.45	1,411	583
312.50 312.55	1,436 1,461	655 727
312.60	1,487	801
312.65	1,512	876
312.70	1,538	952
312.75	1,563	1,029
312.80	1,588	1,108
312.85	1,614	1,188
312.90	1,639	1,270
312.95	1,665	1,352
313.00 313.05	1,690	1,436 1,521
313.10	1,725 1,761	1,609
313.15	1,796	1,697
313.20	1,832	1,788
313.25	1,867	1,881
313.30	1,902	1,975
313.35	1,938	2,071
313.40	1,973	2,169
313.45	2,009	2,268
313.50	2,044	2,370
313.55 313.60	2,079 2,115	2,473 2,577
313.65	2,113	2,684
313.70	2,186	2,792
313.75	2,221	2,903
313.80	2,256	3,015
313.85	2,292	3,128
313.90	2,327	3,244
313.95	2,363	3,361
314.00	2,398	3,480

Pre-Post Development REV 1-26-24NRCC 24Prepared by Guerriere & Halnon, Inc.HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD Software Solutions LLC

#### Stage-Area-Storage for Pond 1P: Infiltration Basin #1

ElevationSurfaceHorizontalStorage(feet)(sq-ft)(cubic-feet)305.5010,45110,4510305.5610,56610,566631305.6210,68010,6801,268305.6810,79510,7951,912305.7410,91010,9102,563305.8011,02511,0253,221305.8611,13911,1393,886305.9211,2544,558305.9211,2544,558305.9311,36911,3695.9411,6056,615306.1011,60511,605306.1611,72411,7247,315306.2211,962306.2411,9628,736306.3412,08012,0809,457306.4012,19912,19912,19910,186306.6412,67512,675306.7612,91212,437306.7612,91214,706306.8213,03113,031306.7612,91214,706307.0013,38813,388307.1213,625307.2413,66313,663307.4814,33844,33814,33824,516307.4414,576307.6014,576307.6114,932307.7214,813307.7414,33844,33844,338307.7514,932307.7614,932307				-
305.50 $10,451$ $10,451$ $0$ $305.56$ $10,566$ $10,566$ $631$ $305.62$ $10,680$ $10,680$ $1,268$ $305.68$ $10,795$ $10,795$ $1,912$ $305.74$ $10,910$ $10,910$ $2,563$ $305.86$ $11,025$ $11,025$ $3,221$ $305.86$ $11,399$ $11,399$ $3,886$ $305.92$ $11,254$ $11,254$ $4,558$ $305.98$ $11,369$ $11,369$ $5,237$ $306.04$ $11,486$ $11,486$ $5,922$ $306.10$ $11,605$ $11,605$ $6,615$ $306.16$ $11,724$ $11,724$ $7,315$ $306.22$ $11,962$ $8,736$ $306.34$ $12,080$ $12,080$ $9,457$ $306.40$ $12,199$ $12,199$ $10,186$ $306.52$ $12,437$ $12,437$ $11,664$ $306.55$ $12,556$ $12,556$ $12,414$ $306.64$ $12,675$ $12,793$ $13,935$ $306.76$ $12,912$ $12,912$ $14,706$ $306.84$ $13,269$ $13,269$ $17,062$ $307.06$ $13,506$ $13,506$ $18,669$ $307.12$ $13,625$ $13,625$ $19,483$ $307.14$ $13,744$ $13,744$ $20,304$ $307.44$ $14,576$ $14,576$ $26,251$ $307.60$ $14,576$ $14,576$ $26,251$ $307.60$ $14,576$ $14,576$ $26,251$ $307.66$ $14,695$ $27,129$ $307$				
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305.68 $10,795$ $10,795$ $1,912$ $305.74$ $10,910$ $10,910$ $2,563$ $305.86$ $11,025$ $11,025$ $3,221$ $305.86$ $11,369$ $11,139$ $3,886$ $305.92$ $11,254$ $11,254$ $4,558$ $305.98$ $11,369$ $11,369$ $5,237$ $306.04$ $11,486$ $11,486$ $5,922$ $306.10$ $11,605$ $11,605$ $6,615$ $306.16$ $11,724$ $11,724$ $7,315$ $306.22$ $11,843$ $11,843$ $8,022$ $306.28$ $11,962$ $11,962$ $8,736$ $306.34$ $12,080$ $12,080$ $9,457$ $306.40$ $12,199$ $12,199$ $10,186$ $306.52$ $12,437$ $12,437$ $11,664$ $306.56$ $12,556$ $12,556$ $12,414$ $306.56$ $12,556$ $12,556$ $12,414$ $306.70$ $12,793$ $12,793$ $13,935$ $306.76$ $12,912$ $12,912$ $14,706$ $306.82$ $13,031$ $13,031$ $15,484$ $306.84$ $13,506$ $13,506$ $18,669$ $307.12$ $13,625$ $13,625$ $19,483$ $307.14$ $13,744$ $13,744$ $20,304$ $307.24$ $13,883$ $14,338$ $24,516$ $307.42$ $14,457$ $14,457$ $25,380$ $307.42$ $14,932$ $14,932$ $28,906$ $307.76$ $14,576$ $14,576$ $26,251$ $307.60$ $15,787$ $15,7$				
305.74 $10.910$ $2.563$ $305.80$ $11.025$ $11.025$ $3.221$ $305.86$ $11.139$ $11.139$ $3.886$ $305.92$ $11.254$ $11.254$ $4.558$ $305.92$ $11.254$ $11.254$ $4.558$ $305.98$ $11.369$ $5.237$ $306.04$ $11.486$ $11.486$ $5.922$ $306.10$ $11.605$ $11.605$ $6.615$ $306.16$ $11.724$ $11.724$ $7.315$ $306.22$ $11.843$ $11.843$ $8.022$ $306.34$ $12.080$ $2.080$ $9.457$ $306.40$ $12.199$ $12.199$ $10.186$ $306.46$ $12.318$ $12.318$ $10.921$ $306.52$ $12.2437$ $12.437$ $11.664$ $306.52$ $12.256$ $12.556$ $12.414$ $306.64$ $12.675$ $12.675$ $13.171$ $306.70$ $12.793$ $12.793$ $13.935$ $306.76$ $12.912$ $12.912$ $14.706$ $306.82$ $13.031$ $13.031$ $15.484$ $306.84$ $13.269$ $13.269$ $17.062$ $307.00$ $13.388$ $13.388$ $17.862$ $307.18$ $13.744$ $13.744$ $20.304$ $307.24$ $13.863$ $13.863$ $21.132$ $307.48$ $14.338$ $14.338$ $24.516$ $307.72$ $14.813$ $14.813$ $28.014$ $307.74$ $14.992$ $14.995$ $27.129$ $307.754$ $14.992$ $14.932$ $28.906$ <t< td=""><td></td><td></td><td></td><td></td></t<>				
305.80 $11,025$ $11,025$ $3,221$ $305.86$ $11,139$ $11,139$ $3,886$ $305.92$ $11,254$ $11,254$ $4,558$ $305.98$ $11,369$ $11,369$ $5,237$ $306.04$ $11,486$ $11,486$ $5,922$ $306.10$ $11,605$ $11,605$ $6,615$ $306.16$ $11,724$ $11,724$ $7,315$ $306.22$ $11,843$ $11,843$ $8,022$ $306.28$ $11,962$ $11,962$ $8,736$ $306.40$ $12,199$ $12,199$ $10,186$ $306.40$ $12,199$ $12,199$ $10,186$ $306.46$ $12,318$ $12,556$ $12,556$ $12,556$ $12,556$ $12,414$ $306.670$ $12,793$ $12,793$ $13,935$ $306.76$ $12,912$ $12,912$ $14,706$ $306.82$ $13,031$ $15,484$ $306.88$ $13,150$ $13,150$ $16,270$ $306.94$ $13,269$ $13,269$ $17,062$ $307.00$ $13,388$ $13,863$ $21,132$ $307.12$ $13,625$ $13,625$ $19,483$ $307.14$ $13,744$ $3,744$ $20,304$ $307.24$ $13,863$ $13,863$ $21,132$ $307.30$ $13,982$ $13,982$ $21,967$ $307.42$ $14,457$ $14,457$ $25,380$ $307.44$ $14,576$ $14,576$ $26,251$ $307.66$ $14,695$ $14,695$ $27,129$ $307.76$ $14,576$ $14,576$ $26,251$ <				
305.86 $11,139$ $11,139$ $3,886$ $305.92$ $11,254$ $11,254$ $4,558$ $305.98$ $11,369$ $11,369$ $5,237$ $306.04$ $11,486$ $11,486$ $5,922$ $306.10$ $11,605$ $11,605$ $6,615$ $306.16$ $11,724$ $11,724$ $7,315$ $306.22$ $11,843$ $11,843$ $8,022$ $306.28$ $11,962$ $11,962$ $8,736$ $306.34$ $12,080$ $9,457$ $306.40$ $12,199$ $12,199$ $10,186$ $306.46$ $12,318$ $12,318$ $10,921$ $306.52$ $12,437$ $12,437$ $11,664$ $306.58$ $12,556$ $12,556$ $12,414$ $306.64$ $12,675$ $12,675$ $13,171$ $306.76$ $12,912$ $12,912$ $14,706$ $306.82$ $13,031$ $13,031$ $15,484$ $306.82$ $13,031$ $13,031$ $15,484$ $306.88$ $13,150$ $13,150$ $16,270$ $307.00$ $13,388$ $13,388$ $17,862$ $307.06$ $13,506$ $13,606$ $18,669$ $307.12$ $13,625$ $13,625$ $19,483$ $307.14$ $13,744$ $3,744$ $20,304$ $307.24$ $13,863$ $13,863$ $21,132$ $307.60$ $14,576$ $14,576$ $26,251$ $307.66$ $14,695$ $27,129$ $307.72$ $14,813$ $14,813$ $28,014$ $307.74$ $14,932$ $14,932$ $28,906$ <t< td=""><td></td><td></td><td></td><td></td></t<>				
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305.98 $11,369$ $11,369$ $5,237$ $306.04$ $11,486$ $11,486$ $5,922$ $306.10$ $11,605$ $11,605$ $6,615$ $306.16$ $11,724$ $11,724$ $7,315$ $306.22$ $11,843$ $11,843$ $8,022$ $306.28$ $11,962$ $11,962$ $8,736$ $306.40$ $12,199$ $12,199$ $10,186$ $306.40$ $12,199$ $12,199$ $10,186$ $306.46$ $12,318$ $12,318$ $10,921$ $306.52$ $12,437$ $12,437$ $11,664$ $306.58$ $12,556$ $12,556$ $12,414$ $306.64$ $12,675$ $12,675$ $13,171$ $306.76$ $12,912$ $12,9912$ $14,706$ $306.82$ $13,031$ $13,031$ $15,484$ $306.88$ $13,150$ $13,150$ $16,270$ $306.94$ $13,269$ $13,269$ $17,662$ $307.06$ $13,506$ $13,506$ $18,669$ $307.12$ $13,625$ $13,625$ $19,483$ $307.18$ $13,744$ $13,744$ $20,304$ $307.24$ $13,863$ $21,132$ $307.30$ $13,982$ $13,982$ $21,967$ $307.66$ $14,695$ $14,695$ $27,129$ $307.48$ $14,338$ $14,338$ $24,516$ $307.48$ $14,932$ $14,932$ $28,906$ $307.48$ $14,932$ $14,932$ $28,906$ $307.66$ $14,695$ $14,695$ $27,129$ $307.72$ $14,813$ $14,813$ <t< td=""><td></td><td></td><td></td><td></td></t<>				
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306.10 $11,605$ $11,605$ $6,615$ $306.16$ $11,724$ $11,724$ $7,315$ $306.22$ $11,843$ $11,843$ $8,022$ $306.28$ $11,962$ $11,962$ $8,736$ $306.34$ $12,080$ $12,080$ $9,457$ $306.40$ $12,199$ $12,199$ $10,186$ $306.46$ $12,318$ $12,318$ $10,921$ $306.52$ $12,437$ $12,437$ $11,664$ $306.58$ $12,556$ $12,556$ $12,414$ $306.64$ $12,675$ $13,171$ $306.70$ $12,793$ $12,793$ $13,935$ $306.76$ $12,912$ $12,912$ $14,706$ $306.82$ $13,031$ $13,031$ $15,484$ $306.88$ $13,150$ $13,150$ $16,270$ $306.94$ $13,269$ $13,269$ $17,062$ $307.00$ $13,388$ $13,388$ $17,862$ $307.12$ $13,625$ $13,625$ $19,483$ $307.12$ $13,625$ $13,625$ $19,483$ $307.14$ $13,744$ $13,744$ $23,569$ $307.24$ $13,863$ $13,863$ $21,132$ $307.30$ $13,982$ $13,982$ $21,967$ $307.48$ $14,338$ $14,338$ $24,516$ $307.54$ $14,457$ $14,457$ $25,380$ $307.66$ $14,695$ $27,129$ $307.72$ $14,813$ $14,813$ $28,906$ $307.90$ $15,170$ $15,170$ $30,713$ $307.66$ $14,695$ $14,695$ $27,129$ </td <td></td> <td></td> <td></td> <td></td>				
306.16 $11,724$ $11,724$ $7,315$ $306.22$ $11,843$ $11,843$ $8,022$ $306.28$ $11,962$ $11,962$ $8,736$ $306.34$ $12,080$ $12,080$ $9,457$ $306.40$ $12,199$ $12,199$ $10,186$ $306.46$ $12,318$ $12,318$ $10,921$ $306.52$ $12,437$ $12,437$ $11,664$ $306.52$ $12,437$ $12,437$ $11,664$ $306.64$ $12,675$ $12,675$ $13,171$ $306.70$ $12,793$ $12,793$ $13,935$ $306.76$ $12,912$ $12,912$ $14,706$ $306.82$ $13,031$ $13,031$ $15,484$ $306.88$ $13,150$ $13,150$ $16,270$ $306.94$ $13,269$ $13,269$ $17,062$ $307.06$ $13,506$ $13,506$ $18,669$ $307.12$ $13,625$ $13,625$ $19,483$ $307.18$ $13,744$ $13,744$ $20,304$ $307.24$ $13,863$ $13,863$ $21,132$ $307.30$ $13,982$ $13,982$ $21,967$ $307.42$ $14,219$ $14,219$ $23,659$ $307.44$ $14,576$ $14,576$ $26,251$ $307.66$ $14,695$ $14,695$ $27,129$ $307.72$ $14,813$ $14,4813$ $28,016$ $307.78$ $14,932$ $14,932$ $28,906$ $307.78$ $14,932$ $14,932$ $28,906$ $307.84$ $15,535$ $15,535$ $33,476$ $308.08$ $15,535$				
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306.28 $11,962$ $11,962$ $8,736$ $306.34$ $12,080$ $12,080$ $9,457$ $306.40$ $12,199$ $12,199$ $10,186$ $306.46$ $12,318$ $12,318$ $10,921$ $306.52$ $12,437$ $12,437$ $11,664$ $306.58$ $12,556$ $12,556$ $12,414$ $306.64$ $12,675$ $12,675$ $13,171$ $306.70$ $12,793$ $12,793$ $13,935$ $306.76$ $12,912$ $12,912$ $14,706$ $306.82$ $13,031$ $13,031$ $15,484$ $306.88$ $13,150$ $13,150$ $16,270$ $306.94$ $13,269$ $13,269$ $17,062$ $307.00$ $13,388$ $13,388$ $17,862$ $307.00$ $13,506$ $13,506$ $18,669$ $307.12$ $13,625$ $13,625$ $19,483$ $307.18$ $13,744$ $13,744$ $20,304$ $307.24$ $13,863$ $13,863$ $21,132$ $307.36$ $14,100$ $14,100$ $22,810$ $307.42$ $14,219$ $14,219$ $23,659$ $307.48$ $14,338$ $14,338$ $24,516$ $307.66$ $14,695$ $27,129$ $307.72$ $14,813$ $14,813$ $28,014$ $307.78$ $14,932$ $14,932$ $28,906$ $307.84$ $15,051$ $15,535$ $33,476$ $308.02$ $15,787$ $15,787$ $35,355$ $308.08$ $15,535$ $15,535$ $33,476$ $308.14$ $15,661$ $14,612$ <td></td> <td></td> <td></td> <td></td>				
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$\begin{array}{cccccccccccccccccccccccccccccccccccc$	306.64	12,675	12,675	13,171
306.82 $13,031$ $13,031$ $15,484$ $306.88$ $13,150$ $13,150$ $16,270$ $306.94$ $13,269$ $13,269$ $17,062$ $307.00$ $13,388$ $13,388$ $17,862$ $307.06$ $13,506$ $13,506$ $18,669$ $307.12$ $13,625$ $13,625$ $19,483$ $307.18$ $13,744$ $13,744$ $20,304$ $307.24$ $13,863$ $21,132$ $307.30$ $13,982$ $13,982$ $21,967$ $307.36$ $14,100$ $14,100$ $22,810$ $307.42$ $14,219$ $14,219$ $23,659$ $307.48$ $14,338$ $14,338$ $24,516$ $307.54$ $14,457$ $14,457$ $25,380$ $307.60$ $14,576$ $14,576$ $26,251$ $307.66$ $14,695$ $14,695$ $27,129$ $307.72$ $14,813$ $14,813$ $28,906$ $307.96$ $15,289$ $15,051$ $29,806$ $307.96$ $15,289$ $15,289$ $31,626$ $308.02$ $15,410$ $15,410$ $32,547$ $308.08$ $15,535$ $15,535$ $33,476$ $308.14$ $15,661$ $34,412$ $308.20$ $15,787$ $15,787$ $35,355$ $308.26$ $15,912$ $15,912$ $36,306$ $308.32$ $16,038$ $16,038$ $37,264$ $308.44$ $16,289$ $16,289$ $39,204$ $308.50$ $16,415$ $16,415$ $40,185$	306.70	12,793	12,793	13,935
306.88 $13,150$ $13,150$ $16,270$ $306.94$ $13,269$ $13,269$ $17,062$ $307.00$ $13,388$ $13,388$ $17,862$ $307.06$ $13,506$ $13,506$ $18,669$ $307.12$ $13,625$ $13,625$ $19,483$ $307.18$ $13,744$ $13,744$ $20,304$ $307.24$ $13,863$ $21,132$ $307.30$ $13,982$ $13,982$ $21,967$ $307.36$ $14,100$ $14,100$ $22,810$ $307.42$ $14,219$ $14,219$ $23,659$ $307.48$ $14,338$ $14,338$ $24,516$ $307.54$ $14,457$ $14,457$ $25,380$ $307.60$ $14,576$ $14,576$ $26,251$ $307.66$ $14,695$ $14,695$ $27,129$ $307.72$ $14,813$ $14,813$ $28,906$ $307.96$ $15,289$ $15,051$ $29,806$ $307.90$ $15,170$ $15,170$ $30,713$ $307.96$ $15,289$ $15,289$ $31,626$ $308.02$ $15,410$ $15,410$ $32,547$ $308.08$ $15,535$ $15,535$ $33,476$ $308.20$ $15,787$ $15,787$ $35,355$ $308.26$ $15,912$ $15,912$ $36,306$ $308.32$ $16,038$ $16,038$ $37,264$ $308.34$ $16,289$ $16,289$ $39,204$ $308.50$ $16,415$ $16,415$ $40,185$	306.76			
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308.50 16,415 16,415 40,185	308.38	16,164	16,164	
	308.44		16,289	39,204
308.56 16,540 16,540 41,174	308.50			
	308.56	16,540	16,540	41,174

Pre-Post Development REV 1-26-24NRCC 24Prepared by Guerriere & Halnon, Inc.HydroCAD® 10.00-21 s/n 10299 © 2018 HydroCAD Software Solutions LLC

#### Stage-Area-Storage for Pond 1P: Infiltration Basin #1 (continued)

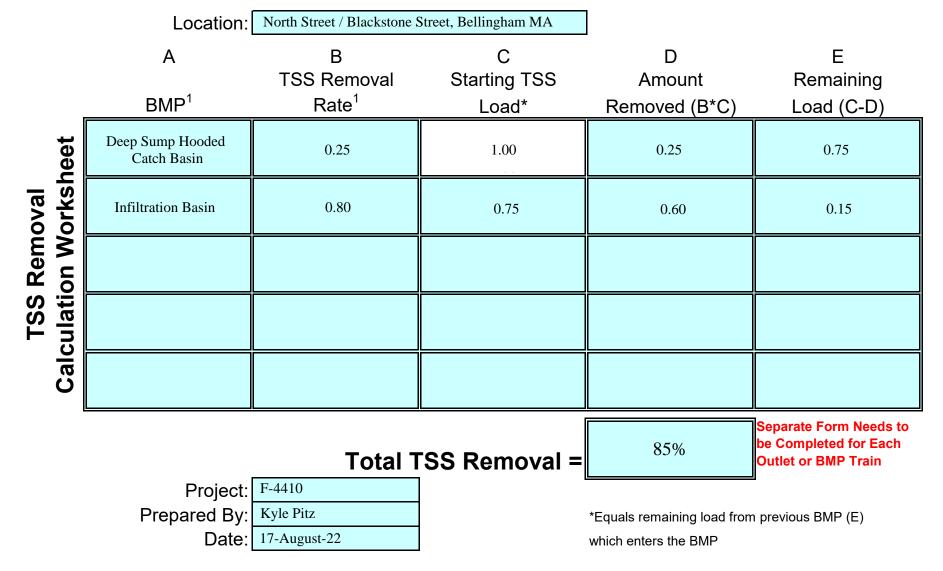
Elevation	Surface	Horizontal	Storage
(feet)	(sq-ft)	(sq-ft)	(cubic-feet)
308.62	16,666	16,666	42,170
308.68	16,792	16,792	43,174
308.74	16,917	16,917	44,185
308.80	17,043	17,043	45,204
308.86	17,168	17,168	46,230
308.92	17,294	17,294	47,264
308.98	17,420	17,420	48,305
309.04	17,545	17,545	49,354
309.10	17,671	17,671	50,411
309.16	17,796	17,796	51,475
309.22	17,922	17,922	52,546
309.28	18,048	18,048	53,626
309.34	18,173	18,173	54,712
309.40	18,299	18,299	55,806
309.46	18,425	18,425	56,908
309.52	18,550	18,550	58,017
309.58	18,676	18,676	59,134
309.64	18,801	18,801	60,258
309.70	18,927	18,927	61,390
309.76	19,053	19,053	62,530
309.82	19,178	19,178	63,677
309.88	19,304	19,304	64,831
309.94	19,429	19,429	65,993
310.00	19,555	19,555	67,163
310.06	19,685	19,685	68,340
310.12	19,815	19,815	69,525
310.18	19,945	19,945	70,717
310.24	20,074	20,074	71,918
310.30	20,204	20,204	73,126
310.36	20,334	20,334	74,343
310.42	20,464	20,464	75,566
310.48	20,594	20,594	76,798
310.54	20,637	20,637	78,036
310.60	20,637	20,637	79,274
310.66	20,637	20,637	80,512
310.72	20,637	20,637	81,751
310.78	20,637	20,637	82,989
310.84	20,637	20,637	84,227
310.90	20,637	20,637	85,465
310.96	20,637	20,637	86,704

# <u>TSS Removal Worksheet</u> Appendix 6

INSTRUCTIONS:

1. Sheet is nonautomated. Print sheet and complete using hand calculations. Column A and B: See MassDEP Structural BMP Table

- 2. The calculations must be completed using the Column Headings specified in Chart and Not the Excel Column Headings
- 3. To complete Chart Column D, multiple Column B value within Row x Column C value within Row
- 4. To complete Chart Column E value, subtract Column D value within Row from Column C within Row
- 5. Total TSS Removal = Sum All Values in Column D



INSTRUCTIONS:

1. Sheet is nonautomated. Print sheet and complete using hand calculations. Column A and B: See MassDEP Structural BMP Table

- 2. The calculations must be completed using the Column Headings specified in Chart and Not the Excel Column Headings
- 3. To complete Chart Column D, multiple Column B value within Row x Column C value within Row

-

- 4. To complete Chart Column E value, subtract Column D value within Row from Column C within Row
- 5. Total TSS Removal = Sum All Values in Column D

	Location: North Street / Blackstone Street, Bellingham MA				
	А	В	С	D	E
	BMP <sup>1</sup>	TSS Removal Rate <sup>1</sup>	Starting TSS Load*	Amount Removed (B*C)	Remaining Load (C-D)
neet	Deep Sump Hooded Catch Basin	0.25	1.00	0.25	0.75
moval Worksheet	Sediment Forebay	0.25	0.75	0.19	0.56
<b>D</b>					
TSS Re Calculation					
Calc					
Ľ			atment 'SS Removal =	44%	Separate Form Needs to be Completed for Each Outlet or BMP Train
	Project: Prepared By: Date:			*Equals remaining load from which enters the BMP	previous BMP (E)

**Long Term Operation and Maintenance Plan** Appendix 7 The following shall serve as the (O&M) Plan required by Standard 9, as well as the Long-Term Pollution Prevention Plan required by Standard 4.

A. <u>Names of Persons or Entity Responsible for Plan Compliance</u> Applicant: Raven Homes, Inc. 22 Buckhill Road Northborough, MA 01532 PH: 508-393-4511

B. <u>Stormwater Management System Owner</u> Owner: Raven Homes, Inc.

Raven Homes, Inc. 22 Buckhill Road Northborough, MA 01532 PH: 508-393-4511

- C. <u>Good housekeeping practices</u>
  - 1. Maintain site, landscaping and vegetation.
  - 2. Sweep and pick up litter on pavements and grounds.
  - 3. Deliveries shall be monitored by owners or representative to ensure that if any spillage occurs, it shall be contained and cleaned up immediately.
  - 4. Maintain pavement and curbing in good repair.
- D. Requirements for routine inspections and maintenance of stormwater BMPs
  - 1. Plans: The stormwater Operation and Maintenance Plan shall consist of all Plans, documents and all local state and federal approvals as required for the subject property.
  - 2. Record Keeping:
    - a. Maintain a log of all operation and maintenance activities for at least three years following construction, including inspections, repairs, replacement and disposal (for disposal, the log shall indicate the type of material and the disposal location).
    - b. Make this log available to MassDEP and the Conservation Commission upon request; and
    - c. Allow MassDEP and the Conservation Commission to inspect each BMP to determine whether the responsible party is implementing the Operation and Maintenance Plan.
  - 3. Descriptions and Designs: The Best Management Practices (BMP) incorporated into the design include the following.
    - a. Street Sweeping Stipulated within the Construction Period Pollution Prevention Plan, the Long-Term Pollution Prevention Plan, and the Operation and Maintenance Plan. As the amount of TSS removal is discretionary, no credit was taken within the calculations for this BMP.
    - b. Deep sump catch basins with hoods installed to promote TSS Removal of solids and control floatable pollutants. This BMP has a design rate of 25% TSS Removal.
    - c. Infiltration basin and sediment forebay provided to promote the required 80% TSS Removal. Refer to TSS Removal Worksheet in Standard 4 for treatment train.
    - d. Safety Fencing: Provide 6-FT high chain link fence with lockable gates around detention basin for public safety.
    - e. Spill Containment Kit to contain and clean-up spills that could occur on site.

- 4. BMP Maintenance: After construction it is the responsibility of the owner to perform maintenance. The cleaning of the components of the stormwater management system shall generally be as follows:
  - a. Roadway: The owner shall keep the roadway swept with a mechanical sweeper or hand swept semi-annually at a minimum.
  - b. Catch Basins: Shall be cleaned by excavating, pumping or vacuuming four times per year and at the end of foliage and snow removal seasons. The sediment shall be disposed of off-site by the Owner. Inspect quarterly, remove silt when <sup>1</sup>/<sub>4</sub> full.
  - c. Infiltration Basin: Preventative maintenance shall be performed at least twice per year. Inspection shall be performed after every major storm for the first three months and twice a year thereafter and when there are discharges through the high outlet orifice. Mowing of the buffer area, and bottom of basin; removal of trash and debris; removal of grass clippings and organic matter to be performed at least twice per year. Pretreatment devices shall be inspected every other month and a least twice a year and after every major storm event.
- 5. Access Provisions: All of the components of the storm water system shall be accessible by the Owner
- E. <u>Spill prevention and response plans</u>
  - 1. Inventory materials to be present on-site during construction.
  - 2. Train employees and subcontractors in prevention and clean up procedures.
  - 3. All materials stored on site will be stored in their appropriate containers under a roof.
  - 4. Follow manufacturers recommendation for disposal of used containers.
  - 5. Store only enough product on site to do the job.
  - 6. On site equipment, fueling and maintenance measures:
    - a. Inspect on-site vehicles and equipment daily for leaks.
      - b. Conduct all vehicle and equipment maintenance and refueling in one location, away from storm drains.
      - c. Perform major repairs and maintenance off site.
    - d. Use drip pans, drip cloths or absorbent pads when replacing spent fuels.
    - e. Collect spent fuels and remove from site.
  - 7. Clean up spills.
    - a. Never hose down "dirty" pavement or impermeable surfaces where fluids have spilled. Use dry clean up methods (sawdust, cat litter and/or rags and absorbent pads).
    - b. Sweep up dry materials immediately. Never wash them away or bury them.
    - c. Clean up spills on dirt areas by digging up and properly disposing of contaminated soil.
    - d. Report significant spills to the Fire Department, Conservation Commission and Board of Health.
- F. <u>Provisions for maintenance of lawns, gardens, and other landscaped areas</u> Use only organic fertilizer. Dispose of clippings outside of the 100-foot buffer zone to the adjacent wetland.
- G. <u>Requirements for storage and use of herbicides, and pesticides</u> The application of herbicides or pesticides will be done by professional certified contractor.
- H. <u>Provisions for operation and management of septic system</u> Site to be serviced by private on-site sewer.

I. <u>Requirements for handling of pet waste</u>

Pet waste should never be dumped or washed into the local storm drain system. Waste shall be picked up immediately and placed in bags and properly disposed of in the garbage to be collected and taken to a landfill.

J. <u>Provisions for washing of vehicles</u>

Washing of vehicles shall be done in an area as to eliminate wash water from being directly discharged to the local storm drain system. Vehicles should be washed in areas where wash water can be held prior to discharging to the sanitary sewer system or in areas where infiltration precludes runoff to storm drains. Avoid using detergents whenever possible.

- K. Provisions for solid waste management
  - 1. <u>Waste Management Plan</u>
    - a. Recycle materials whenever possible (paper, plaster cardboard, metal cans). Separate containers for material are recommended.
    - b. Do not bury waste and debris on site.
    - c. Certified haulers will be hired to remove the dumpster container waste as needed. Recycling products will also be removed off site weekly.
- L. <u>Snow disposal and plowing plans relative to Wetland Resource Areas</u> Snow storage is adequate around the site for large storm events. Storage of snow shall not be placed directly near areas adjacent to the proposed infiltration basin.
- M. <u>Winter Road Salt and/or Sand Use and Storage restrictions</u> No sand, salt, or chemicals for de-icing will be stored outside.
- N. Street sweeping schedules

Sweeping, the act of cleaning pavement can be done by mechanical sweepers, vacuum sweeper or hand sweeper. The quantity of sand is a direct correlation with the treatment of ice and snow and the types of chemicals and spreaders that are being used on site to manage snow. If a liquid de-icer such as calcium chloride is used as a pretreatment to new events the amount of sand is minimized. Sweeping for this site should be done semi-annually at a minimum. Collecting the particulate before it enters the catch basins is cheaper and more environmentally friendly than in a catch basin mixing with oils and greases in the surface water runoff in catch basins.

- O. <u>Provisions for prevention of illicit discharges to the stormwater management system</u> The discharge into the stormwater system is not being violated, see attachment for illicit discharges compliance.
- P. <u>Training the staff or personnel involved with implementing Long-Term Pollution Prevention</u> <u>Plan</u>

The owner shall develop policies and procedures for containing the illicit spilling of oils, soda, beer, paper and litter. These wastes provide a degrading of the water quality. The placement of signs and trash barrels with lids around the site would contribute to a clean water quality site condition.

Q. List of Emergency contacts for implementing Long-Term Pollution Prevention Plan:

Raven Homes, Inc. 22 Buckhill Road Northborough, MA 01532 PH: 508-393-4511

This shall be the contact until such time as the project is sold.

#### R. Estimated BMP Maintenance Costs

The following prices are estimates of the costs associated with maintenance of the proposed site BMPs. Costs provided are only estimates and may not reflect actual costs to perform the work. Actual costs may vary depending on company/personnel performing the work. Actual costs may increase over time.

#### <u>BMP</u>

Pavement sweeping Catch basin cleaning Infiltration Basin Spill Containment Kit Estimated Maintenance Cost \$ 400 per year \$ 200 per catch basin per cleaning \$ 200 per cleaning \$ 750 purchase price **Construction Period Pollution Prevention Plan** Appendix 8 Construction Period Pollution Prevention Plan and Erosion and Sedimentation Control. EPA NPDES – Storm Water Pollution Prevention Plan (SWPPP)

A. <u>Names of Persons or Entity Responsible for Plan Compliance</u> Applicant: Raven Homes, Inc. 22 Buckhill Road Northborough, MA 01532

PH: 508-393-4511

#### B. <u>Construction Period Pollution Prevention Measures</u>

- 1. Inventory materials to be present on-site during construction.
- 2. Train employees and subcontractors in prevention and clean up procedures.
- 3. All materials stored on site will be stored in their appropriate containers and if possible, under a roof or covered.
- 4. Follow manufacturer's recommendation for disposal of used containers.
- 5. Store only enough product on site to do the job.
- 6. On site equipment, fueling and maintenance measures:
  - a. Inspect on-site vehicles and equipment daily for leaks.
  - b. Conduct all vehicle and equipment maintenance and refueling in front of building, away from storm drains.
  - c. Perform major repairs and maintenance off site.
  - d. Use drip pans, drip cloths or absorbent pads when replacing spent fuels.
  - e. Collect spent fuels and remove from site, per Local and State regulations.
  - f. Maintain a clean construction entrance where truck traffic is frequent to reduce soil compaction constant sweeping is required and limit tracking of sediment into streets, sweeping street when silt is observed on street.
- 7. Stockpile materials and maintain Erosion Control around the materials where it can easily be accessed. Maintain easy access to clean up materials to include brooms, mops, rags gloves, goggles, sand, sawdust, plastic and metal trash containers.
- 8. Clean up spills.
  - a. Never hose down "dirty" pavement or impermeable surfaces where fluids have spilled. Use dry clean up methods (sawdust, cat litter and/or rags/absorbent pads).
  - b. Sweep up dry materials immediately. Never wash them away or bury them.
  - c. Clean up spills on dirt areas by digging up and properly disposing of contaminated soil in a certified container and notify a certified hauler for removal.
  - d. Report significant spills to the Fire Department.
- 9. It is the responsibility of the site superintendent or employees designated by the Applicant to inspect erosion control and repair as needed, also to inspect all on site vehicles for leaks and check all containers on site that may contain hazardous materials daily.
- C. <u>Erosion and Sedimentation Control Plan.</u> Erosion Control Plan prepared by Guerriere & Halnon, Inc. Dated 12/30/22 revised 02/13/2024
- D. <u>Site Development Plans</u>. See Site Plan prepared by Guerriere & Halnon, Inc. Dated 12/30/22 and revised through 02/13/2024
- E. <u>Construction Plans</u> See Site Plan prepared by Guerriere & Halnon, Inc. Dated 12/30/22 and revised through 02/13/2024

- 1. Construction
  - a. Record Order of Conditions The site superintendent shall be aware of all the Conditions contained within the Order including inspection schedules.
  - b. Install DEP File # Sign.
  - c. Prior to any work on the site including tree/brush clearing, the approved limit of clearing as well as the location of the proposed erosion control devices (such as silt fence/mulch sock, etc.) must be staked on the ground under the direction of a Massachusetts registered Professional Land Surveyor.
  - d. Install silt fence/mulch sock at locations shown on Erosion Control Plan
  - e. Strip off top and subsoil. Stockpile material to be reused away from the wetland, remove excess material from the site. Install and maintain erosion control barrier around stockpile.
  - f. Rough grade site, maintaining a temporary low area/sediment trap away from the wetland.
  - g. Construct drainage outfalls and stilling basin. Stabilize side slopes with loam, seed and mulch.
  - h. Install underground utilities; protect all open drainage structures with erosion/siltation control devices.
  - i. Install binder course of bituminous asphalt.
  - j. Install wearing course of asphalt, and striping (where required).
  - k. Maintain all erosion control devices until site is stabilized and a Certificate of Compliance is issued by the Conservation Commission.
  - 1. The Contractor shall be responsible to schedule any required inspections of his/her work.
- F. Construction Waste Management Plan
  - a. Dumpster for trash and bulk waste collection shall be provided separately for construction.
  - b. Recycle materials whenever possible (paper, plaster cardboard, metal cans). Separate containers for material are recommended.
  - c. Segregate and provide containers for disposal options for waste.
  - d. Do not bury waste and debris on site.
  - e. Certified haulers will be hired to remove the dumpster container waste as needed. Recycling products will also be removed off site weekly.
  - f. The sewer system is only for disposal of human waste, and substances permitted for disposal in the site sewer permit with the Town B.O.H.

#### G. Operation and Maintenance of Erosion and Sedimentation Controls

- The operation and maintenance of sedimentation control shall be the responsibility of the contractor. The inspection and maintenance of the stormwater component shall be performed as noted below. The contractor shall have erosion control in place at all times. The contractor, based on future weather reports, shall prepare and inspect all erosion control devices; cleaning, repairing and upgrading is a priority so that the devices perform as per design. Inspect the site during rain events. Do not stay away from the site. At a minimum there should be inspection to assure the devices are not clogged or plugged, or that devices have not been destroyed or damaged during the rain event. After a storm event inspection is required to clean and repair any damage components. Immediate repair is required.
- H. Inspection and Maintenance Schedules
  - 1. Inspection must be conducted at least once every 7 days and within 24 hours of the end of a storm event 0.5 inches or greater.

- 2. Inspection frequency can be reduced to once a month if:
  - a. The site is temporarily stabilized.
  - b. Runoff is unlikely due to winter conditions when site is covered with snow or ice.
- 3. Inspections must be conducted by qualified personnel, "qualified personnel" means a person knowledgeable in the principles and practice of erosion and sediment controls and who possess the skills to assess the conditions and take measures to maintain and ensure proper operation, also to conclude if the erosion control methods selected are effective.
- 4. For each inspection, the inspection report must include: (See attached inspection and maintenance log)
  - a. The inspection date.
  - b. Names, titles of personnel making the inspection.
  - c. Weather information for the period since the last inspection.
  - d. Weather information at the time of the inspection.
  - e. Locations of discharges of sediment from the site, if any.
  - f. Locations of BMP's that need to be maintained.
  - g. Locations where additional BMP's may be required.
  - h. Corrective action required or any changes to the SWPPP that may be necessary.
- 5. The owner, or their representative, such as the contractor, shall inspect the following inplace work.

Inspection Schedule:	
Erosion Control	Weekly
Catch Basins	Weekly
Temporary Sedimentation Traps/Basins	Weekly
Street Sweeping	Weekly

Please Note: Special inspections shall also be made after a significant rainfall event.

Maintenance Schedule	
Erosion Control Devices Failure	Immediately
Catch Basins	Sump 1/4 full of sediment
Street Sweeping	14 days minimum and prior to any
	significant rain event.

Please Note: Special maintenance shall also be made after a significant rainfall event.

I. <u>Inspection and Maintenance Log Form</u>. (Log Form Follows)

<u>Illicit Discharge Statement</u> Appendix 9

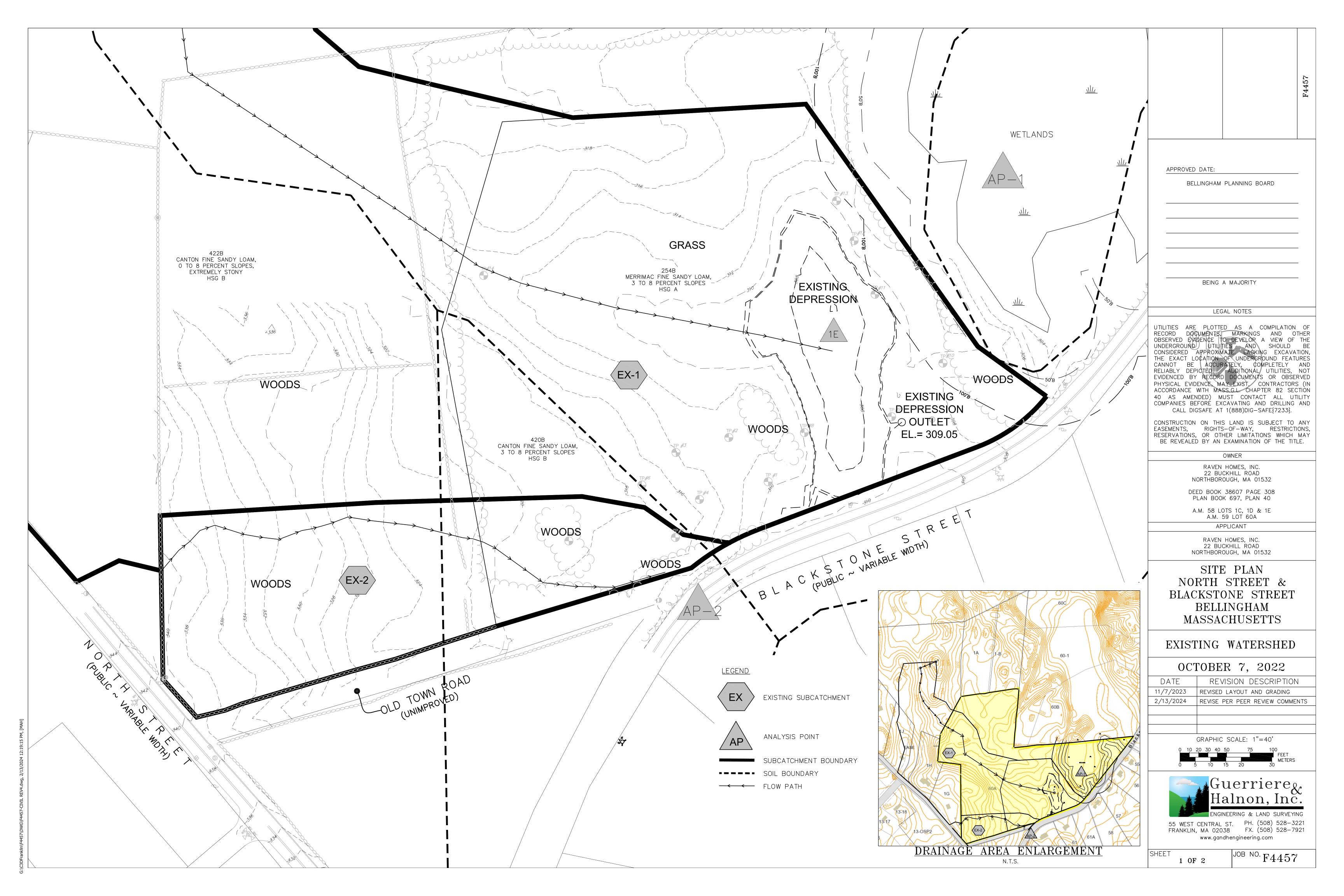
#### **Illicit Discharge Compliance Statement**

It is the intent of the Applicant, Raven Homes, Inc, 22 Buckhill Road, Northborough, MA 01532, (508)393-4511, to control illicit disposal into the storm drainage system. There will be no connection to the storm water system to inadvertently direct other types of liquids, chemicals or solids into the storm drainage system. The Applicant will also promote a clean Green Environment by mitigating spills onto pavements, oils, chemicals, pet waste, debris and litter.

Respectfully Acknowledged,

1000 Rayen Homes, Inc.

### Drainage Area Plans Appendix 10





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## SUPPLEMENTAL ATTACHMENTS Appendix 11

Pre-Post Development for 5 building layoutNRCC 2Prepared by {enter your company name here}HydroCAD® 10.00-21s/n 10299 © 2018 HydroCAD Software Solutions LLC

#### Hydrograph for Pond 1P: Infiltration Basin #1

Time	Inflow	Storage	Elevation	Outflow	Discarded	Primary	Secondary
(hours)	(cfs)	(cubic-feet)	(feet)	(cfs)	(cfs)	(cfs)	(cfs)
0.00	0.00	0	305.50	0.00	0.00	0.00	0.00
2.50	0.00	0	305.50	0.00	0.00	0.00	0.00
5.00	0.00	0	305.50	0.00	0.00	0.00	0.00
7.50	0.07	4	305.50	0.07	0.07	0.00	0.00
10.00	0.44	23	305.50	0.44	0.44	0.00	0.00
12.50	21.99	33,606	308.09	8.18	5.17	3.01	0.00
15.00	4.01	27,902	307.71	6.60	4.67	1.93	0.00
17.50	2.34	15,133	306.79	3.50	3.50	0.00	0.00
20.00	1.71	5,853	306.03	2.59	2.59	0.00	0.00
22.50	1.43	104	305.51	1.99	1.99	0.00	0.00
25.00	0.06	7	305.50	0.13	0.13	0.00	0.00
27.50	0.00	0	305.50	0.00	0.00	0.00	0.00
30.00	0.00	0	305.50	0.00	0.00	0.00	0.00
32.50	0.00	0	305.50	0.00	0.00	0.00	0.00
35.00	0.00	0	305.50	0.00	0.00	0.00	0.00
37.50	0.00	0	305.50	0.00	0.00	0.00	0.00
40.00	0.00	0	305.50	0.00	0.00	0.00	0.00
42.50	0.00	0	305.50	0.00	0.00	0.00	0.00
45.00	0.00	0	305.50	0.00	0.00	0.00	0.00
47.50	0.00	0	305.50	0.00	0.00	0.00	0.00
50.00	0.00	0	305.50	0.00	0.00	0.00	0.00
52.50	0.00	0	305.50	0.00	0.00	0.00	0.00
55.00	0.00	0	305.50	0.00	0.00	0.00	0.00
57.50	0.00	0	305.50	0.00	0.00	0.00	0.00
60.00	0.00	0	305.50	0.00	0.00	0.00	0.00
62.50	0.00	0	305.50	0.00	0.00	0.00	0.00
65.00	0.00	0	305.50	0.00	0.00	0.00	0.00
67.50	0.00	0	305.50	0.00	0.00	0.00	0.00
70.00	0.00	0	305.50	0.00	0.00	0.00	0.00

#### Land Use Coefficients "C"

Pave	0.90
Gravel	0.80
Wetland	0.72
Grass	0.30
Woods	0.25
Roof	0.90

Drainage	Land Use Area							Weighted
Area	Impervious	Gravel	Wetland	Pervious	Woods	Roof	Total	"C"
	(acres)	(acres)	(acres)	(acres)	(acres)	(acres)	(acres)	
DA-1A	0.346			0.198		0.186	0.731	0.74
DA-1B	0.357			0.108		0.130	0.595	0.79
DA-3A	0.094			0.093		0.000	0.187	0.60
DA-3B	0.076			0.041		0.000	0.118	0.69
DA-5					14.336		15.372	0.23
DA-6				0.351	0.000		0.351	0.30
SUBTOTAL	0.874	0.000	0.000	0.791	14.336	0.316	17.353	
OVERALL								
TOTALS	0.874			0.791	14.336	0.316	16.317	

Guerriere &	Halnon, Inc.										Project			Ν	orth Stre	eet & Blacks	tone Street,	Bellingham M	ΛA					
55 West Ce	ntral Steet										Job No.			4457										
Franklin, M	A 01757-023	4													-									
		DESIGN COMPUTATIONS FOR STORM DRAINS										I	Prepared By	KKP	Date	10/	12/2022	Revised	11-7-23	MAH				
		DESIGN COMPUTATIONS FOR STORM DRAINS											Checked By		Date			Revised						
																Invert E	levation	Rim	Elev					
Drainage				f ntrat ()	ty II	al Flow (Q)	ter		ness cient	II.	ty.	L7	of *()	.5	all									
Area			Sum of	ne of ncent	Rainfall Intensity (I)		e	Slope	tough Doeffic n)	Design Flow Ft (Q)	Velocity Flow Full (V)	Actual Velocity (V)	Length Pipe (L)	l'ime ii dipe	otal F.							Destinati	on	
	Upper	Lower	CA's	Tin Coi ion	Rai Inte (I)	Actu Peak Rate	Pip Dia	Slo	E C &	De: Flo (Q)	Vel Flo (V)	Act Vel (V)	Ler Pip	Tin pip	Tot	Elev.	Elev.	Elev.	Elev.					
	Structure	Structure	(sf)	(min)	(in/hr)	(cfs)	(in)	(ft/ft)		(cfs)	(fps)	(fps)	(ft)	(min)	(ft)	Upper End	Lower End	Upper End	Lower End					
DA-1	CB-1A	DMH-1	0.54	6.00	5.80	3.12	12	0.013	0.011	4.89	6.22	3.98	24.5	0.07	0.33	309.60	309.27	313.84	313.68					
	CB-1B	DMH-1	0.47	6.00	5.80	2.73	12	0.018	0.011	5.61	7.14	3.47	18.6	0.04	0.33	309.60	309.27	313.73	313.68					
	DMH-1	HW #1	1.01	6.07	5.80	5.85	12	0.024	0.011	6.51	8.29	7.45	73.9	0.15	1.77	308.77	307.00	313.68						
DA-3	CB-2A	DMH-2	0.11	6.00	5.80	0.65	12	0.005	0.011	2.97	3.78	0.83	14.1	0.06	0.07	307.67	307.60	310.47	310.86					
	CB-2B	DMH-2	0.08	6.00	5.80	0.47	12	0.007	0.011	3.48	4.43	0.60	10.3	0.04	0.07	307.67	307.60	310.47	310.86					
	DMH-2	HW #2	0.19	6.06	5.80	1.12	18	0.005	0.011	9.01	5.10	0.64	94.8	0.31	0.50	307.50	307.00	310.86						
																					IN	FILTRATION		
	OCS	HW #2				1.12	24	0.005	0.013	15.96	5.08	0.36	96.5	0.32	0.48	306.00	305.52				IIN		N DAGIN	

#### CONSTRUCTION PHASE INSPECTION FORMS

North Street and Blackston Bellingham MA	e Street
Date	Prev. Insp. Date:
Inspector:	Title:
Weather:	
Erosion Control - Inspect Weekly	
Comments:	
Corrective measures taken and date	
On Site Pavement Sweeping - Inspect Weekly	
Comments:	
Corrective measures taken and date	
Catch Basins - Inspect Weekly	
Comments:	
Corrective measures taken and date	
Corrective measures taken and date	
Stormceptor - Inspect Weekly	
Comments:	
Corrective measures taken and date	
Temporary Sediment Traps/Basins - Inspect Weekly	
Comments:	
Corrective measures taken and date	

#### CONSTRUCTION PHASE INSPECTION FORMS

#### North Street and Blackstone Street

#### Bellingham MA

#### Notify Conservation Commission RE Issues Effecting Resource Areas

Comments:
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Corrective measures taken and date

#### Silt on Public Streets - Inspect Weekly

Comments:

Corrective measures taken and date

Stock Pile Materials - Ring with Haybales - Inspect Weekly

Comments:

Corrective measures taken and date

Any Fuel or Chemical Spill - Inspect Daily

Comments:

Corrective measures taken and date

#### Post Construction Inspection Report North Street/Blackstone Street Bellingham, Massachusetts

INSPECTION DATE:				1				
Person Inspecting		Weather		Other Personnel Present				
		Clear						
ltem	N/A*	sat.**	NMR***	CAM**	MCA*	Comments:		
Pavement Swept								
Catch Basins								
CB #1A								
CB #1B								
CB #2A								
CB #2B								
Infiltration Basin #1								
Sediment Forebay Infiltration Basin								
Inlet Basin #2								
Infiltration Basin								
NMR* normal maintenance								
N/A* not applicable at the ti		ection						
CAM* corrective action - m								
SAT* satisfactory condition		ant						
MCA* Major corrective action	on							